

APPENDIX "E" TO SPECIAL PROVISIONS
STRUCTURES DESIGN CALCULATIONS

STRUCTURES DESIGN CALCULATIONS

FOR

Project Number:

PW Project No. 20200315, EDP-MT-20200315

Rehabilitation Design

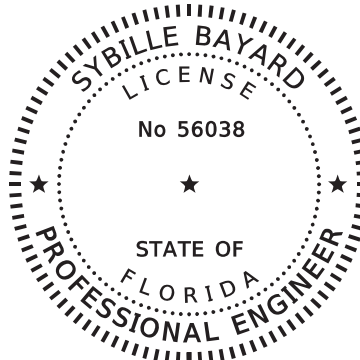
For

**Matheson Hammock Park Road (Bridge No.874294) over
Matheson Hammock Canal**

MIAMI-DADE

DEPARTMENT OF TRANSPORTATION AND PUBLIC WORKS

1/25/2022



Sybille Bayard
2022.04.21 10:54:49-04'00'

Table of Contents

1.0	LRFR BRIDGE CONDITION EVALUATION	3
1.1	LOAD RATING ANALYSIS APPROACH	4
1.2	SUMMARY OF LOAD RATING PARAMETERS	10
1.3	LRFR LOAD RATING ANALYSIS INPUT	21
1.4	SUMMARY OF LRFR LOAD RATING ANALYSIS RESULTS	167
2.0	SONOVOID SLAB UNIT STRENGTHENING - CFRP WRAPS EVALUATION	273
3.0	REQUIRED FORCE AND PRESTRESSING STRAND FOR REPLACEMENT OF EXISTING POST-TENSIONING WIRE	292
4.0	COLUMN LOADS FOR TEMPORARY SHORING	298
	APPENDICES	322
	APPENDIX A – AS-BUILT BRIDGE PLANS	323
	APPENDIX B – FDOT BRIDGE INSPECTION REPORT AND SUBSEQUENT INTERIM REPORTS	337
	APPENDIX C – HANNA ET. AL, “TRANSVERSE POST-TENSIONING DESIGN AND DETAILING OF PRECAST, PRESTRESSED CONCRETE ADJACENT-BOX-GIRDER BRIDGES”	501
	APPENDIX D – STRUCTURAL TECHNOLOGIES, LLC, “V-WRAP C200HM HIGH MODULUS CARBON FIBER FABRIC” ..	517
	APPENDIX E – STRUCTURAL TECHNOLOGIES, LLC., PRELIMINARY BRIDGE REPAIR RECOMMENDATIONS	520

1.0 LRFR BRIDGE CONDITION EVALUATION

1.1 LOAD RATING ANALYSIS APPROACH

Introduction

Bridge 874294, constructed in 1967, carries Matheson Hammock Road over Matheson Hammock Canal in Miami-Dade County. According to the the latest NBIS inspection report dated 04/06/2020 and subsequent interim reports, the ADT for this section of roadway is around 736 vehicles per day with a truck percentage of 1%.

Purpose and Need

The purpose of this analysis is to assess the existing bridge conditions and determine the added capacity required to restore the bridge to a non-posted state and able to load rate for anticipated construction vehicles for an upcoming park sea-level improvement project and able to safely maintain current traffic until the complete bridge replacement.

Bridge Configuration

The bridge superstructure consists of three simply-supported prestressed concrete 17"x36" sonovoid slab units. There is evidence at the bridge site of reflective longitudinal cracks in the asphalt wearing surface across the bridge indicating that the slab units are acting independently due to possible deterioration or broken transverse post-tensioned cables. The span configuration is 30.0 feet – 40.0 feet – 30.0 feet, with 11 prestressed slab units in each span. A variable asphalt wearing surface is present along the bridge spans.

Analysis Approach

This current load rating was performed using Load and Resistance Factor Rating (LRFR) methodology from the AASHTOWare Bridge Rating (Version 6.8.4) software. The previous load rating was performed on January 13, 2020 using LRFR methodology and Smart Bridge Suite Version 3.1 software. Since the most recent inspection (performed on 4/26/2021 by Marlin Engineering, Inc.) rated the deck and superstructure as "3 Serious", and the substructure as "4 Poor", this current load rating was performed using a Condition Factor of 0.85 for significantly deteriorated prestressed slab units, and a Condition Factor of 0.90 for non-deteriorated prestressed slab units per AASHTO MBE Table 6A.4.2.3-1.

Moreover, given the damage sustained by the controlling interior slab units 2-8 and 2-9 in span no. 2 (severed strand), and as per the 2007 Revision to Publication 238 Bridge Safety Inspection Manual from the Pennsylvania Department of Transportation, under section 6.6.3.3.1I, the following conservative assumptions were considered in the analysis:

"Load ratings of beams with deteriorated and/or damaged prestressing strands are to be based on the following procedures:

- Visually observed strands + 25% - Deduct 100% of all exposed strands plus an additional 25% (125% of the total area of the exposed strands) from capacity calculations.*
- Strands adjacent to or intersecting a crack shall be considered ineffective in the region immediately adjacent to the crack.*
- If significant strand loss is noted (>20%), especially for fascia beams, contact BQAD for further instructions.*
- For beams with no exposed strands but which appear to have internal damage (as evidenced by bottom flange cracking with rust and/or delamination), contact BQAD for further instructions.*

Bridge 874294 Load Rating

- *For fascia beams with Capacity/Dead Load < 1.5 or an Operating Rating < 1.5 based on a conventional analysis, an analysis that considers biaxial stresses will be performed by BQAD.*
- *These analysis methods may also be applicable to other pre-stressed box beam bridges”*

Therefore, a load rating analysis was performed to evaluate the existing capacity of the slab units within all three spans and provide recommendations for repair and strengthening as needed.

Evaluation of Existing Bridge (Current Conditions)

As stated above, the intent of the load rating analysis is to restore the bridge to a non-posted state able to safely carry the anticipated construction loads and the continuing traffic loading for a period not to exceed five years after the repairs, until the bridge is replaced. As such, only the Florida legal loads (SU2, SU3, SU4, C3, C4, C5 and ST5) were considered in this evaluation to provide a minimum rating factor of 1.0. The bridge does not carry interstate traffic nor is it State-owned or lying within 1 mile driving distance of an interstate interchange. Therefore, no Emergency Vehicles were investigated for this analysis (EV2 and EV3 were omitted). Load and Resistance Factor Rating (LRFR) was used for this assessment, as the preferred method for bridge rehabilitation per the FDOT Load Rating Manual.

Assumptions used in the analysis:

- 1) Assume independent action of the slab units: slab units are considered non-composite and the following criteria was used in the distribution of live loads for moment and shear applications:
 - a. Interior slab units assumed a wheel load distribution factor = 1.0 (no wheel load distribution between units assuming that the transverse post-tensioning system is ineffective).
 - b. Exterior (fascia) slab units located underneath the sidewalk assumed a wheel load distribution factor = 0.0 due to location of sidewalk curb directly above the units and no transfer of live from the adjacent units.
- 2) Assume a condition factor of 0.9, conservatively, to account for the age-related deterioration of the non-deteriorated units (units with minor or no deterioration identified in the most current interim inspection report).
- 3) Assume a condition factor of 0.85, conservatively, to account for the severe deterioration noted in the most current interim inspection report (Slab Units 1-6, 1-8, 2-8, 2-9).
- 4) For Slab Units 2-8 and 2-9 assume 100% section loss of a total of 7 strands in addition to the condition factor of 0.85.

Evaluation of Rehabilitated Bridge (Repaired Condition)

Additional analysis was conducted to evaluate the existing slab units assuming the replacement of the transverse post-tensioning system and the repair of cracks, delamination and spalls noted in the inspection report. The slab units were analyzed as integral, assuming a live load distribution factor in accordance with the AASHTO LRFD, Section 4.6.2.2.

The following assumptions were made:

1. Assume a condition factor of 0.9 for all slab units.

For Slab Units 2-8 and 2-9 assume 100% section loss of a total of 7 strands in addition to the condition factor of 0.9.

References

This current load rating was performed in accordance with the following manuals, specifications, and software:

- FDOT Structures Manual, January 2021 (SM) (Volume 1 - Structures Design Guidelines - (SDG))
- AASHTO LRFD Bridge Design Specifications, 9th Edition (AASHTO)
- FDOT Bridge Load Rating Manual, January 2021 (BLRM)
- The Manual for Bridge Evaluation, 3rd Edition 2018 (MBE) with 2019 Interims
- PCI Design Handbook, 8th Edition (PCI)
- AASHTOWare Bridge Rating, Version 6.8.4.
- Commonwealth of Pennsylvania Department of Transportation, Revision to Publication 238 Bridge Safety Inspection Manual, 2007.

It should be noted that the 2021 BLRM uses the 9th Edition of the AASHTO LRFD design specifications, and that AASHTOWare Bridge Rating Version 6.8.4 uses the 8th Edition of the AASHTO LRFD design specifications. However, since this bridge uses normal weight concrete and does not have prestressed slab units subjected to significant torsion, the applicable portions of the design codes have not changed between the two editions. Therefore, the software still meets the BLRM requirements for evaluating flexure and shear.

Summary of Results

Existing Bridge (Current Conditions)

The complete evaluation of all non-deteriorated and deteriorated slab units is shown in Sections 1.2 through 1.4 of the report. Given that no distribution is assumed between slab units, the exterior slab units were not evaluated for vehicular live loads and therefore do not control the results. By observations, the SU4 legal truck is the controlling live load; the resulting LRFR rating factors are summarized in the table below.

SUMMARY OF LRFR LOAD RATING RESULTS - SONOVOID SLAB UNITS (Existing Condition)								
Vehicle	Condition Factor	Member Condition	Live Load Type	Limit State	Controlling Member	Controlling Location (% Span)	Controlling Limit State	Rating Factor
SU 4	0.90	Non-Deteriorated	Axle Load	Legal	Interior Unit (Span 1)	50.0	STRENGTH-I Concrete Flexure	0.684
		Non-Deteriorated			Interior Unit (Span 2)	50.0	STRENGTH-I Concrete Flexure	0.624
	0.85	Deteriorated			Interior Unit (Unit 1-6 or 1-8)	50.0	STRENGTH-I Concrete Flexure	0.634
		Deteriorated			Interior Unit (Unit 2-8 or 2-9)	30.0	STRENGTH-I Concrete Shear	0.324

Figure 1-4.1 Summary of LRFR Load Rating Results for Existing Sonovoid Slab Units under Current Conditions.

As indicated in the table above, none of the slab units present an acceptable rating factor which would satisfy the demand for the anticipated construction loads. As such, re-establishing the post-tensioning of the existing non-deteriorated slabs and deteriorated slab units is required.

Rehabilitated Bridge (Repaired Condition)

The complete evaluation of all non-deteriorated slab units and repaired deteriorated slab units is shown in Sections 1.2 through 1.4 of the report. The interior and exterior slab units were both evaluated for vehicular live loads. By observations, the SU4 legal truck is the controlling live load; the resulting LRFR rating factors are summarized in the table below.

SUMMARY OF LRFR LOAD RATING RESULTS – SONOVOID SLAB UNITS (w/ Concrete Repairs and Post Tensioning Restored)								
Vehicle	Condition Factor	Member Condition	Live Load Type	Limit State	Controlling Member	Controlling Location (% Span)	Controlling Limit State	Rating Factor
SU 4	0.90	Non-Deteriorated	Axle Load	Legal	Interior Unit (Span 1)	50.0	STRENGTH-I Concrete Flexure	1.387
		Non-Deteriorated			Interior Unit (Span 2)	50.0	STRENGTH-I Concrete Flexure	1.461
		Deteriorated (repaired)			Interior Unit (Unit 1-6 or 1-8)	50.0	STRENGTH-I Concrete Flexure	1.387
		Deteriorated (repaired)			Interior Unit (Unit 2-8 or 2-9)	50.0	STRENGTH-I Concrete Flexure	0.931

Figure 1-4.2 Summary of LRFR Load Rating Results for Rehabilitated Sonovoid Slab Units with Concrete Repairs completed, and Post Tensioning restored.

Bridge 874294 Load Rating

As indicated above, the deteriorated slab units in Span 2 (2-8 & 2-9) did not achieve a minimum rating factor of 1.0 even when analyzed as integral. Consequently, the remaining capacity that is required to satisfy a minimum LRFR legal rating of 1.0 was computed as a final step in the evaluation process to determine the level of strengthening required to restore the bridge to a non-posted stated, as shown in the table below.


LOAD RATING SUMMARY - (Assuming Post Tensioning)					
Span 2 - INTERIOR Unit 2-8 (LRFR) - SU4					
Location	Condition Factor	Existing Flexural Capacity (kip-ft) **	Existing Shear Capacity (kip) **	Required Flexural Capacity (kip-ft) *	Required Shear Capacity (kip) *
0.00	0.90	135.08	-	-	-
1.12		-	94.16	-	-
1.48		293.46	89.01	-	-
3.85		344.64	70.05	-	-
7.7		344.64	70.05	-	-
11.55		344.64	49.78	-	-
15.4		344.64	38.99	359.34	-
19.25		344.64	-38.35	368.62	-
23.1		344.64	-38.99	359.34	-
26.95		362.07	-53.70	-	-
30.8		344.64	-70.05	-	-
34.65		344.64	-70.05	-	-
37.02		293.46	-89.01	-	-
37.39		-	-94.28	-	-
38.5		108.44	-	-	-

* Minimum Required capacity to meet a minimum Inventory Rating Factor of 1.1, conservatively.

** Existing condition assumes the removal of 7 strands, and 1 exterior stirrup leg to account for the controlling deterioration along the bottom face of the slab units.

Figure 1-4.3 Required Capacity of Rehabilitated Slab Units to satisfy LRFR Legal Rating.

1.2 SUMMARY OF LOAD RATING PARAMETERS

	Project No:		D210107FL.00	YRA	Date:	9/21/2021
	Bridge No.:		874294	HGD	Date:	9/24/2021
	Feature Carried:		Matheson Hammock Park		Page:	1 of 1

SUMMARY OF DEFICIENCIES

SONOVOID SLABS (UNDERSIDE) - SPAN 1

BEAM NO.	LOCATION	DEFICIENCY
1-1	EB1	Outward location with 1/4" height difference to top of cap
1-6	9-ft from EB1	15" x 6" x 1/2" - spall w/ exposed rebar / minor section loss
	EB1 / East	5'L x 6"W delamination with associated 1/16" cracks
	Pier 2 / East	9'L x 12"W delamination with associated 1/16" cracks
1-7	EB1 / East	24"L x 12"W spall/delamination with associated 1/32" cracks
	Pier 2 / East	7'L x 4"W delamination with associated 1/16" cracks
1-8	EB1 / West	15'L x 15"W delamination with associated 1/4" cracks
	9" from EB1 / West	4' x 6" x 2" - spall
	Pier 2 / East	4'L x 15"W delamination with associated 1/32" cracks
	Pier 2	8'L x 3'W delamination with associated 1/16" cracks
1-9	EB1	36"L x 24"W x 2.5" spall/delamination with exposed stirrup (no loss)
	Pier 2 / West	9'L x 10"W delamination with associated 1/16" cracks

SONOVOID SLABS (UNDERSIDE) - SPAN 2

BEAM NO.	LOCATION	DEFICIENCY
2-6	Pier 2 / East	30"L x 4"W delamination
2-7	Pier 2 / West	24"L x 4"W delamination
	full length	16"W delamination with associated 1/4" cracks
	Pier 2	36"L x full width with associated cracks
2-8	Pier 2 / West	15' x 18"W (average) delamination with associated 1/4" cracks
	Midspan	15'x34"x4" with 7 exposed and corroded transverse rebars w/ 60% section remaining and 5 exposed and corroded strands (3 broken strands) - 0% section remaining
	Pier 3 / West	15' x 18"W (average) delamination with associated 1/4" cracks
	Pier 2 / West	5'L x 5" delamination with associated 1/4" cracks
2-9	Midspan	15'x12"x2" spall/delamination with 2 strands and 7 transverse rebars having up to 90% section remaining

SONOVOID SLABS (UNDERSIDE) - SPAN 3

BEAM NO.	LOCATION	DEFICIENCY
3-6	Pier 3 / East	24"L x 6"W delamination with associated 1/16" crack
	~10' from EB 4 / East	42"L x 8" W with associated 1/16" cracks
3-7	Pier 3	8'L x 15"W delamination with associated cracks
	Midspan	3'L x 30" W
	EB 4	12'L x 36"W unsound repair / hollow sounding
3-8	Pier 3	8'L x 3'W x 1" with associated cracks
	EB4	42" x 30"W unsound repair/ delamination with associated 1/16" cracks
	5.5' from EB 4	74" x 36"W unsound repair/ delamination with associated 1/16" cracks

SUBSTRUCTURE

COMPONENT	LOCATION	DEFICIENCY
PIER CAPS	PIER 2 / South Face	48"L X 17" H X 3/4" Spall / Delamination over column 2-2
	PIER 2 / North Face	20"L x 12" H delamination over column 2-2
	PIER 3 / bottom / North	2~ 30"L x 24"W unsound repairs with 1/64" associated cracks between columns 3-1 and 3-2.
	PIER 3 / top & Bottom / North	3'L x 16" delamination between columns 3-1 and 3-2
COLUMNS	Column 2-2	55"H x 32"W x 4"D spall delamination with exposed longitudinal rebars and 5 stirrups (up to 80% remaining)
	Column 2-2	Delamination (entire column height / circumference) with associated 1/4" cracks
	Columns 2-1, 3-1, 3-2	Delamination (entire length) with associated 1/16" cracks (full height)

SPAN 1 OR 3 - SUPPLEMENTAL CALCULATIONS - LOADING PARAMETERS

Bridge Type: Prestressed Voided Slab Unit - 17"x36"
 Standard Drawing:

Total Superimposed Dead Load:	1.396 k/ft
Bridge Railing/ Guardrail Dead Load:	0.148 k/ft
Curb/Sidewalk Dead Load:	1.248 k/ft
Attached Utility Dead Load:	0.000 k/ft
Asphalt W.S. Dead Load (DW):	0.379 k/ft

Number of Spans = 3
 Structure Length = 100 ft.
 Brg.-to-Brg. Span Length = 28.2917 ft. (Assumed at Centerline of 1/4"x6" wide asbestos graphite pads)
 Analyzed Span Length = 30.00 ft.
 Clear Roadway Width = 26.00 ft.
 Wearing Surface: Yes A 1.0-inch wearing surface is present at the supports, and 1.5-in present at midspan.
 The wearing surface dead loads are calculated by BrR and included in the analysis.

Location	Thickness	Average Thickness		
Begin span	1.00 in	1.167 in	0.040833	4.085469
Mid Span	1.50 in			
End Span	1.00 in			

Bridge Railing/Guardrail: Yes Bridge Railing is present.
 Per SCDOT Load Rating guidance, guardrail dead loads are applied only to fascia beams.
 Curb/Sidewalk: Yes A curbs or sidewalks are present. See below for curb/sidewalk dimensions and dead load calculations.
 Parapet: No No parapets are present.
 Attached Utilities: Yes See below for dead load calculations.

Rail 1 Type: Other Metal Posts and Pipes - Assume 10 lb/ft per SDG Table 2.2-1, Bullet Railing **0.010 k/ft**
 10 lb/ft

Rail 2 Type: Rect. Conc. Beam Rectangular Concrete Beam Guardrail **0.125 k/ft**
 125 lb/ft

Rail Post:	Concrete	Quantity	Length/Height	Shape	Area (Standard shapes per AISC 7-14)	
	150 pcf	3 / span	0.83 ft	Rect. 10x10	100.00 in ²	0.013 k/ft
	150 pcf	2 / span	0.83 ft	Rect. 8x10	80.00 in ²	

Rail Blockout: none

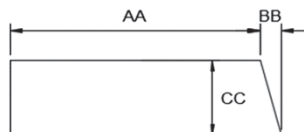
Curb/Sidewalk:	AA	29.0 in				
(South End)	BB	1.0 in				
	CC	10.563 in				0.325 k/ft

- Superstructure is modeled without the sidewalk overhang, that is removing the additional 6" of overhang.
- To account for the actual weight of curb/sidewalk, compute an equivalent Thickness of sidewalk corresponding to a rectangular sidewalk with an equivalent width of:


Equiv. Width of Sidewalk = 24 in (Equivalent width of rectangular sidewalk input in AASHTOWare software)


Equiv. CC = 12.9831 in (Equivalent thickness of rectangular sidewalk input in AASHTOWare software)

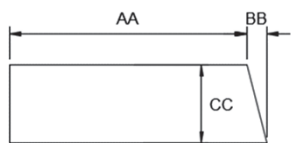
Typical Curb/Sidewalk Section



Curb/Sidewalk:	AA	77.0 in				
(North End)	BB	1.0 in				
	CC	11.4 in				0.923 k/ft

 CONSOR	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

 CONSOR	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	2 of 4



- Superstructure is modeled without the sidewalk overhang, that is removing the additional 6" of overhang.
- The 1-ft utility opening will be neglected, leaving 1-ft of additional solid sidewalk material assumed to account for the weight of utilities and attachments at the opening. The resulting width of sidewalk to be input in the software shall be:

Equiv. Width of Sidewalk = 60 in (Equivalent width of rectangular sidewalk input in AASHTOWare software)

- No information is available on the utilities and attachments along the North side of the bridge.
- The Concrete sidewalk will be assumed to be solid at the location of the utility opening to account for the weight of the utilities and attachments, conservatively.
- Assume weight of sidewalk taken by the exterior slab units.

Diaphragm:

Width of Slab Unit = 36 in
Depth of Slab Unit = 17 in
No. of Voids = 2.0000
Diameter of Voids = 10.0000 in

Begin Span					
	Start Dist. From Left End* (FT)	Diaphragm Spacing (FT)	No. of Spaces	Width/ Thickness (IN)	Diaphragm Weight (KIP)
Span 1, Begin	0.00	1.00	1	24.0	0.3272
Span 1, 1/4 Point	1.00	6.25	1	12.0	0.1636
Span 1, 3/4 Point	7.25	15.00	1	12.0	0.1636
Span 1, End	22.25	6.25	1	24.0	0.3272
Span 3, Begin	0.00	1.00	1	24.0	0.3272
Span 3, 1/4 Point	1.00	6.25	1	12.0	0.1636
Span 3, 3/4 Point	7.25	15.00	1	12.0	0.1636
Span 3, End	22.25	6.25	1	24.0	0.3272


LLDF (Post-Tensioned - LFD): (Assuming Members are sufficiently connected to act as a unit, meaning accounting for effective post tensioning)


For Interior/Exterior Slab Units: (Moment & Shear)

[AASHTO LFD 3.23.4.3]

S = 3.0 ft. (Width of precast member)
W = 34.0 ft. (Assumed total width of Bridge Superstructure - ignore opening at the N end sidewalk)
L = 28.291667 ft. (Brg.-to-Brg. Span Length - Span 2)
NL = 2.0 (Number of traffic lanes)
Nb = 11.0 (Number of concrete slab units)
μ = 0.2 (Assumed Poisson's Ratio for concrete slab units)

I = 13330.10 in⁴ (Moment of Inertia of Slab Unit - from BrM software)
J = 14593.77 in⁴ (Saint-Venant Torsion constant - from BrM software)

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	3 of 4

$$K = [(1 + \mu) \cdot I/J]^{1/2} = 1.04694$$

$$C = \text{if } \left[\frac{W}{L} < 1, K \left(\frac{W}{L} \right), K \right] = 1.04694$$

$$D = (5.75 - 0.5N_L) + 0.7N_L(1 - 0.2C)^2 = 5.6251$$

$$\text{LLDF (INT-M)} = S/D = \boxed{0.5333} \text{ (Live Load Distribution Fraction for Moment)}$$

LLDF (Post-Tensioned - LRFR): (Assuming Members are sufficiently connected to act as a unit, meaning accounting for effective post tensioning)

LLDF(INT - OneLane) =	0.296	(LLDF for One lane loaded for Moment and Shear computed for Interior Slab unit in AASHTOWare BrR in accordance with AASHTO LRFD Tables 4.6.2.2.2b-1 and 4.6.2.2.2d-1)
LLDF(INT - MultiLane) =	0.273	(LLDF for Multi lanes loaded for Moment and Shear computed for Interior Slab unit in AASHTOWare BrR in accordance with AASHTO LRFD Tables 4.6.2.2.2b-1 and 4.6.2.2.2d-1)

For Exterior Slab Units: (Moment)

[AASHTO LRFD Table 4.6.2.2.2d-1]

$$d_{e,G11} = -1.0 \text{ ft.}$$

(Horizontal distance from centerline of exterior web of exterior beam/slab unit along the south end at deck level to interior edge of curb or traffic barrier) - (Ext.web = 5"; outboard of curb) - limited to -1.0 since de computed is = 1.8' per AASHTO LRFD 4.6.2.2.2d.

$$d_{e,G1} = -1.0 \text{ ft.}$$

(Horizontal distance from centerline of exterior web of exterior slab unit along the south end at deck level to interior edge of curb or traffic barrier) - (Ext. web = 5"; outboard of curb) - limited to -1.0 since de computed is = 4.8' per AASHTO LRFD 4.6.2.2.2d.

- One Design Lane Loaded:

$$e_{\text{OneLane}_G1} = 1.125 + \frac{d_{e,G1}}{30} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{OneLane}_{G11}} = 1.125 + \frac{d_{e,G11}}{30} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$\text{LLDF (EXT.G1-M}_{\text{OneLane}}) = e \cdot \text{LLDF(INT - M)} = \boxed{0.2960} \text{ (Live Load Distribution Fraction for Moment for One lane Loaded - Unit G1)}$$

$$\text{LLDF (EXT.G11-M}_{\text{OneLane}}) = e \cdot \text{LLDF(INT - M)} = \boxed{0.2960} \text{ (Live Load Distribution Fraction for Moment for One lane Loaded - Unit G11)}$$


- Two or More Design Lanes Loaded:


$$e_{\text{OneLane}_G1} = 1.04 + \frac{d_{e,G1}}{25} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{OneLane}_{G11}} = 1.04 + \frac{d_{e,G11}}{25} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$\text{LLDF (EXT.-M}_{\text{MultiLane}}) = e \cdot \text{LLDF(INT - M)} = \boxed{0.2730} \text{ (Live Load Distribution Fraction for Moment for Multi-Lanes Loaded - Unit G1)}$$

$$\text{LLDF (EXT.-M}_{\text{MultiLane}}) = e \cdot \text{LLDF(INT - M)} = \boxed{0.2730} \text{ (Live Load Distribution Fraction for Moment for Multi-Lanes Loaded - Unit G11)}$$

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	4 of 4

For Exterior Slab Units: (Shear)

[AASHTO LRFD Table 4.6.2.2.3b-1]

$$d_{e,G1} = -1.0 \text{ ft.}$$

(Horizontal distance from centerline of exterior web of exterior slab unit along the south end at deck level to interior edge of curb or traffic barrier) - (Ext. web = 5"; outboard of curb) - limited to -1.0 since d_e computed is = 4.8' per AASHTO LRFD 4.6.2.2.2d.

$$d_{e,G11} = -1.0 \text{ ft.}$$

(Horizontal distance from centerline of exterior web of exterior beam/slab unit along the south end at deck level to interior edge of curb or traffic barrier) - (Ext. web = 5"; outboard of curb)

$$b = 36.0 \text{ in.}$$

(Width of precast member)

- One Design Lane Loaded:

$$e_{\text{OneLane}_G1} = 1.25 + \frac{d_{e,G1}}{20} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{OneLane}_{G11}} = 1.25 + \frac{d_{e,G11}}{20} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$LLDF(\text{EXT.}G1-M_{\text{OneLane}}) = e_{\text{OneLane}_G1} \cdot LLDF(INT,V) = 0.2960 \text{ (Live Load Distribution Fraction for Shear for One lane Loaded - Unit G1)}$$

$$LLDF(\text{EXT.}G11-M_{\text{OneLane}}) = e_{\text{OneLane}_{G11}} \cdot LLDF(INT,V) = 0.2960 \text{ (Live Load Distribution Fraction for Shear for One lane Loaded - Unit G11)}$$

- Two or More Design Lanes Loaded:

$$e_{\text{MultiLane}_G1} = 1.0 + \left(\frac{d_{e,G1} + \frac{b}{12} - 2.0}{40} \right)^{0.5} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{MultiLane}_{G11}} = 1.0 + \left(\frac{d_{e,G11} + \frac{b}{12} - 2.0}{40} \right)^{0.5} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$LLDF(\text{EXT.}-M_{\text{MultiLane}}) = e_{\text{MultiLane}_G1} \cdot LLDF(INT,V) = 0.2730 \text{ (Live Load Distribution Fraction for Shear for Multi-Lanes Loaded - Unit G1)}$$

$$LLDF(\text{EXT.}-M_{\text{MultiLane}}) = e_{\text{MultiLane}_{G11}} \cdot LLDF(INT,V) = 0.2730 \text{ (Live Load Distribution Fraction for Shear for Multi-Lanes Loaded - Unit G11)}$$

LLDF (Exist.Condition - LFD): (Assuming Slab Members acting independently - no effective post tensioning)

$$S = 3.0 \text{ ft.}$$

(Width of precast member)

$$W = 34.0 \text{ ft.}$$

(Assumed total width of Bridge Superstructure - ignore opening at the N end sidewalk)

$$L = 28.291667 \text{ ft.}$$

(Brg.-to-Brg. Span Length - Span 2)

$$NL = 2.0$$

(Number of traffic lanes)

$$Nb = 11.0$$

(Number of concrete slab units)

$$D = 3.0000$$

(Assumed equal to Precast member width since slab unit will behave independently. Therefore, individual unit can be assumed to take on the full wheel load)

$$LLDF(INT - LFD) = S/D = 1.0000 \text{ (Live Load Distribution Fraction for Moment and Shear)}$$

LLDF (Exist.Condition - LRFR): (Assuming Slab units acting independently - no effective post tensioning)

$$LLDF(INT - \text{OneLane} - LRFR) = 0.5 \times \text{Axle} = 0.5000 \text{ (Live Load Distribution Fraction for Moment and Shear - Half of Axle Load)}$$

$$LLDF(INT - \text{OneLane} - LRFR) = 0.5 \times 1.2 \times \text{Axle} = 0.6000 \text{ (Live Load Distribution Fraction for Moment and Shear - Half of Axle Load)}$$

Analysis Case: A) For the purpose of the Load Rating, the following Cases were assumed for AASHTOWare BrR runs:

- Case 1: Run model to account for the condition where the slab units have been rehabilitated with Post Tensioning.
- Case 2: Run model to account for the existing condition without repairs.

B) Per current inspection report, the following are assumed in the analysis to account for the deterioration of the slab unit 1-8:

- West edge of slab unit intermittently delaminated with efflorescence and corrosion bleed-out and associated spalling.
- Assume a condition factor of 0.85 to account for the analysis of the worst case deteriorated slab unit from spans 1 & 3.

SPAN 2 - SUPPLEMENTAL CALCULATIONS - LOADING PARAMETERS

Bridge Type: **Prestressed Voided Slab Unit - 17"x36"**
Standard Drawing:

Total Superimposed Dead Load:	1.395 k/ft
Bridge Railing/ Guardrail Dead Load:	0.147 k/ft
Curb/Sidewalk Dead Load:	1.248 k/ft
Attached Utility Dead Load:	0.000 k/ft
Asphalt W.S. Dead Load (DW):	0.420 k/ft
Asphalt W.S. Dead Load per Slab Unit (DW):	0.038 k/ft

Number of Spans:	3
Number of Sonovoids:	11
Structure Length:	100 ft.
Brg.-to-Brg. Span Length:	38.5 ft. (Assumed at Centerline of 1/4"x6" wide asbestos graphite pads)
Analyzed Span Length:	40.00 ft.
Clear Roadway Width:	26.00 ft.
Slab Unit Width:	36.00 in.
Wearing Surface:	Yes A 1.0-inch wearing surface is present at the supports, and 1.875-in present at midspan. The wearing surface dead loads are calculated by BrR and included in the analysis.

Location	Thickness	Average Thickness
Begin span	1.00 in	1.292 in
Mid Span	1.88 in	
End Span	1.00 in	

Bridge Railing/Guardrail:	Yes	Bridge Railing is present. Per SCDOT Load Rating guidance, guardrail dead loads are applied only to fascia beams.
Curb/Sidewalk:	Yes	A curbs or sidewalks are present. See below for curb/sidewalk dimensions and dead load calculations.
Parapet:	No	No parapets are present.
Attached Utilities:	Yes	See below for dead load calculations.

Rail 1 Type:	Other	Metal Posts and Pipes - Assume 10 lb/ft per SDG Table 2.2-1, Bullet Railing	0.010 k/ft
	10 lb/ft		

Rail 2 Type:	Rect. Conc. Beam	Rectangular Concrete Beam Guardrail	0.125 k/ft
	125 lb/ft		

Rail Post:	Concrete	Quantity	Length/Height	Shape	Area (Standard shapes per AISC 7-14)	0.012 k/ft
	150 pcf	4 / span	0.83 ft	Rect. 10x10	100.00 in ²	
	150 pcf	2 / span	0.83 ft	Rect. 8x10	80.00 in ²	

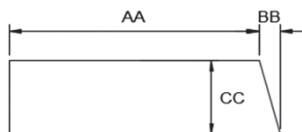
Rail Blockout:	none
----------------	------


Curb/Sidewalk:	AA	29.0 in	0.325 k/ft
(South End)	BB	1.0 in	
	CC	10.6 in	


- Superstructure is modeled without the sidewalk overhang, that is removing the additional 6" of overhang.
- To account for the actual weight of curb/sidewalk, compute an equivalent Thickness of sidewalk corresponding to a rectangular
Equiv. Width of Sidewalk = 24 in (Equivalent width of rectangular sidewalk inputted in AASHTOWare software)

Equiv. CC = 12.9831 in (Equivalent thickness of rectangular sidewalk inputted in AASHTOWare software)

Typical Curb/Sidewalk Section



	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

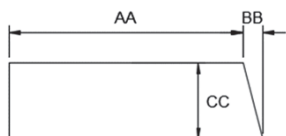
	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	2 of 4

Curb/Sidewalk:	AA	77.0 in
(North End)	BB	1.0 in
	CC	11.4 in

0.923 k/ft

- Superstructure is modeled without the sidewalk overhang, that is removing the additional 6" of overhang.
- The 1-ft utility opening will be neglected, leaving 1-ft of additional solid sidewalk material assumed to account for the weight of utilities and attachments, conservatively.

Equiv. Width of Sidewalk = 60 in (Equivalent width of rectangular sidewalk input in AASHTOWare software)



- No information is available on the utilities and attachments along the North side of the bridge.
- The Concrete sidewalk will be assumed to be solid at the location of the utility opening to account for the weight of the utilities and attachments, conservatively.
- Assume weight of sidewalk taken by the exterior slab units.

Diaphragm:	
Width of Slab Unit =	36 in
Depth of Slab Unit =	17 in
No. of Voids =	2.0000
Diameter of Voids =	10.0000 in

	Begin Span				
	Start Dist. From Left End* (FT)	Diaphragm Spacing (FT)	No. of Spaces	Width/ Thickness (FT)	Diaphragm Weight (KIP)
Span 2, Begin	0.00	1.00	1	2.0	0.3272
Span 2, 1/4 Point	1.00	8.96	1	1.0	0.1636
Span 2, 3/4 Point	9.96	20.00	1	1.0	0.1636
Span 2, End	29.9583	8.96	1	2.0	0.3272


LLDF (Post-Tensioned - LFD): (Assuming Members are sufficiently connected to act as a unit, meaning accounting for effective post tensioning)


For Interior Slab Units:

[AASHTO LRFD Table 4.6.2.2.2b-1]

S =	3.0	ft.	(Width of precast member)
W =	34.0	ft.	(Assumed total width of Bridge Superstructure - ignore opening at the N end sidewalk)
L =	38.5	ft.	(Brg.-to-Brg. Span Length - Span 2)
NL =	2.0		(Number of traffic lanes)
Nb =	11.0		(Number of concrete slab units)
μ =	0.2		(Assumed Poisson's Ratio for concrete slab units)
I =	13330.10	in ⁴	(Moment of Inertia of Slab Unit - from BrM software)
J =	14593.77	in ⁴	(Saint-Venant Torsion constant - from BrM software)

$$K = [(1 + \mu) \cdot I/J]^{1/2} = 1.04694$$

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	3 of 4

$$C = \text{if } \left[\frac{W}{L} < 1, K \left(\frac{W}{L} \right), K \right] = 0.92457$$

$$D = (5.75 - 0.5N_L) + 0.7N_L(1 - 0.2C)^2 = 5.6801$$

$$\text{LLDF (INT - LFD)} = S/D = \boxed{0.5282} \text{ (Live Load Distribution Fraction for Moment and Shear)}$$

For Exterior Slab Units:

[AASHTO LRFD Table 4.6.2.2.2d-1]

$$d_e = \boxed{3.0} \text{ ft. (Width of precast member)}$$

LLDF (Post-Tensioned - LRFR): (Assuming Members are sufficiently connected to act as a unit, meaning accounting for effective post tensioning)

$$\begin{aligned} \text{LLDF(INT - OneLane)} &= \boxed{0.254} && \text{(LLDF for One lane loaded for Moment and Shear computed for Interior Slab unit in AASHTOWare BrR in} \\ \text{LLDF(INT - MultiLane)} &= \boxed{0.256} && \text{(LLDF for Multi lanes loaded for Moment and Shear computed for Interior Slab unit in AASHTOWare BrR in} \end{aligned}$$

For Exterior Slab Units: (Moment)

[AASHTO LRFD Table 4.6.2.2.2d-1]

$$d_{e,G11} = \boxed{-1.0} \text{ ft. (Horizontal distance from centerline of exterior web of exterior beam/slab unit along the south end at deck}$$

$$d_{e,G1} = \boxed{-1.0} \text{ ft. (Horizontal distance from centerline of exterior web of exterior slab unit along the south end at deck level to}$$

- One Design Lane Loaded:

$$e_{\text{OneLane}_G1} = 1.125 + \frac{d_{e,G1}}{30} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{OneLane}_{G11}} = 1.125 + \frac{d_{e,G11}}{30} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$\text{LLDF (EXT.G1-M}_{\text{OneLane}}) = e_{\text{OneLane}_G1} \cdot \text{LLDF(INT, M)} = \boxed{0.2540} \text{ (Live Load Distribution Fraction for Moment for One lane Loaded - Unit G1)}$$

$$\text{LLDF (EXT.G11-M}_{\text{OneLane}}) = e_{\text{OneLane}_{G11}} \cdot \text{LLDF(INT, M)} = \boxed{0.2540} \text{ (Live Load Distribution Fraction for Moment for One lane Loaded - Unit G11)}$$


- Two or More Design Lanes Loaded:


$$e_{\text{MultiLane}_G1} = 1.04 + \frac{d_{e,G1}}{25} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G1)}$$

$$e_{\text{MultiLane}_{G11}} = 1.04 + \frac{d_{e,G11}}{25} \geq 1.0 = 1.000 \text{ (Correction factor for LL distribution on exterior slab unit G11)}$$

$$\text{LLDF (EXT.-M}_{\text{MultiLane}}) = e_{\text{MultiLane}_G1} \cdot \text{LLDF(INT, M)} = \boxed{0.2560} \text{ (Live Load Distribution Fraction for Moment for Multi-Lanes Loaded - Unit G1)}$$

$$\text{LLDF (EXT.-M}_{\text{MultiLane}}) = e_{\text{MultiLane}_{G11}} \cdot \text{LLDF(INT, M)} = \boxed{0.2560} \text{ (Live Load Distribution Fraction for Moment for Multi-Lanes Loaded - Unit G11)}$$

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	1 of 4

	Project No:	D210107FL.00	Calculated by:	YRA	Date:	9/21/2021
	Bridge No.:	874294	Checked by:	MAP	Date:	12/29/2021
	Feature Carried:	Matheson Hammock Road			Page:	4 of 4

For Exterior Slab Units: (Shear)

[AASHTO LRFD Table 4.6.2.2.3b-1]

$d_{e,G1} = -1.0$ ft. (Horizontal distance from centerline of exterior web of exterior slab unit along the south end at deck level to
 $d_{e,G11} = -1.0$ ft. (Horizontal distance from centerline of exterior web of exterior beam/slab unit along the south end at deck
 $b = 36.0$ in. (Width of precast member)

- One Design Lane Loaded:

$$e_{OneLane_G1} = 1.25 + \frac{d_{e,G1}}{20} \geq 1.0 = 1.000 \quad (\text{Correction factor for LL distribution on exterior slab unit G1})$$

$$e_{OneLane_G11} = 1.25 + \frac{d_{e,G11}}{20} \geq 1.0 = 1.000 \quad (\text{Correction factor for LL distribution on exterior slab unit G11})$$

$$LLDF (EXT.G1-M_{OneLane}) = e_{OneLane_G1} \cdot LLDF (INT, V) = 0.2540 \quad (\text{Live Load Distribution Fraction for Shear for One lane Loaded - Unit G1})$$

$$LLDF (EXT.G11-M_{OneLane}) = e_{OneLane_G11} \cdot LLDF (INT, V) = 0.2540 \quad (\text{Live Load Distribution Fraction for Shear for One lane Loaded - Unit G11})$$

- Two or More Design Lanes Loaded:

$$e_{MultiLane_G1} = 1.0 + \left(\frac{d_{e,G1} + \frac{b}{12} - 2.0}{40} \right)^{0.5} \geq 1.0 = 1.000 \quad (\text{Correction factor for LL distribution on exterior slab unit G1})$$

$$e_{MultiLane_G11} = 1.0 + \left(\frac{d_{e,G11} + \frac{b}{12} - 2.0}{40} \right)^{0.5} \geq 1.0 = 1.000 \quad (\text{Correction factor for LL distribution on exterior slab unit G11})$$

$$LLDF (EXT.-M_{MultiLane}) = e_{MultiLane_G1} \cdot LLDF (INT, V) = 0.2560 \quad (\text{Live Load Distribution Fraction for Shear for Multi-Lanes Loaded - Unit G1})$$

$$LLDF (EXT.-M_{MultiLane}) = e_{MultiLane_G11} \cdot LLDF (INT, V) = 0.2560 \quad (\text{Live Load Distribution Fraction for Shear for Multi-Lanes Loaded - Unit G11})$$

LLDF (Exist.Condition - LFD): (Assuming Members acting independently - no effective post tensioning)

$S = 3.0$ ft. (Width of precast member)
 $W = 34.0$ ft. (Assumed total width of Bridge Superstructure - ignore opening at the N end sidewalk)
 $L = 38.5$ ft. (Brg.-to-Brg. Span Length - Span 2)
 $NL = 2.0$ (Number of traffic lanes)
 $Nb = 11.0$ (Number of concrete slab units)
 $D = 3.0000$ (Assumed equal to Precast member width since slab unit will behave independently. Therefore, individual unit can be assumed to take on the full wheel load)

$$LLDF (LFD) = S/D = 1.0000 \quad (\text{Live Load Distribution Fraction for Moment and Shear})$$

LLDF (Exist.Condition - LRFR): (Assuming Slab units acting independently - no effective post tensioning)

$$LLDF (INT - OneLane - LRFR) = 0.5 \times \text{Axle} = 0.5000 \quad (\text{Live Load Distribution Fraction for Moment and Shear - Half of Axle Load})$$

$$LLDF (INT - OneLane - LRFR) = 0.5 \times 1.2 \times \text{Axle} = 0.6000 \quad (\text{Live Load Distribution Fraction for Moment and Shear - Half of Axle Load})$$

Analysis Case: A) For the purpose of the Load Rating, the following Cases were assumed for AASHTOWare BrR runs:

- Case 1: Run model for non deteriorated units to account for the condition where the slab units have been rehabilitated.
- Case 2: Run model for non-deteriorated and deteriorated units to account for the existing condition without repairs.
- Case 3: Run model for deteriorated units to account for the condition where the slab units have been rehabilitated, but no strands have been replaced.

B) Per current inspection report, the following are assumed in the analysis to account for the deterioration of the slab unit 2-8:

- 5 exposed strands, with 3 broken: Remove a total of 5 strands from the bottom layer of strands.
- Assume 50% of the adjacent strands along the same layer have been affected to account for the potential of damage in the adjacent strands. That is: Remove 1 additional strand from the bottom layer of strands.
- Assume 50% of the adjacent strands at the next layer have been affected to account for the potential of damage in the adjacent strands. That is: Remove 1 additional strand from the next layer of strands.
- Per recommendation from "Structural Technologies" on 10/01/2021, assume exterior stirrup leg to be deteriorated. In BrR, use 2 legs of shear reinforcement, conservatively for the critical case.

1.3 LRFR LOAD RATING ANALYSIS INPUT

Username: BrR

Date: Wednesday, September 22, 2021 11:21:02

Bridge ID 874294D Matheson Hmck Bridge over Matheson Hammock Canal

NBI Structure ID (8): 874294D

Description: Rating by YRA, from As-built plans [LAST UPDATED: 9/22/2021]

DETERIORATED MODEL:

Three spans (30'-40'-30') non-composite PS Concrete voided slab unit superstructure comprised of eleven (11) 17"x36" units. Deck width is 35'-0" out-to-out with a 26'-0" clear roadway width.

Wearing surface is present along the bridge with an average thickness of 1.167" along end spans 1 and 3, and 1.292" for interior span 2.

Per current inspection report, the following controlling cases apply:

- Prestressed slab unit 1-8 displaying severe cracking with corrosion stain along the bottom face of the slab unit.
- Prestressed slab unit 2-8 displaying the worst deterioration: Five (5) exposed strands with three (3) broken.

The load rating analysis for the prestressed voided slab units was initially performed using the Load and Resistance factor Rating methodology in accordance with the AASHTO LRFD Bridge Design Specifications (9th edition, 2020), the Manual for Bridge Evaluation (3rd edition with interims through 2019), and the FDOT Bridge Load Rating Manual (January 2021). However, the resulting design and legal rating factors were less than 1, which granted the need to evaluate the structure using the Load Factor Rating methodology.

Description

Location:	Matheson Hammock Park
Total Length:	100.33 <i>(ft)</i>
Facility Carried:	Matheson Hmk Road
Route Number:	00000
Feature Intersected:	Matheson Hammock Canal
Mi Post:	0.08 <i>(mi)</i>
Units:	US Customary
Year Built:	1967
Recent ADTT:	11
District:	District 6
County:	
Owner:	County Hwy Agency
National Highway System:	0 Not on NHS
Functional Class:	09 Rural Local

Global Reference Point

X Coordinate:	0.000 <i>(ft)</i>
Y Coordinate:	0.000 <i>(ft)</i>
Elevation:	<i>(ft)</i>
Longitude:	80.26 <i>(Degrees)</i>
Latitude:	25.68 <i>(Degrees)</i>

Materials

No steel materials.

Concrete

Name: **Class P (5000)**
Description: Class 5000 cement concrete
Specified compressive strength at 28 days (f'_c): 5.000 (ksi)
Initial specified compressive strength (f'_{ci}): 4.000 (ksi)
Coefficient of thermal expansion: 0.0000060000 (1/F)
Density (for dead loads): 0.150 (kcf)
Density (for modulus of elasticity): 0.145 (kcf)
Std Modulus of elasticity (E_c): 4074.28 (ksi)
LRFD Modulus of elasticity (E_c): 4291.19 (ksi)
Poisson's ratio: 0.200
Modulus of rupture: 0.537 (ksi)
Shear factor: 1.000
Composition of concrete: Normal
Std Initial modulus of elasticity (E_{ci}): 3644.15 (ksi)
LRFD Initial modulus of elasticity (E_{ci}): 3986.55 (ksi)
Splitting tensile strength (f_{ct}): (ksi)

Name: **Class A (3000)**
Description: Class A cement concrete (3000 psi)
Specified compressive strength at 28 days (f'_c): 3.000 (ksi)
Initial specified compressive strength (f'_{ci}): (ksi)
Coefficient of thermal expansion: 0.0000060000 (1/F)
Density (for dead loads): 0.150 (kcf)
Density (for modulus of elasticity): 0.145 (kcf)
Std Modulus of elasticity (E_c): 3150.39 (ksi)
LRFD Modulus of elasticity (E_c): 3617.02 (ksi)
Poisson's ratio: 0.200
Modulus of rupture: 0.416 (ksi)
Shear factor: 1.000
Composition of concrete: Normal
Std Initial modulus of elasticity (E_{ci}): (ksi)
LRFD Initial modulus of elasticity (E_{ci}): (ksi)
Splitting tensile strength (f_{ct}): (ksi)

Reinforcing Steel

Name: **Grade 40**
Description: 40 ksi reinforcing steel
Specified yield strength (F_y): 40.000 (ksi)
Modulus of elasticity (E_s): 29000.00 (ksi)
Ultimate strength (F_u): 70.000 (ksi)
Type: Plain

Prestressing Strand

Name: **7/16" (7W-250) SR**
Description: Stress relieved 7/16"/Seven Wire/fpu = 250

Specified yield strength (Fy):	212.500 (ksi)
Ultimate Tensile strength (Fu):	250.000 (ksi)
Modulus of elasticity (Es):	28500.00 (ksi)
Load per unit length:	0.367 (lb/ft)
Cross sectional area (A):	0.108 (in ²)
Nominal diameter (d):	0.4375 (in)
Transfer length (Std):	21.8750 (in)
Transfer length (LRFD):	26.2500 (in)
Type:	Stress Relieved
Epoxy coated:	FALSE

No timber materials.

Beam Shapes

Steel Shapes

No steel shapes.

Prestressed Shapes

No prestressed I shapes.

Prestressed Box Shapes

Name:	17"x36" PSU
Description:	17"x36" Prestressed Slab Unit for units E thru G
Type:	Circular Void
Nominal Depth:	17.0000 (in)
Depth (d):	17.0000 (in)
Top flange width:	35.0000 (in)
Bottom flange width:	36.0000 (in)
Three-void (D1, D2, D1) shape:	FALSE
Circular void diameter:	10.0000 (in)
Distance to CG of void(s) from bottom:	9.0000 (in)
Number of circular voids:	2
Center to center distance of voids:	16.0000 (in)
Vertical location of shear key:	2.0000 (in)
Shear key height:	6.0000 (in)
Shear key depth:	1.5000 (in)
Nominal load:	457.107 (lb/ft)
Cross sectional area:	438.822 (in ²)
Ixx:	13330.101 (in ⁴)
CG from bottom:	8.1667 (in)
Bottom Sxx:	1632.246 (in ³)
Top Sxx:	1509.078 (in ³)

Volume/Surface Ratio: 3.175 (in)
 Half Depth Area for Positive Flexure: (in^2)
 Half Depth Area for Negative Flexure: (in^2)
 St. Venant's Torsional Constant: 14593.772 (in^4)

Strand Grid

Row Number	Number of Strands	Vertical Location (in)	Horizontal Spacing (in)
1	16	2.5000	2.0000
2	6	4.5000	2.0000
3	16	14.5000	2.0000

No prestressed U shapes.

No prestressed tee shapes.

Timber Shapes

No timber shapes.

Appurtenances

No concrete railings.

Railings

Name: **Conc Guardrail w/ metal Post and Rail**
 Description: Conc. Post and beam guardrail with post and tube rail mounted
 Effective Wind Height: 36.0000 (in)
 Railing Load: 0.166 (kip/ft)
 Distance From Edge to Centroid: 5.0000 (in)
 Width: 10.0000 (in)

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Factors

Factors - LFD

Name: 2002 AASHTO Std. Specifications
 Description: AASHTO Standard Specifications for Highway Bridges, 17th Edition, 2002

Load Factors

Load Group	Gamma D		(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.900

Reinforced concrete:

Shear: 0.850

Prestressed concrete:

Flexure: 1.000

Prestressed concrete:

Shear: 0.900

Prestressed concrete:

Flexure in Non-P/S Components: 0.900

Steel:

Flexure: 1.000

Steel:

Shear: 1.000

Steel:

Bearing Stiffeners: 1.000

Name: 2002 AASHTO Std. Specifications(CD=0.90)

Description: AASHTO Standard Specifications for Highway Bridges,
17th Edition, 2002

Load Factors

Load Group	Gamma D		(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.810

Reinforced concrete:

Shear: 0.765

Prestressed concrete:

Flexure: 0.900

Prestressed concrete:

Shear: 0.810

Prestressed concrete:

Flexure in Non-P/S Components: 0.810

Steel:
 Flexure: 0.900
 Steel:
 Shear: 0.900
 Steel:
 Bearing Stiffeners: 0.900
 Name: 2002 AASHTO Std. Specifications(CD=0.85)
 Description: AASHTO Standard Specifications for Highway Bridges,
 17th Edition, 2002

Load Factors

Load Group	Gamma D	(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:
 Flexure: 0.765
 Reinforced concrete:
 Shear: 0.723
 Prestressed concrete:
 Flexure: 0.850
 Prestressed concrete:
 Shear: 0.765
 Prestressed concrete:
 Flexure in Non-P/S Components: 0.765
 Steel:
 Flexure: 0.850
 Steel:
 Shear: 0.850
 Steel:
 Bearing Stiffeners: 0.850

No LRFD Factors specified.

Bridge Alternatives End Span 1 (or 3) - Bridge Alt.

Reference Line

Reference Line Length: (ft)
 Starting Station: (ft)
 Bearing: N 90° 0' 0.00" E
Global Positioning
 Distance: 0.000 (ft)

Offset: 0.000 (ft)
Elevation: (ft)

Structures

Name: Exist. EXT Span 1(or 3) SuperStr
Description:

Structure Alternatives

Name: Exist. END Span 1(or 3) Alt.
Description:
Superstructure Definition: End Span 1 (or 3) - PS Conc PSU

Bridge Alternatives INT Span 2 - Bridge Alt.

Reference Line

Reference Line Length: (ft)
Starting Station: (ft)
Bearing: N 90^ 0' 0.00" E

Global Positioning

Distance: 0.000 (ft)
Offset: 0.000 (ft)
Elevation: (ft)

Structures

Name: Exist. INT Span 2 Superstruct.
Description:

Structure Alternatives

Name: Exist. INT Span 2 Alt.
Description:
Superstructure Definition: INT Span 2 - PS Conc PSU

Superstructure Definition End Span 1 (or 3) - PS Conc PSU

Definition

Units: US Customary
Number of spans: 1
Number of girders: 11

Length
Span (ft)
1 28.2917

Frame Structure Simplified Definition:

Support Frame Connection

1

2

Girder Spacing Display Type: Perpendicular

Average Humidity: 70.000 (%)

Analysis

Default Library Factors

Factor Override

Analysis Module

Analysis Method: ASD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module:

Analysis Module Component:

Properties:

Default rating method: LFD

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Structure Framing Plan Details

Layout

	Skew	
Support	(Degrees)	
1	0.0000	
2	0.0000	
Girder Spacing Orientation:	Perpendicular	

Girder	Girder Spacing	
Bay	Start	End
	(ft)	(ft)

1	3.0000	3.0000
2	3.0000	3.0000
3	3.0000	3.0000
4	3.0000	3.0000
5	3.0000	3.0000
6	3.0000	3.0000
7	3.0000	3.0000
8	3.0000	3.0000
9	3.0000	3.0000
10	3.0000	3.0000

Diaphragms

Girder Bay 1

Girder Bay 2

Girder Bay 3

Girder Bay 4

Girder Bay 5

Girder Bay 6

Girder Bay 7

Girder Bay 8

Girder Bay 9

Girder Bay 10

Structure Typical Section

Deck

Left start width:	18.00	(ft)
Left end width:	18.00	(ft)
Right start width:	15.00	(ft)
Right end width:	15.00	(ft)
Left start overhang:	1.50	(ft)
Left end overhang:	1.50	(ft)

Deck (Cont'd)

Deck concrete:

Total deck thickness: (in)

Deck crack control parameter: (kip/in)

Sustained modular ratio factor: 3.000

Railing

Name	Load Case	Measure To	Measured From	Distance At Start	Distance At End	Front Face Orientation
Conc Guar...	DC1 - R...		Left Ed...	0.00	0.00	Right
Conc Guar...	DC1 - R...		Right E...	0.00	0.00	Left

Sidewalk

Width	Thickness At End	Material	Load Case	Measure to	Measured From	At Start
60.0000	11.4375	Class A...	DC1 - C...		Left Ed...	0.00 ...
24.0000	10.5630	Class A...	DC1 - C...		Right E...	0.00 ...

Lane Position

Offset Left Start: -13.00 (ft)

Offset Left End: -13.00 (ft)

Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)
 Offset Left Start: 13.00 (ft)
 Offset Left End: 13.00 (ft)
 Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)

Wearing Surface

Wearing surface material: Asphalt
 Description: Asphalt Wearing Surface
 Wearing surface thickness: 1.1670 (in)
 Wearing surface density: 145.000 (pcf)
 Load case: DW - A.W.S.

Load Case Description

Load Case Name	Description	Stage	Type	Time (Days)
DC1 - Railing	DC acting on non-comp...	Non-composite (Sta...		D,DC
DC1 - Curb	DC acting on non-comp...	Non-composite (Sta...		D,DC
DW - A.W.S.	DW acting on long-ter...	Composite (long te...		D,DW

Superstructure Loads

DL Distribution

Stage 1 Dead Load Distribution: Tributary Area
 Stage 2 Dead Load Distribution: Uniformly to All Girders

Stiffener Definitions

Stress Limits

Name: PS Conc Stress Limits

Description:

Concrete material: Class P (5000)
 Initial allowable tension (LFD): 0.190 (ksi)
 Initial allowable compression (LFD): 2.400 (ksi)
 Final allowable slab compression (LFD): (ksi)
 Final allowable tension (LFD): 0.425 (ksi)
 Final allowable DL compression (LFD): 2.000 (ksi)
 Final allowable compression (LFD): 3.000 (ksi)
 Final allowable compression (LL + 1/2(Pe+DL)) (LFD): 2.000 (ksi)
 Initial allowable tension (LRFD): 0.190 (ksi)
 Initial allowable compression (LRFD): 2.600 (ksi)
 Final allowable slab compression (LRFD): (ksi)
 Final allowable tension (LRFD): 0.425 (ksi)
 Final allowable DL compression (LRFD): 2.250 (ksi)
 Final allowable compression (LRFD): 3.000 (ksi)
 Final allowable compression (LL + 1/2(Pe+DL)) (LRFD): 2.000 (ksi)

Prestress Properties

Name: PS Strands Properties

General Pretress Data

Prestressing Strand:	7/16" (7W-250) SR
Loss Method:	AASHTO Approximate
Jacking stress ratio:	0.700
Transfer stress ratio:	
Transfer time:	24.0 <i>(Hours)</i>
AASHTO - Dead load percent:	0.0 <i>(%)</i>

Loss Data - PCI

PCI - Maturity coefficient:	
PCI - Ultimate creep loss:	<i>(ksi)</i>
PCI - Ultimate shrinkage loss:	<i>(ksi)</i>
PCI - Additional time 1:	<i>(Days)</i>
PCI - Additional time 2:	<i>(Days)</i>
PCI - Additional time 3:	<i>(Days)</i>
PCI - Additional time 4:	<i>(Days)</i>
PCI - Additional time 5:	<i>(Days)</i>
PCI - Additional time 6:	<i>(Days)</i>
PCI - Additional time 7:	<i>(Days)</i>
PCI - Additional time 8:	<i>(Days)</i>
PCI - Additional time 9:	<i>(Days)</i>
PCI - Additional time 10:	<i>(Days)</i>

Loss Data - Lump-sum

Lump-sum - Composite loss:	<i>(ksi)</i>
Lump-sum - Continuous loss:	<i>(ksi)</i>
Lump-sum - Final loss:	<i>(ksi)</i>

Shear Reinforcement Definitions - Vertical

Name:	#4 Bent Shear Reinf.
Vertical Reinforcement:	Grade 40
Vertical Rebar:	4
Number of legs (Vertical):	3.00
Inclination angle alpha (Vertical):	90.0 <i>(Degrees)</i>

Shear Reinforcement Definitions - Horizontal

Name:	#3 - 2'-7" long
Reinforcement (Horz. 1):	Grade 40
Rebar (Horz. 1):	3
Number of legs (Horz. 1):	1.00
Inclination angle alpha (Horz. 1):	90.0 <i>(Degrees)</i>
Reinforcement (Horz. 2):	
Rebar (Horz. 2):	
Number of legs (Horz. 2):	
Inclination angle alpha (Horz. 2):	90.0 <i>(Degrees)</i>

Member G1

Link with: None

Description:

Existing:	17"x36" EXT PSU -
Current:	17"x36" EXT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" EXT PSU

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:

Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.85)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber NA

Default Materials

Deck concrete: Class A (3000)

Deck reinforcement: Grade 40

Beam concrete: Class P (5000)

Beam reinforcement: Grade 40

Stirrup reinforcemt: Grade 40

Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)
 All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.100	0.100	0.100	0.100
Multi-Lane	0.100	0.100	0.100	0.100

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Deflectio...	0.100	0.100
0.00	28.292	Moment	0.100	0.100
0.00	28.292	Shear	0.100	0.100

Shrinkage/Time

Deck curing method: Moist-cured
 Deck drying time: 3.000 (Days)
 Consider deck differential shrinkage loads: FALSE
 Beam Curing method: Steam-cured
 Curing time: 20.00 (Days)
 Service life: 75.00 (Years)
 Analysis time: 54.00 (Years)
 Composite time: 60.00 (Days)
 Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right Projection
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			
	Right						
1	Left	1	9	Straight/Debonded			
	Right						
1	Left	1	10	Straight/Debonded			
	Right						
1	Left	1	11	Straight/Debonded			

1	Left Right	1	14	Straight/Debonded
1	Left Right	1	15	Straight/Debonded
1	Left Right	1	16	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.62	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.62	1	8.0000	

#3 - 2'-7" long	1	27.29	4	6.0000
-----------------	---	-------	---	--------

Member G2

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:
LFD: 2002 AASHTO Std. Specifications(CD=0.85)

ASD Factors

	Inventory	Operating
Structural steel		
Concrete		
PS Concrete Comp.		
PS Concrete Tens.		
PS Moment Cap.		
Reinforcement		
Bearing Stiffener		
Stirrup		
Timber	NA	

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)

Beam reinforcement: Grade 40
 Stirrup reinforcemt: Grade 40
 Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.167	0.167	0.167	0.167
Multi-Lane	0.167	0.167	0.167	0.167

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Deflectio...	0.167	0.200
0.00	28.292	Moment	0.167	0.200
0.00	28.292	Shear	0.167	0.200

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left	Right
	Projection	Creep		Projection	
				(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			

1	Right	1	9	Straight/Debonded
1	Left Right	1	10	Straight/Debonded
1	Left Right	1	11	Straight/Debonded
1	Left Right	1	14	Straight/Debonded
1	Left Right	1	15	Straight/Debonded
1	Left Right	1	16	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.62	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.62	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G3

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: *(kip/ft)*

Additional Self Load %: 1.0 *(%)*

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.85)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup
Timber NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	1.000	1.000	1.000	1.000
Multi-Lane	1.000	1.000	1.000	1.000

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Deflectio...	0.500	0.600
0.00	28.292	Moment	0.500	0.600
0.00	28.292	Shear	0.500	0.600

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span Prestress Shape Concrete Material Prestress Properties Left Right

	Use	n		Projection
	Projection	Creep		
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	(in) (in) 6.0000 8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	0	-0.750	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						

1		1	6	Straight/Debonded
	Left			
	Right			
1		1	7	Straight/Debonded
	Left			
	Right			
1		1	8	Straight/Debonded
	Left			
	Right			
1		1	9	Straight/Debonded
	Left			
	Right			
1		1	10	Straight/Debonded
	Left			
	Right			
1		1	11	Straight/Debonded
	Left			
	Right			
1		1	14	Straight/Debonded
	Left			
	Right			
1		1	15	Straight/Debonded
	Left			
	Right			
1		1	16	Straight/Debonded
	Left			
	Right			
1		3	1	Straight/Debonded
	Left			
	Right			
1		3	16	Straight/Debonded
	Left			
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Extends into Deck
------------------------	------------	-------------------	------------------	---------	----------------------

#4 Bent Shear R...	1	(ft) 0.21	4	(in) 6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.62	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Composite Length
		(ft)		(in)	(ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.62	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G4

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
	(ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G5

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
	(ft)
1	28.291666

Support	Frame Connection
---------	------------------

1
2

Pedestrian load: *(lb/ft)*

Member G6

Link with: G3

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length <i>(ft)</i>
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: *(lb/ft)*

Member G7

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length <i>(ft)</i>
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: *(lb/ft)*

Member G8

Link with: G9

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G9

Link with: None

Description:

Existing: 17"x36" INT PSU - w/ Post Tensioning -
 Current: 17"x36" INT PSU - w/ Post Tensioning -
 Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU - w/ Post Tensioning

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: *(kip/ft)*

Additional Self Load %: 1.0 *(%)*

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.90)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup
Timber NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.533	0.000	0.533	0.182
Multi-Lane	0.533	0.000	0.533	0.364

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Moment	0.296	0.273
0.00	28.292	Shear	0.296	0.273
0.00	28.292	Deflectio...	0.109	0.182

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span Prestress Shape Concrete Material Prestress Properties Left Right

	Use	n		Projection
	Projection	Creep		
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	(in) (in) 6.0000 8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	0	-0.750	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
Bar		Bar				
No.			Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						

1	Left	1	6	Straight/Debonded
	Right			
1	Left	1	7	Straight/Debonded
	Right			
1	Left	1	8	Straight/Debonded
	Right			
1	Left	1	9	Straight/Debonded
	Right			
1	Left	1	10	Straight/Debonded
	Right			
1	Left	1	11	Straight/Debonded
	Right			
1	Left	1	14	Straight/Debonded
	Right			
1	Left	1	15	Straight/Debonded
	Right			
1	Left	1	16	Straight/Debonded
	Right			
1	Left	3	1	Straight/Debonded
	Right			
1	Left	3	16	Straight/Debonded
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Extends into Deck
------------------------	------------	-------------------	------------------	---------	----------------------

#4 Bent Shear R...	1	(ft) 0.21	4	(in) 6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.62	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Composite Length
		(ft)		(in)	(ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.62	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G10

Link with: G9

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length
	(ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G11

Link with: G1

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
	(ft)
1	28.291666

Support	Frame Connection
---------	------------------

1
2

Pedestrian load: (lb/ft)

Superstructure Definition INT Span 2 - PS Conc PSU

Definition

Units: US Customary

Number of spans: 1

Number of girders: 11

Length

Span (ft)

1 38.5000

Frame Structure Simplified Definition:

Support Frame Connection

1

2

Girder Spacing Display Type: Perpendicular

Average Humidity: 70.000 (%)

Analysis

Default Library Factors

Factor Override

Analysis Module

Analysis Method: ASD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module:

Analysis Module Component:

Properties:

Default rating method: LFD

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Structure Framing Plan Details

Layout

Skew

Support (Degrees)

1 0.0000

2 0.0000

Girder Spacing Orientation: Perpendicular

Girder	Girder Spacing	
Bay	Start	End
	(ft)	(ft)
1	3.0000	3.0000
2	3.0000	3.0000
3	3.0000	3.0000
4	3.0000	3.0000
5	3.0000	3.0000
6	3.0000	3.0000
7	3.0000	3.0000
8	3.0000	3.0000
9	3.0000	3.0000
10	3.0000	3.0000

Diaphragms

Girder Bay 1

Girder Bay 2

Girder Bay 3

Girder Bay 4

Girder Bay 5

Girder Bay 6

Girder Bay 7

Girder Bay 8

Girder Bay 9

Girder Bay 10

Structure Typical Section

Deck

Left start width: 18.00 (ft)

Left end width: 18.00 (ft)

Right start width: 15.00 (ft)

Right end width: 15.00 (ft)

Left start overhang: 1.50 (ft)

Left end overhang: 1.50 (ft)

Deck (Cont'd)

Deck concrete:

Total deck thickness: (in)

Deck crack control parameter: (kip/in)

Sustained modular ratio factor: 3.000

Railing

Name	Load Case	Measure To	Measured From	Distance At Start	Distance At End	Front Face Orientation
Conc Guar...	DC1 - R...		Left Ed...	0.00	0.00	Right
Conc Guar...	DC1 - R...		Right E...	0.00	0.00	Left

Sidewalk

Width	Thickness At End	Material	Load Case	Measure to	Measured From	At Start
60.0000	11.4375	Class A...	DC1 - C...		Left Ed...	0.00 ...
24.0000	10.5630	Class A...	DC1 - C...		Right E...	0.00 ...

Lane Position

Offset Left Start: -13.00 (ft)

Offset Left End: -13.00 (ft)

Offset Right Start: 0.00 (ft)

Offset Right End: 0.00 (ft)

Offset Left Start: 13.00 (ft)

Offset Left End: 13.00 (ft)

Offset Right Start: 0.00 (ft)

Offset Right End: 0.00 (ft)

Wearing Surface

Wearing surface material: Asphalt

Description: Asphalt Wearing Surface

Wearing surface thickness: 1.1670 (in)

Wearing surface density: 145.000 (pcf)

Load case: DW - A.W.S.

Load Case Description

Load Case Name	Description	Stage	Type	Time (Days)
DC1 - Railing	DC acting on non-comp...	Non-composite (Sta...		D,DC
DC1 - Curb	DC acting on non-comp...	Non-composite (Sta...		D,DC
DW - A.W.S.	DW acting on long-ter...	Composite (long te...		D,DW

Superstructure Loads

DL Distribution

Stage 1 Dead Load Distribution: Tributary Area

Stage 2 Dead Load Distribution: Uniformly to All Girders

Stiffener Definitions

Stress Limits

Name: PS Conc Stress Limits

Description:

Concrete material:	Class P (5000)	
Initial allowable tension (LFD):	0.190	(ksi)
Initial allowable compression (LFD):	2.400	(ksi)
Final allowable slab compression (LFD):		(ksi)
Final allowable tension (LFD):	0.425	(ksi)
Final allowable DL compression (LFD):	2.000	(ksi)
Final allowable compression (LFD):	3.000	(ksi)
Final allowable compression (LL + 1/2(Pe+DL)) (LFD):	2.000	(ksi)
Initial allowable tension (LRFD):	0.190	(ksi)
Initial allowable compression (LRFD):	2.600	(ksi)
Final allowable slab compression (LRFD):		(ksi)
Final allowable tension (LRFD):	0.425	(ksi)
Final allowable DL compression (LRFD):	2.250	(ksi)
Final allowable compression (LRFD):	3.000	(ksi)
Final allowable compression (LL + 1/2(Pe+DL)) (LRFD):	2.000	(ksi)

Prestress Properties

Name: **PS Strands Properties**

General Pretress Data

Prestressing Strand:	7/16" (7W-250) SR
Loss Method:	AASHTO Approximate
Jacking stress ratio:	0.700
Transfer stress ratio:	
Transfer time:	24.0 (Hours)
AASHTO - Dead load percent:	0.0 (%)

Loss Data - PCI

PCI - Maturity coefficient:	
PCI - Ultimate creep loss:	(ksi)
PCI - Ultimate shrinkage loss:	(ksi)
PCI - Additional time 1:	(Days)
PCI - Additional time 2:	(Days)
PCI - Additional time 3:	(Days)
PCI - Additional time 4:	(Days)
PCI - Additional time 5:	(Days)
PCI - Additional time 6:	(Days)
PCI - Additional time 7:	(Days)
PCI - Additional time 8:	(Days)
PCI - Additional time 9:	(Days)
PCI - Additional time 10:	(Days)

Loss Data - Lump-sum

Lump-sum - Composite loss:	(ksi)
Lump-sum - Continuous loss:	(ksi)
Lump-sum - Final loss:	(ksi)

Shear Reinforcement Definitions - Vertical

Name:	#4 Bent Shear Reinf.
Vertical Reinforcement:	Grade 40
Vertical Rebar:	4
Number of legs (Vertical):	3.00

Inclination angle alpha (Vertical): 90.0 (Degrees)

Shear Reinforcement Definitions - Horizontal

Name: #3 - 2'-7" long
Reinforcement (Horz. 1): Grade 40
Rebar (Horz. 1): 3
Number of legs (Horz. 1): 1.00
Inclination angle alpha (Horz. 1): 90.0 (Degrees)
Reinforcement (Horz. 2):
Rebar (Horz. 2):
Number of legs (Horz. 2):
Inclination angle alpha (Horz. 2): 90.0 (Degrees)

Member G1

Link with: None

Description:

Existing: 17"x36" EXT PSU -
Current: 17"x36" EXT PSU -
Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				

Member Alternative 17"x36" EXT PSU

Description:

Description

Material Type: Prestressed Concrete
 Girder Type: PS Precast Box
 Member units: US Customary
 Girder property input method: Schedule based
 Additional Self Load: (kip/ft)
 Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
 Analysis Module: AASHTO ASD
 Analysis Module Component:
 Properties:

Analysis Method: LFD
 Analysis Module: AASHTO LFD
 Analysis Module Component:
 Properties:

Analysis Method: LRFD
 Analysis Module: AASHTO LRFD
 Analysis Module Component:
 Properties:

Analysis Method: LRFR
 Analysis Module: AASHTO LRFR
 Analysis Module Component:
 Properties:

Analysis Method: Distribution Factors
 Analysis Module: Legacy BrR Dist Fact
 Analysis Module Component:
 Properties:

Default rating method: LRFR
 LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.90)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.
Reinforcement
Bearing Stiffener
Stirrup
Timber NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.100	0.100	0.100	0.100
Multi-Lane	0.100	0.100	0.100	0.100

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	38.500	Deflectio...	0.100	0.100
0.00	38.500	Moment	0.100	0.100
0.00	38.500	Shear	0.100	0.100

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left Projection	Right
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information**Strand Layout**

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						

1		1	3	Straight/Debonded
	Left			
	Right			
1		1	4	Straight/Debonded
	Left			
	Right			
1		1	5	Straight/Debonded
	Left			
	Right			
1		1	6	Straight/Debonded
	Left			
	Right			
1		1	7	Straight/Debonded
	Left			
	Right			
1		1	8	Straight/Debonded
	Left			
	Right			
1		1	9	Straight/Debonded
	Left			
	Right			
1		1	10	Straight/Debonded
	Left			
	Right			
1		1	11	Straight/Debonded
	Left			
	Right			
1		1	12	Straight/Debonded
	Left			
	Right			
1		1	13	Straight/Debonded
	Left			
	Right			
1		1	14	Straight/Debonded
	Left			
	Right			
1		1	15	Straight/Debonded
	Left			
	Right			
1		1	16	Straight/Debonded
	Left			
	Right			
1		2	1	Straight/Debonded
	Left			
	Right			
1		2	2	Straight/Debonded
	Left			
	Right			
1		2	3	Straight/Debonded
	Left			

1	Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.96...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Composite Length
------------------------	------------	-------------------	------------------	---------	---------------------

#3 - 2'-7" long	1	(ft) 0.21	4	(in) 6.0000	(ft)
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G2

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:
LFD: 2002 AASHTO Std. Specifications(CD=0.90)

ASD Factors

Inventory Operating

Structural steel
Concrete
PS Concrete Comp.
PS Concrete Tens.
PS Moment Cap.
Reinforcement
Bearing Stiffener
Stirrup
Timber

NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.167	0.167	0.167	0.167
Multi-Lane	0.167	0.167	0.167	0.167

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	38.500	Deflectio...	0.167	0.200
0.00	38.500	Moment	0.167	0.200
0.00	38.500	Shear	0.167	0.200

Shrinkage/Time

Deck curing method: Moist-cured
Deck drying time: 3.000 (Days)
Consider deck differential shrinkage loads: FALSE
Beam Curing method: Steam-cured
Curing time: 20.00 (Days)
Service life: 75.00 (Years)
Analysis time: 54.00 (Years)
Composite time: 60.00 (Days)
Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left Projection	Right Projection
		Creep			

1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	(in) (in) 8.5000	8.5000
---	---------------------	-----------------------------	------------------	---------------------	--------

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support			Right Support	
Bar	Bar	Distance	Bar	Bar	Material	Distance
No.		Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	4	Straight/Debonded			
	Right						

1		1	5	Straight/Debonded
	Left			
	Right			
1		1	6	Straight/Debonded
	Left			
	Right			
1		1	7	Straight/Debonded
	Left			
	Right			
1		1	8	Straight/Debonded
	Left			
	Right			
1		1	9	Straight/Debonded
	Left			
	Right			
1		1	10	Straight/Debonded
	Left			
	Right			
1		1	11	Straight/Debonded
	Left			
	Right			
1		1	12	Straight/Debonded
	Left			
	Right			
1		1	13	Straight/Debonded
	Left			
	Right			
1		1	14	Straight/Debonded
	Left			
	Right			
1		1	15	Straight/Debonded
	Left			
	Right			
1		1	16	Straight/Debonded
	Left			
	Right			
1		2	1	Straight/Debonded
	Left			
	Right			
1		2	2	Straight/Debonded
	Left			
	Right			
1		2	3	Straight/Debonded
	Left			
	Right			
1		2	4	Straight/Debonded
	Left			
	Right			
1		2	5	Straight/Debonded
	Left			

1	Right	2	6	Straight/Debonded
1	Left			
1	Right	3	1	Straight/Debonded
1	Left			
1	Right	3	7	Straight/Debonded
1	Left			
1	Right	3	10	Straight/Debonded
1	Left			
1	Right	3	16	Straight/Debonded
	Left			
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.95...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G3

Link with: None

Description:

Existing: 17"x36" INT PSU - w/ Conc Repair Only -

Current: 17"x36" INT PSU - w/ Conc Repair Only -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU - w/ Conc Repair Only

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.90)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber

NA

Default Materials

Deck concrete: Class A (3000)

Deck reinforcement: Grade 40

Beam concrete: Class P (5000)

Beam reinforcement: Grade 40

Stirrup reinforcemt: Grade 40
 Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	1.000	1.000	1.000	1.000
Multi-Lane	1.000	1.000	1.000	1.000

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	38.500	Deflectio...	0.500	0.600
0.00	38.500	Moment	0.500	0.600
0.00	38.500	Shear	0.500	0.600

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right Projection
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Support Distance Support Distance

Number	on Left, SL (in)	on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support			Right Support	
Bar	Bar	Distance	Bar	Bar	Material	Distance
No.		Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	4	Straight/Debonded			
	Right						
1	Left	1	5	Straight/Debonded			
	Right						
1	Left	1	12	Straight/Debonded			
	Right						

1	Left	1	13	Straight/Debonded
	Right			
1	Left	1	14	Straight/Debonded
	Right			
1	Left	1	15	Straight/Debonded
	Right			
1	Left	1	16	Straight/Debonded
	Right			
1	Left	2	1	Straight/Debonded
	Right			
1	Left	2	2	Straight/Debonded
	Right			
1	Left	2	4	Straight/Debonded
	Right			
1	Left	2	5	Straight/Debonded
	Right			
1	Left	2	6	Straight/Debonded
	Right			
1	Left	3	1	Straight/Debonded
	Right			
1	Left	3	7	Straight/Debonded
	Right			
1	Left	3	10	Straight/Debonded
	Right			
1	Left	3	16	Straight/Debonded
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636

1	29.95...	8.96	1	1.0000	0.1636
---	----------	------	---	--------	--------

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G4

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G5

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G6

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G7

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G8

Link with: None

Description:

Existing: 17"x36" INT PSU -
Current: 17"x36" INT PSU -
Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:

Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.85)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber

NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	1.000	1.000	1.000	1.000
Multi-Lane	1.000	1.000	1.000	1.000

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	38.500	Deflectio...	0.500	0.600
0.00	38.500	Moment	0.500	0.600
0.00	38.500	Shear	0.500	0.600

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
-------------------	---	--

1

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information**Strand Layout**

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	4	Straight/Debonded			
	Right						
1	Left	1	5	Straight/Debonded			
	Right						
1	Left	1	12	Straight/Debonded			
	Right						
1	Left	1	13	Straight/Debonded			
	Right						

1	Left	1	14	Straight/Debonded
	Right			
1	Left	1	15	Straight/Debonded
	Right			
1	Left	1	16	Straight/Debonded
	Right			
1	Left	2	1	Straight/Debonded
	Right			
1	Left	2	2	Straight/Debonded
	Right			
1	Left	2	4	Straight/Debonded
	Right			
1	Left	2	5	Straight/Debonded
	Right			
1	Left	2	6	Straight/Debonded
	Right			
1	Left	3	1	Straight/Debonded
	Right			
1	Left	3	7	Straight/Debonded
	Right			
1	Left	3	10	Straight/Debonded
	Right			
1	Left	3	16	Straight/Debonded
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G9

Link with: G8

Description:

Existing: 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning -

Current: 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G10

Link with: None

Description:

Existing: 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning -

Current: 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning -

Number of Spans: 1

Span Number	Span Length (ft)
-------------	---------------------

1 38.500000

Support Frame Connection

1

2

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
-------------------	--------------------	------------------	-------------------------	----------------

1

2

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
-------------------	---------------------------	---------------------------	----------------------------	---------------------------------

1

2

Member Alternative 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CD=0.90)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber

NA

Default Materials

Deck concrete: Class A (3000)

Deck reinforcement: Grade 40

Beam concrete: Class P (5000)

Beam reinforcement: Grade 40

Stirrup reinforcement: Grade 40

Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes Loaded	Shear	Shear at Supports	Moment	Deflection
1 Lane	0.527	0.000	0.527	0.182
Multi-Lane	0.527	0.000	0.527	0.364

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	38.500	Moment	0.254	0.256
0.00	38.500	Shear	0.254	0.256
0.00	38.500	Deflectio...	0.109	0.182

Shrinkage/Time

Deck curing method: Moist-cured
Deck drying time: 3.000 (Days)
Consider deck differential shrinkage loads: FALSE
Beam Curing method: Steam-cured
Curing time: 20.00 (Days)
Service life: 75.00 (Years)
Analysis time: 54.00 (Years)
Composite time: 60.00 (Days)
Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection (in)	Right Projection (in)
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type: Monolithic
Interface width: (in)
Deck cohesion factor: 0.400 (ksi)
Deck friction factor: 1.400

Continuity Diaphragm

Span	Material	Left Support	Bar	Bar	Right Support	Distance
No.	Bar	Distance	Bar	Count	Material	Count Size

Prestressing Force Information**Strand Layout**

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
1	Right	1	2	Straight/Debonded			
1	Left	1	3	Straight/Debonded			
1	Right	1	4	Straight/Debonded			
1	Left	1	5	Straight/Debonded			
1	Right	1	12	Straight/Debonded			
1	Left	1	13	Straight/Debonded			
1	Right	1	14	Straight/Debonded			
1	Left	1	15	Straight/Debonded			
1	Right	1	16	Straight/Debonded			

1	Right	2	1	Straight/Debonded
1	Left Right	2	2	Straight/Debonded
1	Left Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE

#4 Bent Shear R...	1	37.71	4	6.0000	FALSE
--------------------	---	-------	---	--------	-------

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance <i>(ft)</i>	Number Spaces	Spacing <i>(in)</i>	Composite Length <i>(ft)</i>
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G11

Link with: G1

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length <i>(ft)</i>
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: *(lb/ft)*

Username: BrR

Date: Wednesday, September 22, 2021 10:06:29

Bridge ID 874294 Matheson Hmck Bridge over Matheson Hammock Canal

NBI Structure ID (8): 874294

Description: Rating by YRA, from As-built plans, 9/14/2021

Three spans (30'-40'-30') non-composite PS Concrete voided slab unit superstructure comprised of eleven (11) 17"x36" units. Deck width is 35'-0" out-to-out with a 26'-0" clear roadway width.

Wearing surface is present along the bridge with an average thickness of 1.167" along end spans 1 and 3, and 1.292" for interior span 2.

The load rating analysis for the prestressed voided slab units was initially performed using the Load and Resistance factor Rating methodology in accordance with the AASHTO LRFD Bridge Design Specifications (9th edition, 2020), the Manual for Bridge Evaluation (3rd edition with interims through 2019), and the FDOT Bridge Load Rating Manual (January 2021). However, the resulting design and legal rating factors were less than 1, which granted the need to evaluate the structure using the Load Factor Rating methodology.

Description

Location:	Matheson Hammock Park
Total Length:	100.33 <i>(ft)</i>
Facility Carried:	Matheson Hmk Road
Route Number:	00000
Feature Intersected:	Matheson Hammock Canal
Mi Post:	0.08 <i>(mi)</i>
Units:	US Customary
Year Built:	1967
Recent ADTT:	11
District:	District 6
County:	
Owner:	County Hwy Agency
National Highway System:	0 Not on NHS
Functional Class:	09 Rural Local

Global Reference Point

X Coordinate:	0.000 <i>(ft)</i>
Y Coordinate:	0.000 <i>(ft)</i>
Elevation:	<i>(ft)</i>
Longitude:	80.26 <i>(Degrees)</i>
Latitude:	25.68 <i>(Degrees)</i>

Materials

No steel materials.

Concrete

Name:	Class P (5000)
Description:	Class 5000 cement concrete
Specified compressive strength at 28 days (f _c):	5.000 <i>(ksi)</i>

Initial specified compressive strength (f'ci):	4.000 (ksi)
Coefficient of thermal expansion:	0.0000060000 (1/F)
Density (for dead loads):	0.150 (kef)
Density (for modulus of elasticity):	0.145 (kef)
Std Modulus of elasticity (Ec):	4074.28 (ksi)
LRFD Modulus of elasticity (Ec):	4291.19 (ksi)
Poisson's ratio:	0.200
Modulus of rupture:	0.537 (ksi)
Shear factor:	1.000
Composition of concrete:	Normal
Std Initial modulus of elasticity (Eci):	3644.15 (ksi)
LRFD Initial modulus of elasticity (Eci):	3986.55 (ksi)
Splitting tensile strength (fct):	(ksi)

Name:	Class A (3000)
Description:	Class A cement concrete (3000 psi)
Specified compressive strength at 28 days (f'c):	3.000 (ksi)
Initial specified compressive strength (f'ci):	(ksi)
Coefficient of thermal expansion:	0.0000060000 (1/F)
Density (for dead loads):	0.150 (kef)
Density (for modulus of elasticity):	0.145 (kef)
Std Modulus of elasticity (Ec):	3150.39 (ksi)
LRFD Modulus of elasticity (Ec):	3617.02 (ksi)
Poisson's ratio:	0.200
Modulus of rupture:	0.416 (ksi)
Shear factor:	1.000
Composition of concrete:	Normal
Std Initial modulus of elasticity (Eci):	(ksi)
LRFD Initial modulus of elasticity (Eci):	(ksi)
Splitting tensile strength (fct):	(ksi)

Reinforcing Steel

Name:	Grade 40
Description:	40 ksi reinforcing steel
Specified yield strength (Fy):	40.000 (ksi)
Modulus of elasticity (Es):	29000.00 (ksi)
Ultimate strength (Fu):	70.000 (ksi)
Type:	Plain

Prestressing Strand

Name:	7/16" (7W-250) SR
Description:	Stress relieved 7/16"/Seven Wire/fpu = 250
Specified yield strength (Fy):	212.500 (ksi)
Ultimate Tensile strength (Fu):	250.000 (ksi)
Modulus of elasticity (Es):	28500.00 (ksi)
Load per unit length:	0.367 (lb/ft)
Cross sectional area (A):	0.108 (in^2)
Nominal diameter (d):	0.4375 (in)
Transfer length (Std):	21.8750 (in)
Transfer length (LRFD):	26.2500 (in)

Type:
Epoxy coated:

Stress Relieved
FALSE

No timber materials.

Beam Shapes

Steel Shapes

No steel shapes.

Prestressed Shapes

No prestressed I shapes.

Prestressed Box Shapes

Name: 17"x36" PSU
Description: 17"x36" Prestressed Slab Unit for units E thru G
Type: Circular Void
Nominal Depth: 17.0000 (in)
Depth (d): 17.0000 (in)
Top flange width: 35.0000 (in)
Bottom flange width: 36.0000 (in)
Three-void (D1, D2, D1) shape: FALSE
Circular void diameter: 10.0000 (in)
Distance to CG of void(s) from bottom: 9.0000 (in)
Number of circular voids: 2
Center to center distance of voids: 16.0000 (in)
Vertical location of shear key: 2.0000 (in)
Shear key height: 6.0000 (in)
Shear key depth: 1.5000 (in)
Nominal load: 457.107 (lb/ft)
Cross sectional area: 438.822 (in²)
Ixx: 13330.101 (in⁴)
CG from bottom: 8.1667 (in)
Bottom Sxx: 1632.246 (in³)
Top Sxx: 1509.078 (in³)
Volume/Surface Ratio: 3.175 (in)
Half Depth Area for Positive Flexure: (in²)
Half Depth Area for Negative Flexure: (in²)
St. Venant's Torsional Constant: 14593.772 (in⁴)

Strand Grid

Row Number	Number of Strands	Vertical Location (in)	Horizontal Spacing (in)
1	16	2.5000	2.0000

2	6	4.5000	2.0000
3	16	14.5000	2.0000

No prestressed U shapes.

No prestressed tee shapes.

Timber Shapes

No timber shapes.

Appurtenances

No concrete railings.

Railings

Name: **Conc Guardrail w/ metal Post and Rail**
Description: Conc. Post and beam guardrail with post and tube rail mounted
Effective Wind Height: 36.0000 (in)
Railing Load: 0.166 (kip/ft)
Distance From Edge to Centroid: 5.0000 (in)
Width: 10.0000 (in)

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Factors

Factors - LFD

Name: 2002 AASHTO Std. Specifications

Description: AASHTO Standard Specifications for Highway Bridges, 17th Edition, 2002

Load Factors

Load Group	Gamma D	(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.900

Reinforced concrete:

Shear: 0.850

Prestressed concrete:

Flexure: 1.000

Prestressed concrete:

Shear: 0.900

Prestressed concrete:

Flexure in Non-P/S Components: 0.900

Steel:

Flexure: 1.000

Steel:

Shear: 1.000

Steel:

Bearing Stiffeners: 1.000

Name:

2002 AASHTO Std. Specifications(CF=0.9)

Description:

AASHTO Standard Specifications for Highway Bridges,

17th Edition, 2002

Load Factors

Load Group	Gamma D		(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.810

Reinforced concrete:

Shear: 0.765

Prestressed concrete:

Flexure: 0.900

Prestressed concrete:

Shear: 0.810

Prestressed concrete:

Flexure in Non-P/S Components: 0.810

Steel:

Flexure: 0.900

Steel:

Shear: 0.900

Steel:

Bearing Stiffeners: 0.900

Name:

2002 AASHTO Std. Specifications(CF=0.95)

Description:

AASHTO Standard Specifications for Highway Bridges,

17th Edition, 2002

Load Factors

Load Group	Gamma	D	(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.855

Reinforced concrete:

Shear: 0.807

Prestressed concrete:

Flexure: 0.950

Prestressed concrete:

Shear: 0.855

Prestressed concrete:

Flexure in Non-P/S Components: 0.855

Steel:

Flexure: 0.950

Steel:

Shear: 0.950

Steel:

Bearing Stiffeners: 0.950

Name: 2002 AASHTO Std. Specifications(CF=0.85)

Description: AASHTO Standard Specifications for Highway Bridges,

17th Edition, 2002

Load Factors

Load Group	Gamma	D	(L+I)n	(L+I)p	CF	E	B
Inventory	1.300	1.000	1.670	0.000	1.000	1.000	1.000
Operating	1.300	1.000	1.000	0.000	1.000	1.000	1.000

Load Group	SF	W	WL	LF	R+S+T	EQ	ICE
Inventory	1.000	0.000	0.000	0.000	0.000	0.000	0.000
Operating	1.000	0.000	0.000	0.000	0.000	0.000	0.000

Resistance Factors

Reinforced concrete:

Flexure: 0.765

Reinforced concrete:

Shear: 0.723

Prestressed concrete:

Flexure: 0.850

Prestressed concrete:

Shear:	0.765
Prestressed concrete:	
Flexure in Non-P/S Components:	0.765
Steel:	
Flexure:	0.850
Steel:	
Shear:	0.850
Steel:	
Bearing Stiffeners:	0.850

No LRFD Factors specified.

Bridge Alternatives End Span 1 (or 3) - Bridge Alt.

Reference Line

Reference Line Length:	(ft)
Starting Station:	(ft)
Bearing:	N 90^ 0' 0.00" E

Global Positioning

Distance:	0.000 (ft)
Offset:	0.000 (ft)
Elevation:	(ft)

Structures

Name:	Exist. EXT Span 1(or 3) SuperStr
Description:	

Structure Alternatives

Name: Exist. END Span 1(or 3) Alt.

Description:

Superstructure Definition: End Span 1 (or 3) - PS Conc PSU

Bridge Alternatives INT Span 2 - Bridge Alt.

Reference Line

Reference Line Length:	(ft)
Starting Station:	(ft)
Bearing:	N 90^ 0' 0.00" E

Global Positioning

Distance:	0.000 (ft)
Offset:	0.000 (ft)
Elevation:	(ft)

Structures

Name:	Exist. INT Span 2 Superstruct.
-------	--------------------------------

Description:

Structure Alternatives

Name: Exist. INT Span 2 Alt.

Description:

Superstructure Definition: INT Span 2 - PS Conc PSU

Superstructure Definition End Span 1 (or 3) - PS Conc PSU

Definition

Units: US Customary

Number of spans: 1

Number of girders: 11

Length

Span (ft)

1 28.2917

Frame Structure Simplified Definition:

Support Frame Connection

1

2

Girder Spacing Display Type: Perpendicular

Average Humidity: 70.000 (%)

Analysis

Default Library Factors

Factor Override

Analysis Module

Analysis Method: ASD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module:

Analysis Module Component:
Properties:

Default rating method: LFD

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Structure Framing Plan Details

Layout

	Skew	
Support	(Degrees)	
1	0.0000	
2	0.0000	

Girder Spacing Orientation: Perpendicular

Girder	Girder Spacing	
Bay	Start	End
	(ft)	(ft)
1	3.0000	3.0000
2	3.0000	3.0000
3	3.0000	3.0000
4	3.0000	3.0000
5	3.0000	3.0000
6	3.0000	3.0000
7	3.0000	3.0000
8	3.0000	3.0000
9	3.0000	3.0000
10	3.0000	3.0000

Diaphragms

Girder Bay 1
Girder Bay 2
Girder Bay 3
Girder Bay 4
Girder Bay 5
Girder Bay 6
Girder Bay 7
Girder Bay 8
Girder Bay 9
Girder Bay 10

Structure Typical Section

Deck

Left start width: 18.00 (ft)

Left end width: 18.00 (ft)

Right start width: 15.00 (ft)
 Right end width: 15.00 (ft)
 Left start overhang: 1.50 (ft)
 Left end overhang: 1.50 (ft)

Deck (Cont'd)

Deck concrete:

Total deck thickness: (in)

Deck crack control parameter: (kip/in)

Sustained modular ratio factor: 3.000

Railing

Name	Load Case	Measure To	Measured From	Distance At Start	Distance At End	Front Face Orientation
Conc Guar...	DC1 - R...		Left Ed...	0.00	0.00	Right
Conc Guar...	DC1 - R...		Right E...	0.00	0.00	Left

Sidewalk

Width	Thickness At End	Material	Load Case	Measure to	Measured From	At Start
60.0000	11.4375	Class A...	DC1 - C...		Left Ed...	0.00 ...
24.0000	10.5630	Class A...	DC1 - C...		Right E...	0.00 ...

Lane Position

Offset Left Start: -13.00 (ft)
 Offset Left End: -13.00 (ft)
 Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)
 Offset Left Start: 13.00 (ft)
 Offset Left End: 13.00 (ft)
 Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)

Wearing Surface

Wearing surface material: Asphalt
 Description: Asphalt Wearing Surface
 Wearing surface thickness: 1.1670 (in)
 Wearing surface density: 145.000 (pcf)
 Load case: DW - A.W.S.

Load Case Description

Load Case Name	Description	Stage	Type	Time (Days)
DC1 - Railing	DC acting on non-comp...	Non-composite (Sta...		D,DC
DC1 - Curb	DC acting on non-comp...	Non-composite (Sta...		D,DC
DW - A.W.S.	DW acting on long-ter...	Composite (long te...		D,DW

Superstructure Loads

DL Distribution

Stage 1 Dead Load Distribution: Tributary Area

Stage 2 Dead Load Distribution: Uniformly to All Girders

Stiffener Definitions

Stress Limits

Name:

PS Conc Stress Limits

Description:

Concrete material: Class P (5000)

Initial allowable tension (LFD): 0.190 (ksi)

Initial allowable compression (LFD): 2.400 (ksi)

Final allowable slab compression (LFD): (ksi)

Final allowable tension (LFD): 0.425 (ksi)

Final allowable DL compression (LFD): 2.000 (ksi)

Final allowable compression (LFD): 3.000 (ksi)

Final allowable compression (LL + 1/2(Pe+DL)) (LFD): 2.000 (ksi)

Initial allowable tension (LRFD): 0.190 (ksi)

Initial allowable compression (LRFD): 2.600 (ksi)

Final allowable slab compression (LRFD): (ksi)

Final allowable tension (LRFD): 0.425 (ksi)

Final allowable DL compression (LRFD): 2.250 (ksi)

Final allowable compression (LRFD): 3.000 (ksi)

Final allowable compression (LL + 1/2(Pe+DL)) (LRFD): 2.000 (ksi)

Prestress Properties

Name:

PS Strands Properties

General Pretress Data

Prestressing Strand: 7/16" (7W-250) SR

Loss Method: AASHTO Approximate

Jacking stress ratio: 0.700

Transfer stress ratio:

Transfer time: 24.0 (Hours)

AASHTO - Dead load percent: 0.0 (%)

Loss Data - PCI

PCI - Maturity coefficient:

PCI - Ultimate creep loss: (ksi)

PCI - Ultimate shrinkage loss: (ksi)

PCI - Additional time 1: (Days)

PCI - Additional time 2: (Days)

PCI - Additional time 3: (Days)

PCI - Additional time 4: (Days)

PCI - Additional time 5: (Days)

PCI - Additional time 6: (Days)

PCI - Additional time 7: (Days)

PCI - Additional time 8: (Days)

PCI - Additional time 9: (Days)

PCI - Additional time 10: (Days)

Loss Data - Lump-sum

Lump-sum - Composite loss: (ksi)

Lump-sum - Continuous loss: (ksi)

Lump-sum - Final loss: (ksi)

Shear Reinforcement Definitions - Vertical

Name:

#4 Bent Shear Reinf.

Vertical Reinforcement:	Grade 40
Vertical Rebar:	4
Number of legs (Vertical):	3.00
Inclination angle alpha (Vertical):	90.0 <i>(Degrees)</i>

Shear Reinforcement Definitions - Horizontal

Name:	#3 - 2'-7" long
Reinforcement (Horz. 1):	Grade 40
Rebar (Horz. 1):	3
Number of legs (Horz. 1):	1.00
Inclination angle alpha (Horz. 1):	90.0 <i>(Degrees)</i>
Reinforcement (Horz. 2):	
Rebar (Horz. 2):	
Number of legs (Horz. 2):	
Inclination angle alpha (Horz. 2):	90.0 <i>(Degrees)</i>

Member G1

Link with: None

Description:

Existing:	17"x36" EXT PSU -
Current:	17"x36" EXT PSU -
Number of Spans:	1

Span	Span Length
Number	<i>(ft)</i>
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: *(lb/ft)*

Member Loads

Member Loads - Settlement

Support	Horizontal	Vertical	Rotational	Load Case Name
Number	<i>(in)</i>	<i>(in)</i>	<i>(Radians)</i>	
1				
2				

Support Constraints

General

Support	Support			
Number	Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" EXT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel

Concrete	
PS Concrete Comp.	
PS Concrete Tens.	
PS Moment Cap.	
Reinforcement	
Bearing Stiffener	
Stirrup	
Timber	NA

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcemt:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type:	Standard - AASHTO
-------	-------------------

LRFD Dynamic Load Allowance

Fatigue and fracture limit states:	15.0 (%)
------------------------------------	----------

All other limit states:	33.0 (%)
-------------------------	----------

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.010	0.010	0.010	0.010
Multi-Lane	0.010	0.010	0.010	0.010

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	28.292	Deflectio...	0.010	0.010
0.00	28.292	Moment	0.010	0.010
0.00	28.292	Shear	0.010	0.010

Shrinkage/Time

Deck curing method:	Moist-cured
Deck drying time:	3.000 (Days)
Consider deck differential shrinkage loads:	FALSE
Beam Curing method:	Steam-cured
Curing time:	20.00 (Days)
Service life:	75.00 (Years)
Analysis time:	54.00 (Years)
Composite time:	60.00 (Days)
Continuous time:	45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left Projection	Right
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	(in) 6.0000	(in) 8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left Right	1	1	Straight/Debonded			

1	Left	1	2	Straight/Debonded
	Right			
1	Left	1	3	Straight/Debonded
	Right			
1	Left	1	6	Straight/Debonded
	Right			
1	Left	1	7	Straight/Debonded
	Right			
1	Left	1	8	Straight/Debonded
	Right			
1	Left	1	9	Straight/Debonded
	Right			
1	Left	1	10	Straight/Debonded
	Right			
1	Left	1	11	Straight/Debonded
	Right			
1	Left	1	14	Straight/Debonded
	Right			
1	Left	1	15	Straight/Debonded
	Right			
1	Left	1	16	Straight/Debonded
	Right			
1	Left	3	1	Straight/Debonded
	Right			
1	Left	3	16	Straight/Debonded
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636

1	22.25...	6.25	1	1.0000	0.1636
---	----------	------	---	--------	--------

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.63	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.63	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G2

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

	Inventory	Operating
Structural steel		
Concrete		
PS Concrete Comp.		
PS Concrete Tens.		
PS Moment Cap.		
Reinforcement		
Bearing Stiffener		
Stirrup		
Timber	NA	

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcemt:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)				
Lanes		Shear at		
Loaded	Shear	Supports	Moment	Deflection
1 Lane	0.167	0.017	0.017	0.017
Multi-Lane	0.167	0.017	0.017	0.017

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Deflectio...	0.167	0.200
0.00	28.292	Moment	0.167	0.200
0.00	28.292	Shear	0.167	0.200

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 *(Days)*
 Consider deck differential shrinkage loads: FALSE
 Beam Curing method: Steam-cured
 Curing time: 20.00 *(Days)*
 Service life: 75.00 *(Years)*
 Analysis time: 54.00 *(Years)*
 Composite time: 60.00 *(Days)*
 Continuous time: 45.0 *(Days)*

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left	Right
	Projection	Creep		Projection	
				<i>(in)</i> <i>(in)</i>	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL <i>(in)</i>	Support Distance on Right, SR <i>(in)</i>
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance <i>(ft)</i>	Length <i>(ft)</i>
PS Conc Stress Lim...	1	0.000	29.50

Slab Interface

Deck interface type: Monolithic
 Interface width: *(in)*
 Deck cohesion factor: 0.400 *(ksi)*
 Deck friction factor: 1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			
	Right						
1	Left	1	9	Straight/Debonded			
	Right						
1	Left	1	10	Straight/Debonded			
	Right						
1	Left	1	11	Straight/Debonded			
	Right						
1	Left	1	14	Straight/Debonded			
	Right						
1	Left	1	15	Straight/Debonded			
	Right						
1	Left	1	16	Straight/Debonded			
	Right						
1	Left	3	1	Straight/Debonded			
	Right						
1	Left	3	16	Straight/Debonded			
	Right						

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.63	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.63	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G3

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:

Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber NA

Default Materials

Deck concrete: Class A (3000)

Deck reinforcement: Grade 40

Beam concrete: Class P (5000)

Beam reinforcement: Grade 40

Stirrup reinforcement: Grade 40

Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	1.000	1.000	1.000	1.000
Multi-Lane	1.000	1.000	1.000	1.000

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	28.292	Moment	0.500	0.600
0.00	28.292	Shear	0.500	0.600
0.00	28.292	Deflectio...	0.500	0.600

Shrinkage/Time

Deck curing method: Moist-cured
Deck drying time: 3.000 (Days)
Consider deck differential shrinkage loads: FALSE
Beam Curing method: Steam-cured
Curing time: 20.00 (Days)
Service life: 75.00 (Years)
Analysis time: 54.00 (Years)
Composite time: 60.00 (Days)
Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection (in)	Right Projection (in)
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	0	-0.750	29.50

Slab Interface

Deck interface type: Monolithic
Interface width: (in)
Deck cohesion factor: 0.400 (ksi)
Deck friction factor: 1.400

Continuity Diaphragm

Left Support

Right Support

Span No.	Material Bar	Distance Bar	Bar Count	Bar Size	Material	Distance
					Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			
	Right						
1	Left	1	9	Straight/Debonded			
	Right						
1	Left	1	10	Straight/Debonded			
	Right						
1	Left	1	11	Straight/Debonded			
	Right						
1	Left	1	14	Straight/Debonded			
	Right						
1	Left	1	15	Straight/Debonded			
	Right						
1	Left	1	16	Straight/Debonded			
	Right						
1		3	1	Straight/Debonded			

1	Left	3	16	Straight/Debonded
	Right			
	Left			
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.63	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.63	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G4

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Span Length

Number *(ft)*
1 28.291666

Support Frame Connection
1
2

Pedestrian load: *(lb/ft)*

Member G5

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Span Length
Number *(ft)*
1 28.291666

Support Frame Connection
1
2

Pedestrian load: *(lb/ft)*

Member G6

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Span Length
Number *(ft)*
1 28.291666

Support Frame Connection
1
2

Pedestrian load: *(lb/ft)*

Member G7

Link with: G3

Description:

Existing:
Current:
Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G8

Link with: G3
Description:

Existing:
Current:
Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G9

Link with: G3
Description:

Existing:
Current:
Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G10

Link with: None

Description:

Existing: 17"x36" INT PSU - (w/ Post Tensioning) -

Current: 17"x36" INT PSU - (w/ Post Tensioning) -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU - (w/ Post Tensioning)

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement

Bearing Stiffener

Stirrup

Timber

NA

Default Materials

Deck concrete: Class A (3000)

Deck reinforcement: Grade 40

Beam concrete: Class P (5000)

Beam reinforcement: Grade 40

Stirrup reinforcemt: Grade 40
 Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.533	0.000	0.533	0.182
Multi-Lane	0.533	0.000	0.533	0.364

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Moment	0.296	0.273
0.00	28.292	Shear	0.296	0.273
0.00	28.292	Deflectio...	0.109	0.182

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right Projection
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000	8.5000

Continuous Support Details

Support Support Distance Support Distance

Number	on Left, SL (in)	on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	0	-0.750	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support			Right Support	
Bar	Bar	Distance	Bar	Bar	Material	Distance
No.		Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			
	Right						

1	Left	1	9	Straight/Debonded
	Right			
1	Left	1	10	Straight/Debonded
	Right			
1	Left	1	11	Straight/Debonded
	Right			
1	Left	1	14	Straight/Debonded
	Right			
1	Left	1	15	Straight/Debonded
	Right			
1	Left	1	16	Straight/Debonded
	Right			
1	Left	3	1	Straight/Debonded
	Right			
1	Left	3	16	Straight/Debonded
	Right			

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.63	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.63	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Member G11

Link with: None

Description:

Existing: 17"x36" EXT PSU (w/ Post Tensioning) -

Current: 17"x36" EXT PSU (w/ Post Tensioning) -

Number of Spans: 1

Span Number	Span Length (ft)
1	28.291666

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" EXT PSU (w/ Post Tensioning)

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR
LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:
LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel
Concrete
PS Concrete Comp.
PS Concrete Tens.
PS Moment Cap.
Reinforcement
Bearing Stiffener
Stirrup

Timber

NA

Default Materials

Deck concrete: Class A (3000)
Deck reinforcement: Grade 40
Beam concrete: Class P (5000)
Beam reinforcement: Grade 40
Stirrup reinforcement: Grade 40
Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.100	0.100	0.100	0.100
Multi-Lane	0.100	0.100	0.100	0.100

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	28.292	Deflectio...	0.100	0.100
0.00	28.292	Moment	0.100	0.100
0.00	28.292	Shear	0.100	0.100

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape	Concrete Material	Prestress Properties	Left	Right
	Use	n			

	Projection	Creep		Projection
				(in) (in)
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	6.0000 8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	29.50

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support	Bar	Bar	Right Support	
Bar	Bar	Distance	Bar	Bar	Material	Distance
No.		Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						

1	Left Right	1	7	Straight/Debonded
1	Left Right	1	8	Straight/Debonded
1	Left Right	1	9	Straight/Debonded
1	Left Right	1	10	Straight/Debonded
1	Left Right	1	11	Straight/Debonded
1	Left Right	1	14	Straight/Debonded
1	Left Right	1	15	Straight/Debonded
1	Left Right	1	16	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	6.25	1	1.0000	0.1636
1	7.25...	15.00	1	1.0000	0.1636
1	22.25...	6.25	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
------------------------	------------	---------------------------	------------------	-----------------	----------------------

#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	8.0000	FALSE
#4 Bent Shear R...	1	2.88	19	15.0000	FALSE
#4 Bent Shear R...	1	26.62	1	8.0000	FALSE
#4 Bent Shear R...	1	27.29	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	8.0000	
#3 - 2'-7" long	1	2.88	19	15.0000	
#3 - 2'-7" long	1	26.62	1	8.0000	
#3 - 2'-7" long	1	27.29	4	6.0000	

Superstructure Definition INT Span 2 - PS Conc PSU

Definition

Units: US Customary

Number of spans: 1

Number of girders: 11

Length

Span (ft)

1 38.5000

Frame Structure Simplified Definition:

Support Frame Connection

1

2

Girder Spacing Display Type: Perpendicular

Average Humidity: 70.000 (%)

Analysis

Default Library Factors

Factor Override

Analysis Module

Analysis Method: ASD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module:

Analysis Module Component:

Properties:

Analysis Method: LRFR
Analysis Module:
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module:
Analysis Module Component:
Properties:

Default rating method: LFD

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Structure Framing Plan Details

Layout

Skew
Support (Degrees)
1 0.0000
2 0.0000
Girder Spacing Orientation: Perpendicular

Girder	Girder Spacing	
Bay	Start	End
	(ft)	(ft)
1	3.0000	3.0000
2	3.0000	3.0000
3	3.0000	3.0000
4	3.0000	3.0000
5	3.0000	3.0000
6	3.0000	3.0000
7	3.0000	3.0000
8	3.0000	3.0000
9	3.0000	3.0000
10	3.0000	3.0000

Diaphragms

Girder Bay 1
Girder Bay 2
Girder Bay 3
Girder Bay 4
Girder Bay 5
Girder Bay 6
Girder Bay 7

Girder Bay 8
 Girder Bay 9
 Girder Bay 10

Structure Typical Section

Deck

Left start width: 18.00 (ft)
 Left end width: 18.00 (ft)
 Right start width: 15.00 (ft)
 Right end width: 15.00 (ft)
 Left start overhang: 1.50 (ft)
 Left end overhang: 1.50 (ft)

Deck (Cont'd)

Deck concrete:
 Total deck thickness: (in)
 Deck crack control parameter: (kip/in)
 Sustained modular ratio factor: 3.000

Railing

Name	Load Case	Measure To	Measured From	Distance At Start	Distance At End	Front Face Orientation
Conc Guar...	DC1 - R...		Left Ed...	0.00	0.00	Right
Conc Guar...	DC1 - R...		Right E...	0.00	0.00	Left

Sidewalk

Width	Thickness At End	Material	Load Case	Measure to	Measured From	At Start
60.0000	11.4375	Class A...	DC1 - C...		Left Ed...	0.00 ...
24.0000	10.5630	Class A...	DC1 - C...		Right E...	0.00 ...

Lane Position

Offset Left Start: -13.00 (ft)
 Offset Left End: -13.00 (ft)
 Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)
 Offset Left Start: 13.00 (ft)
 Offset Left End: 13.00 (ft)
 Offset Right Start: 0.00 (ft)
 Offset Right End: 0.00 (ft)

Wearing Surface

Wearing surface material: Asphalt
 Description: Asphalt Wearing Surface
 Wearing surface thickness: 1.1670 (in)
 Wearing surface density: 145.000 (pcf)
 Load case: DW - A.W.S.

Load Case Description

Load Case Name	Description	Stage	Type (Days)	Time
DC1 - Railing	DC acting on non-comp...	Non-composite (Sta...		D,DC
DC1 - Curb	DC acting on non-comp...	Non-composite (Sta...		D,DC
DW - A.W.S.	DW acting on long-ter...	Composite (long te...		D,DW

Superstructure Loads

DL Distribution

Stage 1 Dead Load Distribution: Tributary Area

Stage 2 Dead Load Distribution: Uniformly to All Girders

Stiffener Definitions

Stress Limits

Name:

PS Conc Stress Limits

Description:

Concrete material: Class P (5000)

Initial allowable tension (LFD): 0.190 (ksi)

Initial allowable compression (LFD): 2.400 (ksi)

Final allowable slab compression (LFD): (ksi)

Final allowable tension (LFD): 0.425 (ksi)

Final allowable DL compression (LFD): 2.000 (ksi)

Final allowable compression (LFD): 3.000 (ksi)

Final allowable compression (LL + 1/2(Pe+DL)) (LFD): 2.000 (ksi)

Initial allowable tension (LRFD): 0.190 (ksi)

Initial allowable compression (LRFD): 2.600 (ksi)

Final allowable slab compression (LRFD): (ksi)

Final allowable tension (LRFD): 0.425 (ksi)

Final allowable DL compression (LRFD): 2.250 (ksi)

Final allowable compression (LRFD): 3.000 (ksi)

Final allowable compression (LL + 1/2(Pe+DL)) (LRFD): 2.000 (ksi)

Prestress Properties

Name:

PS Strands Properties

General Pretress Data

Prestressing Strand: 7/16" (7W-250) SR

Loss Method: AASHTO Approximate

Jacking stress ratio: 0.700

Transfer stress ratio:

Transfer time: 24.0 (Hours)

AASHTO - Dead load percent: 0.0 (%)

Loss Data - PCI

PCI - Maturity coefficient:

PCI - Ultimate creep loss: (ksi)

PCI - Ultimate shrinkage loss: (ksi)

PCI - Additional time 1: (Days)

PCI - Additional time 2: (Days)

PCI - Additional time 3: (Days)

PCI - Additional time 4: (Days)

PCI - Additional time 5: (Days)

PCI - Additional time 6: (Days)

PCI - Additional time 7: (Days)

PCI - Additional time 8: (Days)

PCI - Additional time 9: (Days)

PCI - Additional time 10: (Days)
Loss Data - Lump-sum
 Lump-sum - Composite loss: (ksi)
 Lump-sum - Continuous loss: (ksi)
 Lump-sum - Final loss: (ksi)

Shear Reinforcement Definitions - Vertical

Name: **#4 Bent Shear Reinf.**
 Vertical Reinforcement: Grade 40
 Vertical Rebar: 4
 Number of legs (Vertical): 3.00
 Inclination angle alpha (Vertical): 90.0 (Degrees)

Shear Reinforcement Definitions - Horizontal

Name: **#3 - 2'-7" long**
 Reinforcement (Horz. 1): Grade 40
 Rebar (Horz. 1): 3
 Number of legs (Horz. 1): 1.00
 Inclination angle alpha (Horz. 1): 90.0 (Degrees)
 Reinforcement (Horz. 2):
 Rebar (Horz. 2):
 Number of legs (Horz. 2):
 Inclination angle alpha (Horz. 2): 90.0 (Degrees)

Member G1

Link with: None

Description:

Existing: 17"x36" EXT PSU -
 Current: 17"x36" EXT PSU -
 Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" EXT PSU

Description:

Description

Material Type: Prestressed Concrete
Girder Type: PS Precast Box
Member units: US Customary
Girder property input method: Schedule based
Additional Self Load: (kip/ft)
Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
Analysis Module: AASHTO ASD
Analysis Module Component:
Properties:

Analysis Method: LFD
Analysis Module: AASHTO LFD
Analysis Module Component:
Properties:

Analysis Method: LRFD
Analysis Module: AASHTO LRFD
Analysis Module Component:
Properties:

Analysis Method: LRFR
Analysis Module: AASHTO LRFR
Analysis Module Component:
Properties:

Analysis Method: Distribution Factors
Analysis Module: Legacy BrR Dist Fact
Analysis Module Component:
Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD:

ASD Factors

	Inventory	Operating
Structural steel		
Concrete		
PS Concrete Comp.		
PS Concrete Tens.		
PS Moment Cap.		
Reinforcement		
Bearing Stiffener		
Stirrup		
Timber	NA	

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcement:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)				
Lanes		Shear at		
Loaded	Shear	Supports	Moment	Deflection
1 Lane	0.100	0.100	0.100	0.100
Multi-Lane	0.100	0.100	0.100	0.100

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	38.500	Deflectio...	0.100	0.100
0.00	38.500	Moment	0.100	0.100
0.00	38.500	Shear	0.100	0.100

Shrinkage/Time

Deck curing method: Moist-cured
 Deck drying time: 3.000 *(Days)*
 Consider deck differential shrinkage loads: FALSE
 Beam Curing method: Steam-cured
 Curing time: 20.00 *(Days)*
 Service life: 75.00 *(Years)*
 Analysis time: 54.00 *(Years)*
 Composite time: 60.00 *(Days)*
 Continuous time: 45.0 *(Days)*

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left	Right
	Projection	Creep		Projection	
				<i>(in)</i> <i>(in)</i>	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL <i>(in)</i>	Support Distance on Right, SR <i>(in)</i>
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance <i>(ft)</i>	Length <i>(ft)</i>
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type: Monolithic
 Interface width: *(in)*
 Deck cohesion factor: 0.400 *(ksi)*
 Deck friction factor: 1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						
1	Left	1	3	Straight/Debonded			
	Right						
1	Left	1	4	Straight/Debonded			
	Right						
1	Left	1	5	Straight/Debonded			
	Right						
1	Left	1	6	Straight/Debonded			
	Right						
1	Left	1	7	Straight/Debonded			
	Right						
1	Left	1	8	Straight/Debonded			
	Right						
1	Left	1	9	Straight/Debonded			
	Right						
1	Left	1	10	Straight/Debonded			
	Right						
1	Left	1	11	Straight/Debonded			
	Right						
1	Left	1	12	Straight/Debonded			
	Right						
1	Left	1	13	Straight/Debonded			
	Right						
1	Left	1	14	Straight/Debonded			
	Right						
1	Left	1	15	Straight/Debonded			

1	Right	1	16	Straight/Debonded
1	Left Right	2	1	Straight/Debonded
1	Left Right	2	2	Straight/Debonded
1	Left Right	2	3	Straight/Debonded
1	Left Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.96...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear	Span	Start	Number	Spacing	Extends into
-------	------	-------	--------	---------	--------------

Reinforcement	No	Distance (ft)	Spaces	(in)	Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G2

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free

2	Roller	Free	Fixed	Free
<u>Elastic</u>				
Support	X Translation	Y Translation	Z Rotation	Override Computed
Number	(kip/ft)	(kip/ft)	(kip-in/rad)	Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD:

ASD Factors

	Inventory	Operating
Structural steel		
Concrete		
PS Concrete Comp.		
PS Concrete Tens.		
PS Moment Cap.		
Reinforcement		
Bearing Stiffener		
Stirrup		
Timber	NA	

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcement:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type:	Standard - AASHTO
-------	-------------------

LRFD Dynamic Load Allowance

Fatigue and fracture limit states:	15.0 (%)
All other limit states:	33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)				
Lanes		Shear at		
Loaded	Shear	Supports	Moment	Deflection
1 Lane	0.167	0.167	0.167	0.167
Multi-Lane	0.167	0.167	0.167	0.167

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	38.500	Deflectio...	0.167	0.200
0.00	38.500	Moment	0.167	0.200
0.00	38.500	Shear	0.167	0.200

Shrinkage/Time

Deck curing method:	Moist-cured
Deck drying time: 3.000	(Days)
Consider deck differential shrinkage loads:	FALSE
Beam Curing method:	Steam-cured
Curing time: 20.00	(Days)
Service life: 75.00	(Years)

Analysis time: 54.00 *(Years)*
 Composite time: 60.00 *(Days)*
 Continuous time: 45.0 *(Days)*

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right
	Projection	Creep		<i>(in)</i> <i>(in)</i>	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL <i>(in)</i>	Support Distance on Right, SR <i>(in)</i>
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance <i>(ft)</i>	Length <i>(ft)</i>
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	<i>(in)</i>
Deck cohesion factor:	0.400 <i>(ksi)</i>
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material Bar	Left Support Distance Bar	Bar Count	Bar Size	Right Support Material	Distance Count	Size
No.							

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance <i>(ft)</i>	Debond Distance <i>(in)</i>	Harp Curvature <i>(in)</i>
------	------	---------	----------	--------------	------------------------------	--------------------------------	-------------------------------

1		1	1	Straight/Debonded
	Left			
	Right			
1		1	2	Straight/Debonded
	Left			
	Right			
1		1	3	Straight/Debonded
	Left			
	Right			
1		1	4	Straight/Debonded
	Left			
	Right			
1		1	5	Straight/Debonded
	Left			
	Right			
1		1	6	Straight/Debonded
	Left			
	Right			
1		1	7	Straight/Debonded
	Left			
	Right			
1		1	8	Straight/Debonded
	Left			
	Right			
1		1	9	Straight/Debonded
	Left			
	Right			
1		1	10	Straight/Debonded
	Left			
	Right			
1		1	11	Straight/Debonded
	Left			
	Right			
1		1	12	Straight/Debonded
	Left			
	Right			
1		1	13	Straight/Debonded
	Left			
	Right			
1		1	14	Straight/Debonded
	Left			
	Right			
1		1	15	Straight/Debonded
	Left			
	Right			
1		1	16	Straight/Debonded
	Left			
	Right			
1		2	1	Straight/Debonded
	Left			

1	Right	2	2	Straight/Debonded
1	Left Right	2	3	Straight/Debonded
1	Left Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.95...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE

#4 Bent Shear R...	1	37.71	4	6.0000	FALSE
--------------------	---	-------	---	--------	-------

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G3

Link with: None

Description:

Existing: 17"x36" INT PSU -

Current: 17"x36" INT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				

Member Alternative 17"x36" INT PSU

Description:

Description

Material Type: Prestressed Concrete
 Girder Type: PS Precast Box
 Member units: US Customary
 Girder property input method: Schedule based
 Additional Self Load: (kip/ft)
 Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD
 Analysis Module: AASHTO ASD
 Analysis Module Component:
 Properties:

Analysis Method: LFD
 Analysis Module: AASHTO LFD
 Analysis Module Component:
 Properties:

Analysis Method: LRFD
 Analysis Module: AASHTO LRFD
 Analysis Module Component:
 Properties:

Analysis Method: LRFR
 Analysis Module: AASHTO LRFR
 Analysis Module Component:
 Properties:

Analysis Method: Distribution Factors
 Analysis Module: Legacy BrR Dist Fact
 Analysis Module Component:
 Properties:

Default rating method: LRFR
 LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.
 Reinforcement
 Bearing Stiffener
 Stirrup
 Timber NA

Default Materials

Deck concrete: Class A (3000)
 Deck reinforcement: Grade 40
 Beam concrete: Class P (5000)
 Beam reinforcement: Grade 40
 Stirrup reinforcement: Grade 40
 Prestressing strand: 7/16" (7W-250) SR

Impact

Standard Impact Factor

Type: Standard - AASHTO

LRFD Dynamic Load Allowance

Fatigue and fracture limit states: 15.0 (%)

All other limit states: 33.0 (%)

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	1.000	1.000	1.000	1.000
Multi-Lane	1.000	1.000	1.000	1.000

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	38.500	Deflectio...	0.500	0.600
0.00	38.500	Moment	0.500	0.600
0.00	38.500	Shear	0.500	0.600

Shrinkage/Time

Deck curing method: Moist-cured

Deck drying time: 3.000 (Days)

Consider deck differential shrinkage loads: FALSE

Beam Curing method: Steam-cured

Curing time: 20.00 (Days)

Service life: 75.00 (Years)

Analysis time: 54.00 (Years)

Composite time: 60.00 (Days)

Continuous time: 45.0 (Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left Projection	Right
	Projection	Creep		(in) (in)	
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information**Strand Layout**

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
	Right						
1	Left	1	2	Straight/Debonded			
	Right						

1		1	3	Straight/Debonded
	Left			
	Right			
1		1	4	Straight/Debonded
	Left			
	Right			
1		1	5	Straight/Debonded
	Left			
	Right			
1		1	6	Straight/Debonded
	Left			
	Right			
1		1	7	Straight/Debonded
	Left			
	Right			
1		1	8	Straight/Debonded
	Left			
	Right			
1		1	9	Straight/Debonded
	Left			
	Right			
1		1	10	Straight/Debonded
	Left			
	Right			
1		1	11	Straight/Debonded
	Left			
	Right			
1		1	12	Straight/Debonded
	Left			
	Right			
1		1	13	Straight/Debonded
	Left			
	Right			
1		1	14	Straight/Debonded
	Left			
	Right			
1		1	15	Straight/Debonded
	Left			
	Right			
1		1	16	Straight/Debonded
	Left			
	Right			
1		2	1	Straight/Debonded
	Left			
	Right			
1		2	2	Straight/Debonded
	Left			
	Right			
1		2	3	Straight/Debonded
	Left			

1	Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance	Number Spaces	Spacing	Composite Length
------------------------	------------	-------------------	------------------	---------	---------------------

#3 - 2'-7" long	1	(ft) 0.21	4	(in) 6.0000	(ft)
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G4

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G5

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G6

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G7

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G8

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G9

Link with: G3

Description:

Existing:

Current:

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member G10

Link with: None

Description:

Existing: 17"x36" INT PSU - w/ post Tensioning -

Current: 17"x36" INT PSU - w/ post Tensioning -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

<u>Elastic</u>				
Support	X Translation	Y Translation	Z Rotation	Override Computed
Number	(kip/ft)	(kip/ft)	(kip-in/rad)	Z Rotation
1				
2				

Member Alternative 17"x36" INT PSU - w/ post Tensioning

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory

Operating

Structural steel	
Concrete	
PS Concrete Comp.	
PS Concrete Tens.	
PS Moment Cap.	
Reinforcement	
Bearing Stiffener	
Stirrup	
Timber	NA

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcemt:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type:	Standard - AASHTO
-------	-------------------

LRFD Dynamic Load Allowance

Fatigue and fracture limit states:	15.0 (%)
------------------------------------	----------

All other limit states:	33.0 (%)
-------------------------	----------

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.527	0.000	0.527	0.182
Multi-Lane	0.527	0.000	0.527	0.364

LRFD

Distance (ft)	Length (ft)	Type	1 Lane	Multi-Lane
0.00	38.500	Moment	0.254	0.256
0.00	38.500	Shear	0.254	0.256
0.00	38.500	Deflectio...	0.109	0.182

Shrinkage/Time

Deck curing method:	Moist-cured
---------------------	-------------

Deck drying time:	3.000 (Days)
-------------------	--------------

Consider deck differential shrinkage loads:	FALSE
---	-------

Beam Curing method:	Steam-cured
---------------------	-------------

Curing time:	20.00 (Days)
--------------	--------------

Service life:	75.00 (Years)
---------------	---------------

Analysis time:	54.00 (Years)
----------------	---------------

Composite time:	60.00 (Days)
-----------------	--------------

Continuous time: 45.0 *(Days)*

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material n	Prestress Properties	Left Projection	Right Projection
				<i>(in)</i>	<i>(in)</i>
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	8.5000	8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL <i>(in)</i>	Support Distance on Right, SR <i>(in)</i>
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance <i>(ft)</i>	Length <i>(ft)</i>
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	<i>(in)</i>
Deck cohesion factor:	0.400 <i>(ksi)</i>
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material Bar	Left Support Distance Bar	Bar Count	Bar Size	Right Support Material	Distance	Count	Size
No.								

Prestressing Force Information

Strand Layout

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance <i>(ft)</i>	Debond Distance <i>(in)</i>	Harp Curvature <i>(in)</i>
1	Left	1	1	Straight/Debonded			

1	Right	1	2	Straight/Debonded
	Left			
1	Right	1	3	Straight/Debonded
	Left			
1	Right	1	4	Straight/Debonded
	Left			
1	Right	1	5	Straight/Debonded
	Left			
1	Right	1	6	Straight/Debonded
	Left			
1	Right	1	7	Straight/Debonded
	Left			
1	Right	1	8	Straight/Debonded
	Left			
1	Right	1	9	Straight/Debonded
	Left			
1	Right	1	10	Straight/Debonded
	Left			
1	Right	1	11	Straight/Debonded
	Left			
1	Right	1	12	Straight/Debonded
	Left			
1	Right	1	13	Straight/Debonded
	Left			
1	Right	1	14	Straight/Debonded
	Left			
1	Right	1	15	Straight/Debonded
	Left			
1	Right	1	16	Straight/Debonded
	Left			
1	Right	2	1	Straight/Debonded
	Left			
1	Right	2	2	Straight/Debonded

1	Left Right	2	3	Straight/Debonded
1	Left Right	2	4	Straight/Debonded
1	Left Right	2	5	Straight/Debonded
1	Left Right	2	6	Straight/Debonded
1	Left Right	3	1	Straight/Debonded
1	Left Right	3	7	Straight/Debonded
1	Left Right	3	10	Straight/Debonded
1	Left Right	3	16	Straight/Debonded

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.95...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
#3 - 2'-7" long	1	0.21	4	6.0000	
#3 - 2'-7" long	1	2.21	1	10.5000	
#3 - 2'-7" long	1	3.08	27	15.0000	
#3 - 2'-7" long	1	36.83	1	10.5000	
#3 - 2'-7" long	1	37.71	4	6.0000	

Member G11

Link with: None

Description:

Existing: 17"x36" EXT PSU -

Current: 17"x36" EXT PSU -

Number of Spans: 1

Span Number	Span Length (ft)
1	38.500000

Support	Frame Connection
1	
2	

Pedestrian load: (lb/ft)

Member Loads

Member Loads - Settlement

Support Number	Horizontal (in)	Vertical (in)	Rotational (Radians)	Load Case Name
1				
2				

Support Constraints

General

Support Number	Support Type	X Translation	Y Translation	Z Rotation
1	Pinned	Fixed	Fixed	Free
2	Roller	Free	Fixed	Free

Elastic

Support Number	X Translation (kip/ft)	Y Translation (kip/ft)	Z Rotation (kip-in/rad)	Override Computed Z Rotation
1				
2				

Member Alternative 17"x36" EXT PSU

Description:

Description

Material Type: Prestressed Concrete

Girder Type: PS Precast Box

Member units: US Customary

Girder property input method: Schedule based

Additional Self Load: (kip/ft)

Additional Self Load %: 1.0 (%)

Analysis Module

Analysis Method: ASD

Analysis Module: AASHTO ASD

Analysis Module Component:

Properties:

Analysis Method: LFD

Analysis Module: AASHTO LFD

Analysis Module Component:

Properties:

Analysis Method: LRFD

Analysis Module: AASHTO LRFD

Analysis Module Component:

Properties:

Analysis Method: LRFR

Analysis Module: AASHTO LRFR

Analysis Module Component:

Properties:

Analysis Method: Distribution Factors

Analysis Module: Legacy BrR Dist Fact

Analysis Module Component:

Properties:

Default rating method: LRFR

LRFD shear computation method: General Procedure

Factors

Factor Override

LRFD:

LFD: 2002 AASHTO Std. Specifications(CF=0.9)

ASD Factors

Inventory Operating

Structural steel

Concrete

PS Concrete Comp.

PS Concrete Tens.

PS Moment Cap.

Reinforcement	
Bearing Stiffener	
Stirrup	
Timber	NA

Default Materials

Deck concrete:	Class A (3000)
Deck reinforcement:	Grade 40
Beam concrete:	Class P (5000)
Beam reinforcement:	Grade 40
Stirrup reinforcemt:	Grade 40
Prestressing strand:	7/16" (7W-250) SR

Impact

Standard Impact Factor

Type:	Standard - AASHTO
-------	-------------------

LRFD Dynamic Load Allowance

Fatigue and fracture limit states:	15.0 (%)
------------------------------------	----------

All other limit states:	33.0 (%)
-------------------------	----------

Live Load Distribution

Standard

D i s t r i b u t i o n F a c t o r (Wheels)

Lanes	Shear	Shear at Supports	Moment	Deflection
Loaded				
1 Lane	0.100	0.100	0.100	0.100
Multi-Lane	0.100	0.100	0.100	0.100

LRFD

Distance	Length	Type	1 Lane	Multi-Lane
(ft)	(ft)			
0.00	38.500	Deflectio...	0.100	0.100
0.00	38.500	Moment	0.100	0.100
0.00	38.500	Shear	0.100	0.100

Shrinkage/Time

Deck curing method:	Moist-cured
Deck drying time: 3.000	(Days)
Consider deck differential shrinkage loads:	FALSE
Beam Curing method:	Steam-cured
Curing time: 20.00	(Days)
Service life: 75.00	(Years)
Analysis time: 54.00	(Years)
Composite time: 60.00	(Days)
Continuous time: 45.0	(Days)

Beam Details

Span Details

Span	Prestress Shape Use	Concrete Material	Prestress Properties	Left Projection	Right Projection
1	17"x36" PSU TRUE	Class P (5000... 6.64...	PS Strands Pr...	(in) 8.5000	(in) 8.5000

Continuous Support Details

Support Number	Support Distance on Left, SL (in)	Support Distance on Right, SR (in)
1		
2		

Stress Limit Ranges

Stress Limit	Span	Start Distance (ft)	Length (ft)
PS Conc Stress Lim...	1	0.000	39.92

Slab Interface

Deck interface type:	Monolithic
Interface width:	(in)
Deck cohesion factor:	0.400 (ksi)
Deck friction factor:	1.400

Continuity Diaphragm

Span	Material	Left Support Distance	Bar	Bar	Right Support Material	Distance
No.	Bar	Bar	Count	Size	Count	Size

Prestressing Force Information**Strand Layout**

Span	Pos.	Row No.	Col. No.	Config. Type	Harp Distance (ft)	Debond Distance (in)	Harp Curvature (in)
1	Left	1	1	Straight/Debonded			
1	Right	1	2	Straight/Debonded			
1	Left	1	3	Straight/Debonded			
	Right						

1	Left Right	1	4	Straight/Debonded
1	Left Right	1	5	Straight/Debonded
1	Left Right	1	6	Straight/Debonded
1	Left Right	1	7	Straight/Debonded
1	Left Right	1	8	Straight/Debonded
1	Left Right	1	9	Straight/Debonded
1	Left Right	1	10	Straight/Debonded
1	Left Right	1	11	Straight/Debonded
1	Left Right	1	12	Straight/Debonded
1	Left Right	1	13	Straight/Debonded
1	Left Right	1	14	Straight/Debonded
1	Left Right	1	15	Straight/Debonded
1	Left Right	1	16	Straight/Debonded
1	Left Right	2	1	Straight/Debonded
1	Left Right	2	2	Straight/Debonded
1	Left Right	2	3	Straight/Debonded

1	2	4	Straight/Debonded
	Left		
	Right		
1	2	5	Straight/Debonded
	Left		
	Right		
1	2	6	Straight/Debonded
	Left		
	Right		
1	3	1	Straight/Debonded
	Left		
	Right		
1	3	7	Straight/Debonded
	Left		
	Right		
1	3	10	Straight/Debonded
	Left		
	Right		
1	3	16	Straight/Debonded
	Left		
	Right		

Deck Profile

Interior Diaphragms

Span	Start Distance (ft)	Spacing (ft)	No of Spaces	Thickness (in)	Weight (kip)
1	0.00...	1.00	1	2.0000	0.3272
1	1.00...	8.96	1	1.0000	0.1636
1	9.96...	20.00	1	1.0000	0.1636
1	29.96...	8.96	1	1.0000	0.1636

Shear Reinforcement Ranges - Vertical

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Extends into Deck
#4 Bent Shear R...	1	0.21	4	6.0000	FALSE
#4 Bent Shear R...	1	2.21	1	10.5000	FALSE
#4 Bent Shear R...	1	3.08	27	15.0000	FALSE
#4 Bent Shear R...	1	36.83	1	10.5000	FALSE
#4 Bent Shear R...	1	37.71	4	6.0000	FALSE

Shear Reinforcement Ranges - Horizontal

Shear Reinforcement	Span No	Start Distance (ft)	Number Spaces	Spacing (in)	Composite Length (ft)
------------------------	------------	---------------------------	------------------	-----------------	-----------------------------

#3 - 2'-7" long	1	0.21	4	6.0000
#3 - 2'-7" long	1	2.21	1	10.5000
#3 - 2'-7" long	1	3.08	27	15.0000
#3 - 2'-7" long	1	36.83	1	10.5000
#3 - 2'-7" long	1	37.71	4	6.0000

1.4 SUMMARY OF LRFR LOAD RATING ANALYSIS RESULTS

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294
Bridge ID: 874294

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 15:41:57
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 15:42:26

Structure Definition Name: End Span 1 (or 3) - PS Conc PSU
Member Name: G3
Member Alternative Name: 17"x36" INT PSU - Existing Condition

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - Existing Condition
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 1

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location					DL +					
(ft)	Percent	Limit State	Units	Capacity	Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	128.89	7.72	41.31	1.649	59.37	2.138	76.97
1.69	6.0	Flexure	kip-ft	249.21	13.52	68.34	1.942	69.93	2.518	90.65
1.69	6.0	Shear	kip	118.02	7.42	40.19	1.546	55.65	2.004	72.14
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.49	3.891	140.09		
2.83	10.0	Flexure	kip-ft	288.41	21.61	108.12	1.381	49.73	1.791	64.47
2.83	10.0	Shear	kip	61.28	6.76	37.73	0.800	28.81	1.652	59.48
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.78	2.366	85.17		
5.66	20.0	Flexure	kip-ft	304.60	38.40	184.27	0.796	28.65	1.031	37.13
5.66	20.0	Shear	kip	29.07	5.11	31.70	0.409	14.72	0.815	29.33
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	1.33	1.274	45.88		
8.49	30.0	Flexure	kip-ft	304.60	50.23	228.45	0.605	21.77	0.784	28.23
8.49	30.0	Shear	kip	23.83	3.30	25.78	0.437	15.73	0.795	28.61
8.49	30.0	Concrete Stresses	ksi	1.63	0.36	1.65	0.963	34.67		
11.32	40.0	Flexure	kip-ft	304.60	57.22	240.66	0.553	19.92	0.717	25.83
11.32	40.0	Shear	kip	23.83	1.65	19.96	0.623	22.44	1.044	37.57
11.32	40.0	Concrete Stresses	ksi	1.63	0.41	1.73	0.878	31.61		
14.15	50.0	Flexure	kip-ft	304.60	59.54	221.36	0.594	21.39	0.770	27.73
14.15	50.0	Shear	kip	-24.61	-0.00	-14.26	0.986	35.50	1.780	64.09

14.15	50.0	Concrete Stresses	ksi	1.63	0.43	1.60	0.941	33.89		
16.98	60.0	Flexure	kip- ft	304.60	57.20	240.66	0.553	19.93	0.717	25.83
16.98	60.0	Shear	kip	-23.83	-1.65	-19.96	0.623	22.43	1.043	37.56
16.98	60.0	Concrete Stresses	ksi	1.63	0.41	1.73	0.878	31.61		
19.80	70.0	Flexure	kip-ft	304.60	50.19	228.45	0.605	21.78	0.784	28.23
19.80	70.0	Shear	kip	-23.83	-3.30	-25.78	0.437	15.73	0.795	28.61
19.80	70.0	Concrete Stresses	ksi	1.63	0.36	1.65	0.963	34.68		
22.63	80.0	Flexure	kip-ft	304.60	38.37	184.27	0.796	28.65	1.032	37.14
22.63	80.0	Shear	kip	-29.07	-5.12	-31.70	0.409	14.72	0.815	29.32
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	1.33	1.275	45.88		
25.46	90.0	Flexure	kip-ft	295.44	21.57	108.12	1.419	51.08	1.839	66.22
25.46	90.0	Shear	kip	-58.31	-6.76	-37.73	0.755	27.19	1.596	57.45
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.78	2.367	85.19		
26.81	94.8	Flexure	kip-ft	262.19	11.90	60.52	2.335	84.07	3.027	108.97
26.81	94.8	Shear	kip	-118.16	-7.55	-40.64	1.529	55.03	1.981	71.33
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.44	4.428	159.40		
27.11	95.8	Shear	kip	-125.66	-7.72	-41.29	1.605	57.79	2.081	74.92
28.29	100.0	Flexure	kip- ft	88.49	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Condition
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 1

								Inventory	Inventory	Operating	Operating
Location								Rating	Load Rating	Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor		(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip- ft	89.52	0.00	0.00	99.000		3564.00	99.000	3564.00
0.00	0.0		ksi	0.70	-0.00	0.00	99.000		3564.00		

		Concrete Stresses								
1.17	4.1	Shear	kip	128.89	7.72	40.42	1.686	60.69	2.185	78.67
1.69	6.0	Flexure	kip-ft	249.21	13.52	67.18	1.976	71.14	2.562	92.22
1.69	6.0	Shear	kip	118.02	7.42	39.50	1.573	56.63	2.039	73.40
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.48	3.959	142.52		
2.83	10.0	Flexure	kip-ft	288.41	21.61	107.45	1.390	50.04	1.802	64.87
2.83	10.0	Shear	kip	61.99	6.76	37.49	0.816	29.38	1.663	59.86
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.77	2.381	85.71		
5.66	20.0	Flexure	kip-ft	304.60	38.40	189.24	0.775	27.89	1.004	36.16
5.66	20.0	Shear	kip	28.05	5.11	32.58	0.380	13.68	0.758	27.30
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	1.36	1.241	44.67		
8.49	30.0	Flexure	kip-ft	304.60	50.23	245.39	0.563	20.27	0.730	26.28
8.49	30.0	Shear	kip	23.83	3.30	27.77	0.406	14.60	0.663	23.86
8.49	30.0	Concrete Stresses	ksi	1.63	0.36	1.77	0.897	32.28		
11.32	40.0	Flexure	kip- ft	304.60	57.22	275.88	0.483	17.38	0.626	22.53
11.32	40.0	Shear	kip	23.83	1.65	23.07	0.539	19.41	0.746	26.86
11.32	40.0	Concrete Stresses	ksi	1.63	0.41	1.99	0.766	27.57		
14.15	50.0	Flexure	kip- ft	304.60	59.54	280.73	0.469	16.87	0.607	21.86
14.15	50.0	Shear	kip	-23.83	-0.00	-18.49	0.737	26.51	1.013	36.46
14.15	50.0	Concrete Stresses	ksi	1.63	0.43	2.02	0.742	26.73		
16.98	60.0	Flexure	kip- ft	304.60	57.20	275.88	0.483	17.38	0.626	22.53
16.98	60.0	Shear	kip	-23.83	-1.65	-23.07	0.539	19.40	0.746	26.85
16.98	60.0	Concrete Stresses	ksi	1.63	0.41	1.99	0.766	27.58		
19.80	70.0	Flexure	kip-ft	304.60	50.19	245.39	0.563	20.28	0.730	26.28
19.80	70.0	Shear	kip	-23.83	-3.30	-27.77	0.405	14.60	0.663	23.85
19.80	70.0	Concrete Stresses	ksi	1.63	0.36	1.77	0.897	32.29		
22.63	80.0	Flexure	kip-ft	304.60	38.37	189.24	0.775	27.90	1.005	36.16
22.63	80.0	Shear	kip	-28.05	-5.12	-32.58	0.380	13.67	0.758	27.30
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	1.36	1.241	44.68		
25.46	90.0	Flexure	kip-ft	295.44	21.57	107.45	1.428	51.40	1.851	66.63
25.46	90.0	Shear	kip	-59.02	-6.76	-37.49	0.771	27.74	1.606	57.81
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.77	2.381	85.73		

26.81	94.8	Flexure	kip-ft	262.19	11.90	59.38	2.380	85.68	3.085	111.07
26.81	94.8	Shear	kip	-118.16	-7.55	-39.87	1.558	56.09	2.020	72.71
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.43	4.513	162.46		
27.11	95.8	Shear	kip	-125.66	-7.72	-40.40	1.641	59.07	2.127	76.57
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	2772.00
1.17	4.1	Shear	kip	128.89	7.72	22.62	4.054	113.52
1.69	6.0	Flexure	kip-ft	249.21	13.52	37.34	4.785	133.99
1.69	6.0	Shear	kip	118.02	7.42	22.13	3.780	105.84
2.83	10.0	Flexure	kip-ft	288.41	21.61	59.51	3.379	94.61
2.83	10.0	Shear	kip	92.60	6.76	21.03	3.078	86.17
5.66	20.0	Flexure	kip-ft	304.60	38.40	103.67	1.904	53.31
5.66	20.0	Shear	kip	85.06	5.11	18.32	3.303	92.49
8.49	30.0	Flexure	kip-ft	304.60	50.23	132.47	1.404	39.32
8.49	30.0	Shear	kip	75.98	3.30	15.61	3.542	99.17
11.32	40.0	Flexure	kip-ft	304.60	57.22	145.92	1.229	34.40
11.32	40.0	Shear	kip	62.87	1.65	12.89	3.628	101.58
14.15	50.0	Flexure	kip-ft	304.60	59.54	144.02	1.229	34.42
14.15	50.0	Shear	kip	-66.05	-0.00	-10.18	4.990	139.73
16.98	60.0	Flexure	kip-ft	304.60	57.20	145.92	1.229	34.41
16.98	60.0	Shear	kip	-62.88	-1.65	-12.89	3.628	101.57
19.80	70.0	Flexure	kip-ft	304.60	50.19	132.47	1.404	39.32
19.80	70.0	Shear	kip	-76.01	-3.30	-15.61	3.543	99.20
22.63	80.0	Flexure	kip-ft	304.60	38.37	103.67	1.904	53.32
22.63	80.0	Shear	kip	-85.06	-5.12	-18.32	3.303	92.48
25.46	90.0	Flexure	kip-ft	295.44	21.57	59.51	3.470	97.17

25.46	90.0	Shear	kip	-89.73	-6.76	-21.03	2.972	83.23
26.81	94.8	Flexure	kip-ft	262.19	11.90	33.03	5.760	161.28
26.81	94.8	Shear	kip	-118.16	-7.55	-22.33	3.745	104.87
27.11	95.8	Shear	kip	-125.66	-7.72	-22.61	3.946	110.49
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3628.35
1.17	4.1	Shear	kip	128.89	7.72	31.77	2.887	105.82
1.69	6.0	Flexure	kip-ft	249.21	13.52	51.99	3.437	125.98
1.69	6.0	Shear	kip	118.02	7.42	30.81	2.715	99.51
2.83	10.0	Flexure	kip-ft	288.41	21.61	82.09	2.449	89.77
2.83	10.0	Shear	kip	92.60	6.76	29.02	2.231	81.77
5.66	20.0	Flexure	kip-ft	304.60	38.40	144.31	1.368	50.13
5.66	20.0	Shear	kip	64.21	5.11	25.50	1.744	63.92
8.49	30.0	Flexure	kip-ft	304.60	50.23	186.66	0.996	36.52
8.49	30.0	Shear	kip	43.23	3.30	21.99	1.368	50.13
11.32	40.0	Flexure	kip-ft	304.60	57.22	209.15	0.857	31.42
11.32	40.0	Shear	kip	37.55	1.65	18.48	1.477	54.14
14.15	50.0	Flexure	kip-ft	304.60	59.54	211.77	0.836	30.64
14.15	50.0	Shear	kip	-37.72	-0.00	-14.97	1.938	71.03
16.98	60.0	Flexure	kip-ft	304.60	57.20	209.15	0.857	31.42
16.98	60.0	Shear	kip	-37.55	-1.65	-18.48	1.477	54.13
19.80	70.0	Flexure	kip-ft	304.60	50.19	186.66	0.997	36.53
19.80	70.0	Shear	kip	-43.24	-3.30	-21.99	1.368	50.13
22.63	80.0	Flexure	kip-ft	304.60	38.37	144.31	1.368	50.14
22.63	80.0	Shear	kip	-64.23	-5.12	-25.50	1.744	63.93
25.46	90.0	Flexure	kip-ft	295.44	21.57	82.09	2.516	92.21
25.46	90.0	Shear	kip	-89.73	-6.76	-29.02	2.155	78.97
26.81	94.8	Flexure	kip-ft	262.19	11.90	46.14	4.123	151.10
26.81	94.8	Shear	kip	-118.16	-7.55	-31.19	2.681	98.26
27.11	95.8	Shear	kip	-125.66	-7.72	-31.75	2.811	103.01

28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3628.35
-------	-------	---------	--------	-------	------	------	--------	---------

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	128.89	7.72	31.90	2.875	115.01
1.69	6.0	Flexure	kip-ft	249.21	13.52	52.61	3.397	135.88
1.69	6.0	Shear	kip	118.02	7.42	31.17	2.683	107.33
2.83	10.0	Flexure	kip-ft	288.41	21.61	83.64	2.404	96.16
2.83	10.0	Shear	kip	92.60	6.76	29.56	2.190	87.59
5.66	20.0	Flexure	kip-ft	304.60	38.40	144.70	1.364	54.56
5.66	20.0	Shear	kip	63.88	5.11	25.57	1.729	69.18
8.49	30.0	Flexure	kip-ft	304.60	50.23	183.19	1.015	40.62
8.49	30.0	Shear	kip	44.36	3.30	21.58	1.434	57.37
11.32	40.0	Flexure	kip-ft	304.60	57.22	199.10	0.901	36.02
11.32	40.0	Shear	kip	40.01	1.65	17.59	1.659	66.37
14.15	50.0	Flexure	kip-ft	304.60	59.54	209.06	0.847	33.88
14.15	50.0	Shear	kip	-38.63	-0.00	-13.61	2.183	87.33
16.98	60.0	Flexure	kip-ft	304.60	57.20	199.10	0.901	36.02
16.98	60.0	Shear	kip	-40.01	-1.65	-17.59	1.659	66.36
19.80	70.0	Flexure	kip-ft	304.60	50.19	183.19	1.016	40.62
19.80	70.0	Shear	kip	-44.37	-3.30	-21.58	1.434	57.37
22.63	80.0	Flexure	kip-ft	304.60	38.37	144.70	1.364	54.57
22.63	80.0	Shear	kip	-63.89	-5.12	-25.57	1.730	69.18
25.46	90.0	Flexure	kip-ft	295.44	21.57	83.64	2.469	98.77
25.46	90.0	Shear	kip	-89.73	-6.76	-29.56	2.115	84.59
26.81	94.8	Flexure	kip-ft	262.19	11.90	46.55	4.087	163.48
26.81	94.8	Shear	kip	-118.16	-7.55	-31.47	2.658	106.31
27.11	95.8	Shear	kip	-125.66	-7.72	-31.89	2.799	111.94
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3960.00

Detailed Rating Results

**17"x36" INT PSU - Existing Condition
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane**

Span 1

							Permit Rating	Permit Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	5940.00
1.69	6.0	Flexure	kip-ft	249.21	13.52	82.89	2.335	140.13
2.83	10.0	Flexure	kip-ft	288.41	21.61	130.88	1.664	99.86
5.66	20.0	Flexure	kip-ft	304.60	38.40	221.65	0.965	57.89
8.49	30.0	Flexure	kip-ft	304.60	50.23	272.30	0.740	44.40
11.32	40.0	Flexure	kip-ft	304.60	57.22	282.85	0.687	41.20
14.15	50.0	Flexure	kip-ft	304.60	59.54	253.93	0.755	45.32
16.98	60.0	Flexure	kip-ft	304.60	57.20	282.85	0.687	41.21
19.80	70.0	Flexure	kip-ft	304.60	50.19	272.30	0.740	44.41
22.63	80.0	Flexure	kip-ft	304.60	38.37	221.65	0.965	57.89
25.46	90.0	Flexure	kip-ft	295.44	21.57	130.88	1.709	102.57
26.81	94.8	Flexure	kip-ft	262.19	11.90	73.43	2.807	168.40
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	5940.00

**Detailed Rating Results
17"x36" INT PSU - Existing Condition
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane**

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	128.89	7.72	31.15	2.944	117.77
1.69	6.0	Flexure	kip-ft	249.21	13.52	51.25	3.487	139.49
1.69	6.0	Shear	kip	118.02	7.42	30.37	2.754	110.18
2.83	10.0	Flexure	kip-ft	288.41	21.61	81.00	2.482	99.30

2.83	10.0	Shear	kip	92.60	6.76	28.63	2.261	90.45
5.66	20.0	Flexure	kip-ft	304.60	38.40	137.61	1.434	57.38
5.66	20.0	Shear	kip	70.63	5.11	24.32	2.032	81.28
8.49	30.0	Flexure	kip-ft	304.60	50.23	169.84	1.095	43.81
8.49	30.0	Shear	kip	49.40	3.30	20.01	1.741	69.63
11.32	40.0	Flexure	kip-ft	304.60	57.22	189.17	0.948	37.91
11.32	40.0	Shear	kip	43.10	1.65	15.70	2.011	80.43
14.15	50.0	Flexure	kip-ft	304.60	59.54	189.87	0.932	37.30
14.15	50.0	Shear	kip	-43.83	-0.00	-12.33	2.734	109.34
16.98	60.0	Flexure	kip-ft	304.60	57.20	189.17	0.948	37.91
16.98	60.0	Shear	kip	-43.10	-1.65	-15.70	2.011	80.42
19.80	70.0	Flexure	kip-ft	304.60	50.19	169.84	1.095	43.82
19.80	70.0	Shear	kip	-49.41	-3.30	-20.01	1.741	69.63
22.63	80.0	Flexure	kip-ft	304.60	38.37	137.61	1.435	57.38
22.63	80.0	Shear	kip	-70.64	-5.12	-24.32	2.032	81.29
25.46	90.0	Flexure	kip-ft	295.44	21.57	81.00	2.550	101.99
25.46	90.0	Shear	kip	-89.73	-6.76	-28.63	2.184	87.35
26.81	94.8	Flexure	kip-ft	262.19	11.90	45.39	4.191	167.65
26.81	94.8	Shear	kip	-118.16	-7.55	-30.68	2.725	109.02
27.11	95.8	Shear	kip	-125.66	-7.72	-31.14	2.866	114.63
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	1683.00
1.17	4.1	Shear	kip	128.89	7.72	21.61	4.245	72.16
1.69	6.0	Flexure	kip-ft	249.21	13.52	35.63	5.016	85.26
1.69	6.0	Shear	kip	118.02	7.42	21.11	3.962	67.35
2.83	10.0	Flexure	kip-ft	288.41	21.61	56.64	3.550	60.35
2.83	10.0	Shear	kip	92.60	6.76	20.02	3.234	54.97
5.66	20.0	Flexure	kip-ft	304.60	38.40	97.92	2.016	34.27
5.66	20.0	Shear	kip	85.06	5.11	17.31	3.497	59.45
8.49	30.0	Flexure	kip-ft	304.60	50.23	123.85	1.502	25.53

8.49	30.0	Shear	kip	85.06	3.30	14.59	4.267	72.54
11.32	40.0	Flexure	kip-ft	304.60	57.22	134.43	1.334	22.67
11.32	40.0	Shear	kip	73.13	1.65	11.88	4.602	78.24
14.15	50.0	Flexure	kip-ft	304.60	59.54	129.66	1.366	23.21
14.15	50.0	Shear	kip	-81.39	-0.00	-9.17	6.830	116.11
16.98	60.0	Flexure	kip-ft	304.60	57.20	134.43	1.334	22.68
16.98	60.0	Shear	kip	-73.14	-1.65	-11.88	4.602	78.24
19.80	70.0	Flexure	kip-ft	304.60	50.19	123.85	1.502	25.54
19.80	70.0	Shear	kip	-85.06	-3.30	-14.59	4.266	72.53
22.63	80.0	Flexure	kip-ft	304.60	38.37	97.92	2.016	34.27
22.63	80.0	Shear	kip	-85.06	-5.12	-17.31	3.497	59.44
25.46	90.0	Flexure	kip-ft	295.44	21.57	56.64	3.646	61.99
25.46	90.0	Shear	kip	-89.73	-6.76	-20.02	3.123	53.09
26.81	94.8	Flexure	kip-ft	262.19	11.90	31.53	6.034	102.58
26.81	94.8	Shear	kip	-118.16	-7.55	-21.31	3.924	66.71
27.11	95.8	Shear	kip	-125.66	-7.72	-21.60	4.132	70.24
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3267.00
1.17	4.1	Shear	kip	128.89	7.72	38.49	2.383	78.64
1.69	6.0	Flexure	kip-ft	249.21	13.52	63.33	2.822	93.12
1.69	6.0	Shear	kip	118.02	7.42	37.53	2.229	73.55
2.83	10.0	Flexure	kip-ft	288.41	21.61	100.16	2.007	66.24
2.83	10.0	Shear	kip	92.60	6.76	35.40	1.828	60.34
5.66	20.0	Flexure	kip-ft	304.60	38.40	170.52	1.158	38.20
5.66	20.0	Shear	kip	48.46	5.11	30.14	1.074	35.44
8.49	30.0	Flexure	kip-ft	304.60	50.23	211.09	0.881	29.08
8.49	30.0	Shear	kip	36.71	3.30	24.87	1.008	33.26
11.32	40.0	Flexure	kip-ft	304.60	57.22	236.48	0.758	25.02
11.32	40.0	Shear	kip	32.36	1.65	19.60	1.189	39.24
14.15	50.0	Flexure	kip-ft	304.60	59.54	239.38	0.740	24.41

14.15	50.0	Shear	kip	-32.65	-0.00	-14.97	1.677	55.35
16.98	60.0	Flexure	kip-ft	304.60	57.20	236.48	0.758	25.02
16.98	60.0	Shear	kip	-32.37	-1.65	-19.60	1.189	39.23
19.80	70.0	Flexure	kip-ft	304.60	50.19	211.09	0.881	29.09
19.80	70.0	Shear	kip	-36.71	-3.30	-24.87	1.008	33.26
22.63	80.0	Flexure	kip-ft	304.60	38.37	170.52	1.158	38.20
22.63	80.0	Shear	kip	-48.47	-5.12	-30.14	1.074	35.44
25.46	90.0	Flexure	kip-ft	295.44	21.57	100.16	2.062	68.04
25.46	90.0	Shear	kip	-89.73	-6.76	-35.40	1.766	58.28
26.81	94.8	Flexure	kip-ft	262.19	11.90	56.09	3.392	111.93
26.81	94.8	Shear	kip	-118.16	-7.55	-37.92	2.206	72.79
27.11	95.8	Shear	kip	-125.66	-7.72	-38.47	2.320	76.55
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	89.52	0.00	0.00	99.000	3465.00
1.17	4.1	Shear	kip	128.89	7.72	40.09	2.288	80.08
1.69	6.0	Flexure	kip-ft	249.21	13.52	65.94	2.710	94.86
1.69	6.0	Shear	kip	118.02	7.42	39.07	2.141	74.92
2.83	10.0	Flexure	kip-ft	288.41	21.61	104.17	1.930	67.56
2.83	10.0	Shear	kip	92.60	6.76	36.82	1.758	61.54
5.66	20.0	Flexure	kip-ft	304.60	38.40	176.73	1.117	39.09
5.66	20.0	Shear	kip	45.94	5.11	31.23	0.974	34.10
8.49	30.0	Flexure	kip-ft	304.60	50.23	225.32	0.826	28.89
8.49	30.0	Shear	kip	33.91	3.30	25.65	0.893	31.27
11.32	40.0	Flexure	kip-ft	304.60	57.22	257.95	0.695	24.33
11.32	40.0	Shear	kip	29.16	1.65	20.27	1.029	36.00
14.15	50.0	Flexure	kip-ft	304.60	59.54	258.96	0.684	23.93
14.15	50.0	Shear	kip	-29.63	-0.00	-15.79	1.443	50.51
16.98	60.0	Flexure	kip-ft	304.60	57.20	257.95	0.695	24.33
16.98	60.0	Shear	kip	-29.16	-1.65	-20.27	1.028	35.99
19.80	70.0	Flexure	kip-ft	304.60	50.19	225.32	0.826	28.90

19.80	70.0	Shear	kip	-33.91	-3.30	-25.65	0.893	31.27
22.63	80.0	Flexure	kip-ft	304.60	38.37	176.73	1.117	39.10
22.63	80.0	Shear	kip	-45.95	-5.12	-31.23	0.974	34.10
25.46	90.0	Flexure	kip-ft	295.44	21.57	104.17	1.983	69.39
25.46	90.0	Shear	kip	-89.73	-6.76	-36.82	1.698	59.43
26.81	94.8	Flexure	kip-ft	262.19	11.90	58.40	3.257	114.00
26.81	94.8	Shear	kip	-118.16	-7.55	-39.48	2.118	74.13
27.11	95.8	Shear	kip	-125.66	-7.72	-40.07	2.227	77.94
28.29	100.0	Flexure	kip-ft	88.49	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294
Bridge ID: 874294

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 15:45:03
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 15:45:44

Structure Definition Name: End Span 1 (or 3) - PS Conc PSU
Member Name: G10
Member Alternative Name: 17"x36" INT PSU - (w/ Post Tensioning)

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 1

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	129.09	7.72	20.37	3.351	120.64	4.344	156.39
1.69	6.0	Flexure	kip-ft	243.32	13.52	33.69	3.841	138.27	4.979	179.24
1.69	6.0	Shear	kip	118.17	7.42	19.81	3.141	113.07	4.072	146.57
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.25	7.736	278.50		
2.83	10.0	Flexure	kip-ft	284.36	21.61	53.30	2.759	99.33	3.577	128.76
2.83	10.0	Shear	kip	92.75	6.76	18.60	2.590	93.25	3.358	120.88
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.700	169.19		
5.66	20.0	Flexure	kip-ft	304.65	38.40	90.83	1.615	58.13	2.093	75.35
5.66	20.0	Shear	kip	85.08	5.11	15.62	2.878	103.61	3.731	134.31
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	0.67	2.527	90.96		
8.49	30.0	Flexure	kip-ft	304.65	50.23	112.61	1.227	44.18	1.591	57.27
8.49	30.0	Shear	kip	59.51	3.30	12.71	2.491	89.69	4.720	169.93
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	0.83	1.907	68.64		
11.32	40.0	Flexure	kip-ft	304.65	57.22	118.63	1.123	40.43	1.456	52.41
11.32	40.0	Shear	kip	54.86	1.65	9.84	3.066	110.39	6.250	225.00
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	0.87	1.736	62.51		
14.15	50.0	Flexure		304.65	59.54	109.11	1.206	43.40	1.563	56.26

14.15	50.0	Shear	kip-ft	-64.58	-0.00	-7.03	5.251	189.03	8.967	322.81
14.15	50.0	Concrete Stresses	ksi	1.63	0.44	0.80	1.861	67.00		
16.98	60.0	Flexure	kip-ft	304.65	57.20	118.63	1.123	40.43	1.456	52.41
16.98	60.0	Shear	kip	-54.87	-1.65	-9.84	3.066	110.38	6.249	224.98
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	0.87	1.737	62.51		
19.80	70.0	Flexure	kip-ft	304.65	50.19	112.61	1.228	44.19	1.591	57.29
19.80	70.0	Shear	kip	-59.53	-3.30	-12.71	2.492	89.71	4.720	169.91
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	0.83	1.907	68.66		
22.63	80.0	Flexure	kip-ft	304.65	38.37	90.83	1.615	58.13	2.093	75.36
22.63	80.0	Shear	kip	-85.08	-5.12	-15.62	2.878	103.60	3.730	134.30
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	0.67	2.527	90.97		
25.46	90.0	Flexure	kip-ft	291.74	21.57	53.30	2.839	102.20	3.680	132.49
25.46	90.0	Shear	kip	-89.88	-6.76	-18.60	2.502	90.07	3.243	116.75
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.701	169.23		
26.81	94.8	Flexure	kip-ft	256.36	11.90	29.83	4.626	166.53	5.996	215.87
26.81	94.8	Shear	kip	-118.33	-7.55	-20.03	3.106	111.81	4.026	144.94
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.22	8.804	316.93		
27.11	95.8	Shear	kip	-125.83	-7.72	-20.35	3.262	117.43	4.228	152.22
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 1

Location						Inventory		Operating	
						Rating	Load Rating	Rating	Load Rating
(ft)	Percent		Units Capacity	LL	Factor		(Ton)	Factor	(Ton)

		Limit State			DL + Adj- LL*					
0.00	0.0	Flexure	kip- ft	88.32	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	129.09	7.72	19.93	3.425	123.31	4.440	159.85
1.69	6.0	Flexure	kip-ft	243.32	13.52	33.11	3.907	140.67	5.065	182.34
1.69	6.0	Shear	kip	118.17	7.42	19.47	3.196	115.05	4.143	149.13
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.24	7.870	283.33		
2.83	10.0	Flexure	kip-ft	284.36	21.61	52.96	2.777	99.96	3.599	129.57
2.83	10.0	Shear	kip	92.75	6.76	18.48	2.607	93.85	3.379	121.65
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.729	170.26		
5.66	20.0	Flexure	kip- ft	304.65	38.40	93.28	1.572	56.60	2.038	73.37
5.66	20.0	Shear	kip	85.08	5.11	16.06	2.801	100.82	3.630	130.69
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	0.69	2.460	88.57		
8.49	30.0	Flexure	kip- ft	304.65	50.23	120.96	1.143	41.13	1.481	53.32
8.49	30.0	Shear	kip	53.03	3.30	13.69	2.042	73.50	4.381	157.72
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	0.89	1.775	63.90		
11.32	40.0	Flexure	kip- ft	304.65	57.22	135.99	0.980	35.27	1.270	45.71
11.32	40.0	Shear	kip	45.04	1.65	11.37	2.159	77.74	4.245	152.83
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	1.00	1.515	54.53		
14.15	50.0	Flexure	kip- ft	304.65	59.54	138.38	0.951	34.23	1.232	44.37
14.15	50.0	Shear	kip	-44.95	-0.00	-9.11	2.818	101.46	5.444	195.99
14.15	50.0	Concrete Stresses	ksi	1.63	0.44	1.02	1.467	52.83		
16.98	60.0	Flexure	kip- ft	304.65	57.20	135.99	0.980	35.27	1.270	45.72
16.98	60.0	Shear	kip	-45.04	-1.65	-11.37	2.159	77.73	4.245	152.83
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	1.00	1.515	54.53		
19.80	70.0	Flexure	kip- ft	304.65	50.19	120.96	1.143	41.14	1.481	53.33
19.80	70.0	Shear	kip	-53.04	-3.30	-13.69	2.042	73.50	4.381	157.70
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	0.89	1.775	63.92		
22.63	80.0	Flexure		304.65	38.37	93.28	1.572	56.61	2.038	73.38

22.63	80.0	Shear	kip-ft	-85.08	-5.12	-16.06	2.800	100.81	3.630	130.68
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	0.69	2.461	88.58		
25.46	90.0	Flexure	kip-ft	291.74	21.57	52.96	2.857	102.85	3.703	133.32
25.46	90.0	Shear	kip	-89.88	-6.76	-18.48	2.518	90.64	3.264	117.50
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.730	170.30		
26.81	94.8	Flexure	kip-ft	256.36	11.90	29.27	4.715	169.73	6.112	220.02
26.81	94.8	Shear	kip	-118.33	-7.55	-19.65	3.166	113.97	4.104	147.74
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.22	8.973	323.03		
27.11	95.8	Shear	kip	-125.83	-7.72	-19.91	3.334	120.01	4.321	155.57
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	2772.00
1.17	4.1	Shear	kip	129.09	7.72	11.15	8.238	230.67
1.69	6.0	Flexure	kip-ft	243.32	13.52	18.41	9.462	264.94
1.69	6.0	Shear	kip	118.17	7.42	10.91	7.679	215.03
2.83	10.0	Flexure	kip-ft	284.36	21.61	29.33	6.749	188.96
2.83	10.0	Shear	kip	92.75	6.76	10.37	6.254	175.13
5.66	20.0	Flexure	kip-ft	304.65	38.40	51.10	3.864	108.18
5.66	20.0	Shear	kip	85.08	5.11	9.03	6.703	187.69
8.49	30.0	Flexure	kip-ft	304.65	50.23	65.30	2.849	79.78
8.49	30.0	Shear	kip	85.08	3.30	7.69	8.095	226.66
11.32	40.0	Flexure	kip-ft	304.65	57.22	71.93	2.493	69.81
11.32	40.0	Shear	kip	85.08	1.65	6.36	10.048	281.34
14.15	50.0	Flexure	kip-ft	304.65	59.54	70.99	2.495	69.85

14.15	50.0	Shear	kip	-85.08	-0.00	-5.02	13.040	365.13
16.98	60.0	Flexure	kip-ft	304.65	57.20	71.93	2.493	69.82
16.98	60.0	Shear	kip	-85.08	-1.65	-6.36	10.047	281.31
19.80	70.0	Flexure	kip-ft	304.65	50.19	65.30	2.850	79.80
19.80	70.0	Shear	kip	-85.08	-3.30	-7.69	8.094	226.64
22.63	80.0	Flexure	kip-ft	304.65	38.37	51.10	3.864	108.20
22.63	80.0	Shear	kip	-85.08	-5.12	-9.03	6.702	187.67
25.46	90.0	Flexure	kip-ft	291.74	21.57	29.33	6.944	194.42
25.46	90.0	Shear	kip	-89.88	-6.76	-10.37	6.041	169.14
26.81	94.8	Flexure	kip-ft	256.36	11.90	16.28	11.410	319.48
26.81	94.8	Shear	kip	-118.33	-7.55	-11.01	7.610	213.09
27.11	95.8	Shear	kip	-125.83	-7.72	-11.15	8.018	224.49
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3628.35
1.17	4.1	Shear	kip	129.09	7.72	15.66	5.867	215.02
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.63	6.797	249.10
1.69	6.0	Shear	kip	118.17	7.42	15.19	5.516	202.17
2.83	10.0	Flexure	kip-ft	284.36	21.61	40.46	4.892	179.30
2.83	10.0	Shear	kip	92.75	6.76	14.30	4.534	166.17
5.66	20.0	Flexure	kip-ft	304.65	38.40	71.13	2.775	101.72
5.66	20.0	Shear	kip	85.08	5.11	12.57	4.815	176.48
8.49	30.0	Flexure	kip-ft	304.65	50.23	92.01	2.022	74.11
8.49	30.0	Shear	kip	85.08	3.30	10.84	5.745	210.55
11.32	40.0	Flexure	kip-ft	304.65	57.22	103.09	1.739	63.75
11.32	40.0	Shear	kip	85.08	1.65	9.11	7.010	256.93
14.15	50.0	Flexure	kip-ft	304.65	59.54	104.38	1.697	62.18
14.15	50.0	Shear	kip	-85.08	-0.00	-7.38	8.869	325.04
16.98	60.0	Flexure	kip-ft	304.65	57.20	103.09	1.740	63.76
16.98	60.0	Shear	kip	-85.08	-1.65	-9.11	7.010	256.90
19.80	70.0	Flexure	kip-ft	304.65	50.19	92.01	2.022	74.12

19.80	70.0	Shear	kip	-85.08	-3.30	-10.84	5.744	210.53
22.63	80.0	Flexure	kip-ft	304.65	38.37	71.13	2.776	101.73
22.63	80.0	Shear	kip	-85.08	-5.12	-12.57	4.815	176.46
25.46	90.0	Flexure	kip-ft	291.74	21.57	40.46	5.034	184.49
25.46	90.0	Shear	kip	-89.88	-6.76	-14.30	4.379	160.50
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.74	8.167	299.32
26.81	94.8	Shear	kip	-118.33	-7.55	-15.38	5.447	199.65
27.11	95.8	Shear	kip	-125.83	-7.72	-15.65	5.711	209.30
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.09	7.72	15.73	5.842	233.70
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.93	6.717	268.67
1.69	6.0	Shear	kip	118.17	7.42	15.37	5.451	218.06
2.83	10.0	Flexure	kip-ft	284.36	21.61	41.23	4.802	192.06
2.83	10.0	Shear	kip	92.75	6.76	14.57	4.450	178.00
5.66	20.0	Flexure	kip-ft	304.65	38.40	71.33	2.768	110.72
5.66	20.0	Shear	kip	85.08	5.11	12.61	4.802	192.09
8.49	30.0	Flexure	kip-ft	304.65	50.23	90.30	2.060	82.42
8.49	30.0	Shear	kip	85.08	3.30	10.64	5.854	234.15
11.32	40.0	Flexure	kip-ft	304.65	57.22	98.14	1.827	73.09
11.32	40.0	Shear	kip	85.08	1.65	8.67	7.364	294.57
14.15	50.0	Flexure	kip-ft	304.65	59.54	103.05	1.719	68.74
14.15	50.0	Shear	kip	-85.08	-0.00	-6.71	9.756	390.22
16.98	60.0	Flexure	kip-ft	304.65	57.20	98.14	1.827	73.10
16.98	60.0	Shear	kip	-85.08	-1.65	-8.67	7.364	294.54
19.80	70.0	Flexure	kip-ft	304.65	50.19	90.30	2.061	82.43
19.80	70.0	Shear	kip	-85.08	-3.30	-10.64	5.853	234.13
22.63	80.0	Flexure	kip-ft	304.65	38.37	71.33	2.768	110.73
22.63	80.0	Shear	kip	-85.08	-5.12	-12.61	4.802	192.07
25.46	90.0	Flexure	kip-ft	291.74	21.57	41.23	4.940	197.62

25.46	90.0	Shear	kip	-89.88	-6.76	-14.57	4.298	171.92
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.94	8.096	323.85
26.81	94.8	Shear	kip	-118.33	-7.55	-15.51	5.400	216.01
27.11	95.8	Shear	kip	-125.83	-7.72	-15.72	5.686	227.44
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Permit	Permit
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	5940.00
1.69	6.0	Flexure	kip-ft	243.32	13.52	40.86	4.618	277.07
2.83	10.0	Flexure	kip-ft	284.36	21.61	64.51	3.324	199.45
5.66	20.0	Flexure	kip-ft	304.65	38.40	109.25	1.958	117.46
8.49	30.0	Flexure	kip-ft	304.65	50.23	134.22	1.502	90.10
11.32	40.0	Flexure	kip-ft	304.65	57.22	139.42	1.393	83.60
14.15	50.0	Flexure	kip-ft	304.65	59.54	125.17	1.533	91.97
16.98	60.0	Flexure	kip-ft	304.65	57.20	139.42	1.394	83.61
19.80	70.0	Flexure	kip-ft	304.65	50.19	134.22	1.502	90.12
22.63	80.0	Flexure	kip-ft	304.65	38.37	109.25	1.958	117.47
25.46	90.0	Flexure	kip-ft	291.74	21.57	64.51	3.420	205.22
26.81	94.8	Flexure	kip-ft	256.36	11.90	36.20	5.560	333.58
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating

(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.09	7.72	15.36	5.983	239.30
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.26	6.895	275.80
1.69	6.0	Shear	kip	118.17	7.42	14.97	5.596	223.84
2.83	10.0	Flexure	kip-ft	284.36	21.61	39.92	4.958	198.33
2.83	10.0	Shear	kip	92.75	6.76	14.11	4.595	183.81
5.66	20.0	Flexure	kip-ft	304.65	38.40	67.83	2.911	116.42
5.66	20.0	Shear	kip	85.08	5.11	11.99	5.050	201.99
8.49	30.0	Flexure	kip-ft	304.65	50.23	83.72	2.222	88.89
8.49	30.0	Shear	kip	85.08	3.30	9.86	6.314	252.56
11.32	40.0	Flexure	kip-ft	304.65	57.22	93.25	1.923	76.92
11.32	40.0	Shear	kip	85.08	1.65	7.74	8.252	330.08
14.15	50.0	Flexure	kip-ft	304.65	59.54	93.59	1.892	75.69
14.15	50.0	Shear	kip	-85.08	-0.00	-6.08	10.765	430.60
16.98	60.0	Flexure	kip-ft	304.65	57.20	93.25	1.923	76.93
16.98	60.0	Shear	kip	-85.08	-1.65	-7.74	8.251	330.04
19.80	70.0	Flexure	kip-ft	304.65	50.19	83.72	2.223	88.91
19.80	70.0	Shear	kip	-85.08	-3.30	-9.86	6.313	252.53
22.63	80.0	Flexure	kip-ft	304.65	38.37	67.83	2.911	116.44
22.63	80.0	Shear	kip	-85.08	-5.12	-11.99	5.049	201.97
25.46	90.0	Flexure	kip-ft	291.74	21.57	39.92	5.102	204.07
25.46	90.0	Shear	kip	-89.88	-6.76	-14.11	4.438	177.53
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.37	8.303	332.11
26.81	94.8	Shear	kip	-118.33	-7.55	-15.13	5.538	221.51
27.11	95.8	Shear	kip	-125.83	-7.72	-15.35	5.823	232.91
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	1683.00
1.17	4.1	Shear	kip	129.09	7.72	10.65	8.625	146.63

1.69	6.0	Flexure	kip-ft	243.32	13.52	17.56	9.917	168.59
1.69	6.0	Shear	kip	118.17	7.42	10.41	8.049	136.83
2.83	10.0	Flexure	kip-ft	284.36	21.61	27.92	7.091	120.54
2.83	10.0	Shear	kip	92.75	6.76	9.87	6.572	111.72
5.66	20.0	Flexure	kip-ft	304.65	38.40	48.27	4.090	69.54
5.66	20.0	Shear	kip	85.08	5.11	8.53	7.097	120.64
8.49	30.0	Flexure	kip-ft	304.65	50.23	61.05	3.047	51.81
8.49	30.0	Shear	kip	85.08	3.30	7.19	8.658	147.19
11.32	40.0	Flexure	kip-ft	304.65	57.22	66.26	2.706	46.01
11.32	40.0	Shear	kip	85.08	1.65	5.86	10.907	185.42
14.15	50.0	Flexure	kip-ft	304.65	59.54	63.91	2.771	47.11
14.15	50.0	Shear	kip	-85.08	-0.00	-4.52	14.485	246.24
16.98	60.0	Flexure	kip-ft	304.65	57.20	66.26	2.707	46.01
16.98	60.0	Shear	kip	-85.08	-1.65	-5.86	10.906	185.40
19.80	70.0	Flexure	kip-ft	304.65	50.19	61.05	3.048	51.82
19.80	70.0	Shear	kip	-85.08	-3.30	-7.19	8.657	147.18
22.63	80.0	Flexure	kip-ft	304.65	38.37	48.27	4.091	69.54
22.63	80.0	Shear	kip	-85.08	-5.12	-8.53	7.096	120.63
25.46	90.0	Flexure	kip-ft	291.74	21.57	27.92	7.296	124.03
25.46	90.0	Shear	kip	-89.88	-6.76	-9.87	6.347	107.90
26.81	94.8	Flexure	kip-ft	256.36	11.90	15.54	11.954	203.21
26.81	94.8	Shear	kip	-118.33	-7.55	-10.51	7.973	135.54
27.11	95.8	Shear	kip	-125.83	-7.72	-10.65	8.394	142.71
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3267.00
1.17	4.1	Shear	kip	129.09	7.72	18.97	4.842	159.80
1.69	6.0	Flexure	kip-ft	243.32	13.52	31.22	5.579	184.12
1.69	6.0	Shear	kip	118.17	7.42	18.50	4.528	149.43
2.83	10.0	Flexure	kip-ft	284.36	21.61	49.37	4.009	132.31
2.83	10.0	Shear	kip	92.75	6.76	17.45	3.716	122.62

5.66	20.0	Flexure	kip-ft	304.65	38.40	84.06	2.349	77.51
5.66	20.0	Shear	kip	85.08	5.11	14.86	4.075	134.48
8.49	30.0	Flexure	kip-ft	304.65	50.23	104.05	1.788	59.01
8.49	30.0	Shear	kip	85.08	3.30	12.26	5.080	167.65
11.32	40.0	Flexure	kip-ft	304.65	57.22	116.56	1.538	50.77
11.32	40.0	Shear	kip	85.08	1.65	9.66	6.609	218.10
14.15	50.0	Flexure	kip-ft	304.65	59.54	118.00	1.501	49.53
14.15	50.0	Shear	kip	-85.08	-0.00	-7.38	8.869	292.67
16.98	60.0	Flexure	kip-ft	304.65	57.20	116.56	1.539	50.77
16.98	60.0	Shear	kip	-85.08	-1.65	-9.66	6.609	218.08
19.80	70.0	Flexure	kip-ft	304.65	50.19	104.05	1.788	59.02
19.80	70.0	Shear	kip	-85.08	-3.30	-12.26	5.080	167.63
22.63	80.0	Flexure	kip-ft	304.65	38.37	84.06	2.349	77.52
22.63	80.0	Shear	kip	-85.08	-5.12	-14.86	4.075	134.46
25.46	90.0	Flexure	kip-ft	291.74	21.57	49.37	4.125	136.14
25.46	90.0	Shear	kip	-89.88	-6.76	-17.45	3.589	118.44
26.81	94.8	Flexure	kip-ft	256.36	11.90	27.65	6.719	221.73
26.81	94.8	Shear	kip	-118.33	-7.55	-18.69	4.482	147.89
27.11	95.8	Shear	kip	-125.83	-7.72	-18.96	4.713	155.53
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - (w/ Post Tensioning)

SU 4

Axle Load

Impact: With Impact

Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3465.00
1.17	4.1	Shear	kip	129.09	7.72	19.76	4.649	162.71
1.69	6.0	Flexure	kip-ft	243.32	13.52	32.50	5.359	187.56
1.69	6.0	Shear	kip	118.17	7.42	19.26	4.349	152.22
2.83	10.0	Flexure	kip-ft	284.36	21.61	51.35	3.855	134.94
2.83	10.0	Shear	kip	92.75	6.76	18.15	3.573	125.06
5.66	20.0	Flexure	kip-ft	304.65	38.40	87.11	2.266	79.32
5.66	20.0	Shear	kip	85.08	5.11	15.40	3.932	137.62
8.49	30.0	Flexure	kip-ft	304.65	50.23	111.07	1.675	58.63
8.49	30.0	Shear	kip	85.08	3.30	12.64	4.926	172.42

11.32	40.0	Flexure	kip-ft	304.65	57.22	127.15	1.410	49.36
11.32	40.0	Shear	kip	84.27	1.65	9.99	6.330	221.56
14.15	50.0	Flexure	kip-ft	304.65	59.54	127.65	1.387	48.56
14.15	50.0	Shear	kip	-85.08	-0.00	-7.78	8.408	294.29
16.98	60.0	Flexure	kip-ft	304.65	57.20	127.15	1.411	49.37
16.98	60.0	Shear	kip	-84.29	-1.65	-9.99	6.331	221.58
19.80	70.0	Flexure	kip-ft	304.65	50.19	111.07	1.675	58.64
19.80	70.0	Shear	kip	-85.08	-3.30	-12.64	4.926	172.40
22.63	80.0	Flexure	kip-ft	304.65	38.37	87.11	2.267	79.33
22.63	80.0	Shear	kip	-85.08	-5.12	-15.40	3.932	137.61
25.46	90.0	Flexure	kip-ft	291.74	21.57	51.35	3.967	138.84
25.46	90.0	Shear	kip	-89.88	-6.76	-18.15	3.451	120.79
26.81	94.8	Flexure	kip-ft	256.36	11.90	28.79	6.452	225.84
26.81	94.8	Shear	kip	-118.33	-7.55	-19.46	4.304	150.63
27.11	95.8	Shear	kip	-125.83	-7.72	-19.75	4.525	158.36
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294
Bridge ID: 874294

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 15:31:36
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 15:32:03

Structure Definition Name: INT Span 2 - PS Conc PSU
Member Name: G3
Member Alternative Name: 17"x36" INT PSU - Existing Condition

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - Existing Condition
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	1.08	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	112.74	10.73	48.83	1.162	41.84	1.507	54.24
1.48	3.8	Flexure	kip-ft	408.30	16.29	71.63	3.095	111.40	4.011	144.41
1.48	3.8	Shear	kip	106.69	10.52	48.15	1.110	39.96	1.439	51.80
1.48	3.8	Concrete Stresses	ksi	2.45	0.12	0.53	5.535	199.26		
3.85	10.0	Flexure	kip-ft	462.73	39.60	171.07	1.380	49.69	1.789	64.41
3.85	10.0	Shear	kip	76.71	9.14	43.77	0.852	30.69	1.159	41.74
3.85	10.0	Concrete Stresses	ksi	2.45	0.29	1.26	2.147	77.31		
7.70	20.0	Flexure	kip-ft	462.73	70.46	292.21	0.733	26.37	0.950	34.19
7.70	20.0	Shear	kip	32.51	6.89	36.77	0.371	13.37	0.771	27.74
7.70	20.0	Concrete Stresses	ksi	2.45	0.52	2.15	1.125	40.50		
11.55	30.0	Flexure	kip-ft	462.73	92.31	365.43	0.543	19.55	0.704	25.35
11.55	30.0	Shear	kip	24.35	4.49	30.09	0.356	12.81	0.698	25.14
11.55	30.0	Concrete Stresses	ksi	2.45	0.68	2.69	0.825	29.70		
15.40	40.0	Flexure	kip-ft	462.73	105.27	402.57	0.470	16.92	0.609	21.94
15.40	40.0	Shear	kip	22.39	2.24	24.02	0.466	16.78	0.839	30.20
15.40	40.0	Concrete Stresses	ksi	2.45	0.77	2.96	0.709	25.51		
19.25	50.0	Flexure	kip-ft	462.73	109.59	400.72	0.465	16.72	0.602	21.68
19.25	50.0	Shear	kip	-22.39	0.00	-18.10	0.707	25.46	1.251	45.02
19.25	50.0		ksi	2.45	0.81	2.95	0.698	25.14		

		Concrete Stresses									
23.10	60.0	Flexure	kip-ft	462.73	105.27	402.57	0.470	16.92	0.609	21.94	
23.10	60.0	Shear	kip	-22.39	-2.24	-24.02	0.466	16.78	0.839	30.20	
23.10	60.0	Concrete Stresses	ksi	2.45	0.77	2.96	0.709	25.51			
26.95	70.0	Flexure	kip-ft	480.13	92.31	365.43	0.570	20.53	0.739	26.62	
26.95	70.0	Shear	kip	-27.52	-4.49	-30.09	0.416	14.98	0.781	28.10	
26.95	70.0	Concrete Stresses	ksi	2.45	0.68	2.69	0.825	29.70			
30.80	80.0	Flexure	kip-ft	462.73	70.46	292.21	0.733	26.37	0.950	34.19	
30.80	80.0	Shear	kip	-32.51	-6.89	-36.77	0.371	13.37	0.771	27.74	
30.80	80.0	Concrete Stresses	ksi	2.45	0.52	2.15	1.125	40.50			
34.65	90.0	Flexure	kip-ft	462.73	39.60	171.07	1.380	49.69	1.789	64.41	
34.65	90.0	Shear	kip	-76.71	-9.14	-43.77	0.852	30.69	1.159	41.74	
34.65	90.0	Concrete Stresses	ksi	2.45	0.29	1.26	2.147	77.31			
37.02	96.2	Flexure	kip-ft	408.30	16.29	71.63	3.095	111.41	4.012	144.41	
37.02	96.2	Shear	kip	-106.69	-10.52	-48.15	1.110	39.96	1.439	51.80	
37.02	96.2	Concrete Stresses	ksi	2.45	0.12	0.53	5.535	199.26			
37.39	97.1	Shear	kip	-112.75	-10.73	-48.84	1.162	41.84	1.507	54.24	
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3564.00	99.000	3564.00	
38.50	100.0	Concrete Stresses	ksi	1.08	0.00	0.00	99.000	3564.00			

Detailed Rating Results
17"x36" INT PSU - Existing Condition
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 2

Location								Inventory	Inventory	Operating	Operating
								Rating	Load Rating	Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor		(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000		3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	1.08	-0.00	0.00	99.000		3564.00		

1.12	2.9	Shear	kip	112.74	10.73	43.64	1.300	46.82	1.686	60.69
1.48	3.8	Flexure	kip-ft	408.30	16.29	64.20	3.453	124.30	4.476	161.14
1.48	3.8	Shear	kip	106.69	10.52	43.13	1.239	44.62	1.607	57.84
1.48	3.8	Concrete Stresses	ksi	2.45	0.12	0.47	6.176	222.33		
3.85	10.0	Flexure	kip-ft	462.73	39.60	155.89	1.515	54.53	1.964	70.69
3.85	10.0	Shear	kip	79.93	9.14	39.82	0.983	35.39	1.274	45.87
3.85	10.0	Concrete Stresses	ksi	2.45	0.29	1.15	2.357	84.84		
7.70	20.0	Flexure	kip-ft	462.73	70.46	275.36	0.777	27.99	1.008	36.28
7.70	20.0	Shear	kip	35.22	6.89	34.58	0.440	15.83	0.919	33.10
7.70	20.0	Concrete Stresses	ksi	2.45	0.52	2.02	1.194	42.98		
11.55	30.0	Flexure	kip-ft	462.73	92.31	358.42	0.554	19.94	0.718	25.84
11.55	30.0	Shear	kip	24.98	4.49	29.48	0.375	13.52	0.734	26.44
11.55	30.0	Concrete Stresses	ksi	2.45	0.68	2.64	0.841	30.28		
15.40	40.0	Flexure	kip-ft	462.73	105.27	405.06	0.467	16.82	0.606	21.80
15.40	40.0	Shear	kip	22.39	2.24	24.53	0.456	16.43	0.813	29.28
15.40	40.0	Concrete Stresses	ksi	2.45	0.77	2.98	0.704	25.35		
19.25	50.0	Flexure	kip-ft	462.73	109.59	415.29	0.448	16.14	0.581	20.92
19.25	50.0	Shear	kip	-22.39	0.00	-19.73	0.649	23.36	1.095	39.40
19.25	50.0	Concrete Stresses	ksi	2.45	0.81	3.05	0.674	24.26		
23.10	60.0	Flexure	kip-ft	462.73	105.27	405.06	0.467	16.82	0.606	21.80
23.10	60.0	Shear	kip	-22.39	-2.24	-24.53	0.456	16.43	0.813	29.28
23.10	60.0	Concrete Stresses	ksi	2.45	0.77	2.98	0.704	25.35		
26.95	70.0	Flexure	kip-ft	480.13	92.31	358.42	0.582	20.93	0.754	27.14
26.95	70.0	Shear	kip	-28.16	-4.49	-29.48	0.437	15.74	0.819	29.47
26.95	70.0	Concrete Stresses	ksi	2.45	0.68	2.64	0.841	30.28		
30.80	80.0	Flexure	kip-ft	462.73	70.46	275.36	0.777	27.99	1.008	36.28
30.80	80.0	Shear	kip	-35.22	-6.89	-34.58	0.440	15.83	0.919	33.10
30.80	80.0	Concrete Stresses	ksi	2.45	0.52	2.02	1.194	42.98		
34.65	90.0	Flexure	kip-ft	462.73	39.60	155.89	1.515	54.53	1.964	70.69
34.65	90.0	Shear	kip	-79.93	-9.14	-39.82	0.983	35.39	1.274	45.87
34.65	90.0	Concrete Stresses	ksi	2.45	0.29	1.15	2.357	84.84		
37.02	96.2	Flexure	kip-ft	408.30	16.29	64.20	3.453	124.30	4.476	161.14
37.02	96.2	Shear	kip	-106.69	-10.52	-43.13	1.239	44.62	1.607	57.84
37.02	96.2	Concrete Stresses	ksi	2.45	0.12	0.47	6.176	222.33		

37.39	97.1	Shear	kip	-112.75	-10.73	-43.64	1.301	46.82	1.686	60.69
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	1.08	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	2772.00
1.12	2.9	Shear	kip	112.74	10.73	26.81	2.850	79.79
1.48	3.8	Flexure	kip-ft	408.30	16.29	39.03	7.645	214.05
1.48	3.8	Shear	kip	106.69	10.52	26.39	2.727	76.35
3.85	10.0	Flexure	kip-ft	462.73	39.60	91.00	3.493	97.80
3.85	10.0	Shear	kip	79.93	9.14	23.64	2.229	62.42
7.70	20.0	Flexure	kip-ft	462.73	70.46	147.98	1.947	54.53
7.70	20.0	Shear	kip	79.93	6.89	19.22	2.854	79.92
11.55	30.0	Flexure	kip-ft	462.73	92.31	190.63	1.402	39.24
11.55	30.0	Shear	kip	79.93	4.49	16.51	3.464	96.98
15.40	40.0	Flexure	kip-ft	462.73	105.27	215.01	1.185	33.17
15.40	40.0	Shear	kip	79.93	2.24	13.79	4.301	120.44
19.25	50.0	Flexure	kip-ft	462.73	109.59	213.27	1.175	32.90
19.25	50.0	Shear	kip	79.93	0.00	11.08	5.550	155.39
23.10	60.0	Flexure	kip-ft	462.73	105.27	215.01	1.185	33.17
23.10	60.0	Shear	kip	-79.93	-2.24	-13.79	4.301	120.44
26.95	70.0	Flexure	kip-ft	480.13	92.31	190.63	1.472	41.21
26.95	70.0	Shear	kip	-80.21	-4.49	-16.51	3.477	97.35
30.80	80.0	Flexure	kip-ft	462.73	70.46	147.98	1.947	54.53
30.80	80.0	Shear	kip	-79.93	-6.89	-19.22	2.854	79.92
34.65	90.0	Flexure	kip-ft	462.73	39.60	91.00	3.493	97.80
34.65	90.0	Shear	kip	-79.93	-9.14	-23.64	2.229	62.42
37.02	96.2	Flexure	kip-ft	408.30	16.29	39.03	7.645	214.05
37.02	96.2	Shear	kip	-106.69	-10.52	-26.39	2.727	76.35
37.39	97.1	Shear	kip	-112.75	-10.73	-26.81	2.850	79.79
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3628.35
1.12	2.9	Shear	kip	112.74	10.73	37.60	2.032	74.48
1.48	3.8	Flexure	kip-ft	408.30	16.29	54.79	5.446	199.60
1.48	3.8	Shear	kip	106.69	10.52	37.04	1.943	71.19
3.85	10.0	Flexure	kip-ft	462.73	39.60	129.53	2.454	89.94
3.85	10.0	Shear	kip	79.93	9.14	33.65	1.566	57.40
7.70	20.0	Flexure	kip-ft	462.73	70.46	218.51	1.319	48.34
7.70	20.0	Shear	kip	79.93	6.89	28.38	1.933	70.84
11.55	30.0	Flexure	kip-ft	462.73	92.31	266.94	1.001	36.68
11.55	30.0	Shear	kip	55.52	4.49	23.11	1.661	60.88
15.40	40.0	Flexure	kip-ft	462.73	105.27	295.17	0.863	31.63
15.40	40.0	Shear	kip	46.74	2.24	19.17	1.763	64.63
19.25	50.0	Flexure	kip-ft	462.73	109.59	301.38	0.831	30.47
19.25	50.0	Shear	kip	-45.84	0.00	-15.66	2.252	82.55
23.10	60.0	Flexure	kip-ft	462.73	105.27	295.17	0.863	31.63
23.10	60.0	Shear	kip	-46.74	-2.24	-19.17	1.763	64.63
26.95	70.0	Flexure	kip-ft	480.13	92.31	266.94	1.051	38.52
26.95	70.0	Shear	kip	-58.64	-4.49	-23.11	1.765	64.69
30.80	80.0	Flexure	kip-ft	462.73	70.46	218.51	1.319	48.34
30.80	80.0	Shear	kip	-79.93	-6.89	-28.38	1.933	70.84
34.65	90.0	Flexure	kip-ft	462.73	39.60	129.53	2.454	89.94
34.65	90.0	Shear	kip	-79.93	-9.14	-33.65	1.566	57.40
37.02	96.2	Flexure	kip-ft	408.30	16.29	54.79	5.446	199.60
37.02	96.2	Shear	kip	-106.69	-10.52	-37.04	1.943	71.19
37.39	97.1	Shear	kip	-112.75	-10.73	-37.60	2.032	74.48
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - Existing Condition
C 5

Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	112.74	10.73	37.64	2.030	81.19
1.48	3.8	Flexure	kip-ft	408.30	16.29	54.90	5.436	217.43
1.48	3.8	Shear	kip	106.69	10.52	37.11	1.939	77.55
3.85	10.0	Flexure	kip-ft	462.73	39.60	129.65	2.452	98.07
3.85	10.0	Shear	kip	79.93	9.14	33.67	1.565	62.59
7.70	20.0	Flexure	kip-ft	462.73	70.46	216.28	1.332	53.30
7.70	20.0	Shear	kip	79.93	6.89	28.09	1.953	78.12
11.55	30.0	Flexure	kip-ft	462.73	92.31	268.72	0.994	39.77
11.55	30.0	Shear	kip	54.91	4.49	23.27	1.630	65.20
15.40	40.0	Flexure	kip-ft	462.73	105.27	300.26	0.848	33.93
15.40	40.0	Shear	kip	45.69	2.24	19.28	1.711	68.45
19.25	50.0	Flexure	kip-ft	462.73	109.59	310.88	0.806	32.24
19.25	50.0	Shear	kip	-44.19	0.00	-14.79	2.298	91.91
23.10	60.0	Flexure	kip-ft	462.73	105.27	300.26	0.848	33.93
23.10	60.0	Shear	kip	-45.69	-2.24	-19.28	1.711	68.45
26.95	70.0	Flexure	kip-ft	480.13	92.31	268.72	1.044	41.76
26.95	70.0	Shear	kip	-58.05	-4.49	-23.27	1.734	69.36
30.80	80.0	Flexure	kip-ft	462.73	70.46	216.28	1.332	53.30
30.80	80.0	Shear	kip	-79.93	-6.89	-28.09	1.953	78.12
34.65	90.0	Flexure	kip-ft	462.73	39.60	129.65	2.452	98.07
34.65	90.0	Shear	kip	-79.93	-9.14	-33.67	1.565	62.59
37.02	96.2	Flexure	kip-ft	408.30	16.29	54.90	5.436	217.43
37.02	96.2	Shear	kip	-106.69	-10.52	-37.11	1.939	77.55
37.39	97.1	Shear	kip	-112.75	-10.73	-37.64	2.030	81.19
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Permit Rating	Permit Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	5940.00
1.48	3.8	Flexure	kip-ft	408.30	16.29	84.85	3.810	228.59
3.85	10.0	Flexure	kip-ft	462.73	39.60	201.93	1.705	102.32
7.70	20.0	Flexure	kip-ft	462.73	70.46	342.42	0.912	54.71
11.55	30.0	Flexure	kip-ft	462.73	92.31	424.27	0.682	40.93
15.40	40.0	Flexure	kip-ft	462.73	105.27	464.01	0.595	35.68
19.25	50.0	Flexure	kip-ft	462.73	109.59	457.59	0.593	35.59
23.10	60.0	Flexure	kip-ft	462.73	105.27	464.01	0.595	35.68
26.95	70.0	Flexure	kip-ft	480.13	92.31	424.27	0.716	42.98
30.80	80.0	Flexure	kip-ft	462.73	70.46	342.42	0.912	54.71
34.65	90.0	Flexure	kip-ft	462.73	39.60	201.93	1.705	102.32
37.02	96.2	Flexure	kip-ft	408.30	16.29	84.85	3.810	228.59
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	112.74	10.73	34.38	2.222	88.88
1.48	3.8	Flexure	kip-ft	408.30	16.29	50.25	5.938	237.52
1.48	3.8	Shear	kip	106.69	10.52	33.97	2.118	84.72
3.85	10.0	Flexure	kip-ft	462.73	39.60	120.59	2.636	105.44
3.85	10.0	Shear	kip	79.93	9.14	31.32	1.682	67.30
7.70	20.0	Flexure	kip-ft	462.73	70.46	207.99	1.386	55.42
7.70	20.0	Shear	kip	79.93	6.89	27.01	2.031	81.23
11.55	30.0	Flexure	kip-ft	462.73	92.31	262.21	1.019	40.76
11.55	30.0	Shear	kip	57.20	4.49	22.70	1.748	69.93
15.40	40.0	Flexure	kip-ft	462.73	105.27	294.75	0.864	34.57
15.40	40.0	Shear	kip	47.00	2.24	18.39	1.848	73.94

19.25	50.0	Flexure	kip-ft	462.73	109.59	299.85	0.836	33.43
19.25	50.0	Shear	kip	-46.49	0.00	-14.08	2.539	101.56
23.10	60.0	Flexure	kip-ft	462.73	105.27	294.75	0.864	34.57
23.10	60.0	Shear	kip	-47.00	-2.24	-18.39	1.848	73.94
26.95	70.0	Flexure	kip-ft	480.13	92.31	262.21	1.070	42.80
26.95	70.0	Shear	kip	-60.25	-4.49	-22.70	1.851	74.05
30.80	80.0	Flexure	kip-ft	462.73	70.46	207.99	1.386	55.42
30.80	80.0	Shear	kip	-79.93	-6.89	-27.01	2.031	81.23
34.65	90.0	Flexure	kip-ft	462.73	39.60	120.59	2.636	105.44
34.65	90.0	Shear	kip	-79.93	-9.14	-31.32	1.682	67.30
37.02	96.2	Flexure	kip-ft	408.30	16.29	50.25	5.938	237.52
37.02	96.2	Shear	kip	-106.69	-10.52	-33.97	2.118	84.72
37.39	97.1	Shear	kip	-112.75	-10.73	-34.38	2.222	88.89
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load
(ft)	Percent	Limit	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	1683.00
1.12	2.9	Shear	kip	112.74	10.73	23.11	3.306	56.19
1.48	3.8	Flexure	kip-ft	408.30	16.29	33.81	8.827	150.05
1.48	3.8	Shear	kip	106.69	10.52	22.86	3.148	53.52
3.85	10.0	Flexure	kip-ft	462.73	39.60	81.56	3.897	66.25
3.85	10.0	Shear	kip	79.93	9.14	21.19	2.487	42.29
7.70	20.0	Flexure	kip-ft	462.73	70.46	142.24	2.026	34.44
7.70	20.0	Shear	kip	79.93	6.89	18.47	2.970	50.48
11.55	30.0	Flexure	kip-ft	462.73	92.31	182.02	1.468	24.95
11.55	30.0	Shear	kip	79.93	4.49	15.76	3.628	61.67
15.40	40.0	Flexure	kip-ft	462.73	105.27	200.90	1.268	21.55
15.40	40.0	Shear	kip	79.93	2.24	13.05	4.547	77.31
19.25	50.0	Flexure	kip-ft	462.73	109.59	198.90	1.260	21.42
19.25	50.0	Shear	kip	79.93	0.00	10.33	5.950	101.16
23.10	60.0	Flexure	kip-ft	462.73	105.27	200.90	1.268	21.55
23.10	60.0	Shear	kip	-79.93	-2.24	-13.05	4.547	77.31

26.95	70.0	Flexure	kip-ft	480.13	92.31	182.02	1.541	26.20
26.95	70.0	Shear	kip	-80.21	-4.49	-15.76	3.641	61.90
30.80	80.0	Flexure	kip-ft	462.73	70.46	142.24	2.026	34.44
30.80	80.0	Shear	kip	-79.93	-6.89	-18.47	2.970	50.48
34.65	90.0	Flexure	kip-ft	462.73	39.60	81.56	3.897	66.25
34.65	90.0	Shear	kip	-79.93	-9.14	-21.19	2.487	42.29
37.02	96.2	Flexure	kip-ft	408.30	16.29	33.81	8.827	150.05
37.02	96.2	Shear	kip	-106.69	-10.52	-22.86	3.148	53.52
37.39	97.1	Shear	kip	-112.75	-10.73	-23.11	3.306	56.20
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition

SU 3

Axle Load

Impact: With Impact

Lane: Single Lane

Span 2

Location							Legal Rating	Legal Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3267.00
1.12	2.9	Shear	kip	112.74	10.73	42.33	1.805	59.57
1.48	3.8	Flexure	kip-ft	408.30	16.29	61.87	4.823	159.16
1.48	3.8	Shear	kip	106.69	10.52	41.83	1.720	56.77
3.85	10.0	Flexure	kip-ft	462.73	39.60	148.55	2.140	70.61
3.85	10.0	Shear	kip	79.93	9.14	38.58	1.366	45.07
7.70	20.0	Flexure	kip-ft	462.73	70.46	256.55	1.123	37.07
7.70	20.0	Shear	kip	62.13	6.89	33.32	1.236	40.77
11.55	30.0	Flexure	kip-ft	462.73	92.31	323.99	0.825	27.21
11.55	30.0	Shear	kip	41.63	4.49	28.05	0.988	32.59
15.40	40.0	Flexure	kip-ft	462.73	105.27	365.51	0.697	23.00
15.40	40.0	Shear	kip	35.37	2.24	22.78	1.099	36.28
19.25	50.0	Flexure	kip-ft	462.73	109.59	373.79	0.670	22.12
19.25	50.0	Shear	kip	-34.84	0.00	-17.52	1.530	50.49
23.10	60.0	Flexure	kip-ft	462.73	105.27	365.51	0.697	23.00
23.10	60.0	Shear	kip	-35.37	-2.24	-22.78	1.099	36.28
26.95	70.0	Flexure	kip-ft	480.13	92.31	323.99	0.866	28.58
26.95	70.0	Shear	kip	-45.02	-4.49	-28.05	1.081	35.66
30.80	80.0	Flexure	kip-ft	462.73	70.46	256.55	1.123	37.07
30.80	80.0	Shear	kip	-62.13	-6.89	-33.32	1.236	40.77

34.65	90.0	Flexure	kip-ft	462.73	39.60	148.55	2.140	70.61
34.65	90.0	Shear	kip	-79.93	-9.14	-38.58	1.366	45.07
37.02	96.2	Flexure	kip-ft	408.30	16.29	61.87	4.823	159.16
37.02	96.2	Shear	kip	-106.69	-10.52	-41.83	1.720	56.77
37.39	97.1	Shear	kip	-112.75	-10.73	-42.33	1.805	59.57
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - Existing Condition
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.43	0.00	0.00	99.000	3465.00
1.12	2.9	Shear	kip	112.74	10.73	44.35	1.723	60.29
1.48	3.8	Flexure	kip-ft	408.30	16.29	64.83	4.603	161.11
1.48	3.8	Shear	kip	106.69	10.52	43.83	1.642	57.46
3.85	10.0	Flexure	kip-ft	462.73	39.60	155.49	2.044	71.55
3.85	10.0	Shear	kip	79.93	9.14	40.39	1.305	45.67
7.70	20.0	Flexure	kip-ft	462.73	70.46	267.96	1.075	37.64
7.70	20.0	Shear	kip	57.26	6.89	34.80	1.075	37.63
11.55	30.0	Flexure	kip-ft	462.73	92.31	345.07	0.774	27.10
11.55	30.0	Shear	kip	38.34	4.49	29.21	0.862	30.16
15.40	40.0	Flexure	kip-ft	462.73	105.27	394.80	0.645	22.58
15.40	40.0	Shear	kip	32.21	2.24	23.63	0.957	33.51
19.25	50.0	Flexure	kip-ft	462.73	109.59	401.52	0.624	21.84
19.25	50.0	Shear	kip	-31.95	0.00	-18.04	1.362	47.67
23.10	60.0	Flexure	kip-ft	462.73	105.27	394.80	0.645	22.58
23.10	60.0	Shear	kip	-32.21	-2.24	-23.63	0.957	33.51
26.95	70.0	Flexure	kip-ft	480.13	92.31	345.07	0.813	28.46
26.95	70.0	Shear	kip	-41.72	-4.49	-29.21	0.951	33.28
30.80	80.0	Flexure	kip-ft	462.73	70.46	267.96	1.075	37.64
30.80	80.0	Shear	kip	-57.26	-6.89	-34.80	1.075	37.63
34.65	90.0	Flexure	kip-ft	462.73	39.60	155.49	2.044	71.55
34.65	90.0	Shear	kip	-79.93	-9.14	-40.39	1.305	45.67
37.02	96.2	Flexure	kip-ft	408.30	16.29	64.83	4.603	161.11
37.02	96.2	Shear	kip	-106.69	-10.52	-43.83	1.642	57.46

37.39	97.1	Shear	kip	-112.75	-10.73	-44.36	1.723	60.29
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294
Bridge ID: 874294

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 15:34:40
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 15:35:19

Structure Definition Name: INT Span 2 - PS Conc PSU
Member Name: G10
Member Alternative Name: 17"x36" INT PSU - w/ post Tensioning

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	1.08	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	112.73	10.73	20.86	2.720	97.92	3.526	126.94
1.48	3.8	Flexure	kip-ft	408.30	16.29	30.61	7.243	260.75	9.389	338.01
1.48	3.8	Shear	kip	106.69	10.52	20.57	2.598	93.53	3.368	121.24
1.48	3.8	Concrete Stresses	ksi	2.45	0.12	0.23	12.955	466.37		
3.85	10.0	Flexure	kip-ft	462.73	39.60	73.09	3.231	116.30	4.188	150.76
3.85	10.0	Shear	kip	79.93	9.14	18.70	2.093	75.36	2.714	97.69
3.85	10.0	Concrete Stresses	ksi	2.45	0.29	0.54	5.026	180.94		
7.70	20.0	Flexure	kip-ft	462.73	70.46	124.85	1.715	61.73	2.223	80.02
7.70	20.0	Shear	kip	79.93	6.89	15.71	2.594	93.38	3.363	121.05
7.70	20.0	Concrete Stresses	ksi	2.45	0.52	0.92	2.633	94.80		
11.55	30.0	Flexure	kip-ft	462.73	92.31	156.13	1.271	45.76	1.648	59.32
11.55	30.0	Shear	kip	79.93	4.49	12.85	3.304	118.93	4.283	154.17
11.55	30.0	Concrete Stresses	ksi	2.45	0.68	1.15	1.931	69.51		
15.40	40.0	Flexure	kip-ft	462.73	105.27	172.00	1.100	39.61	1.426	51.34
15.40	40.0	Shear	kip	70.23	2.24	10.26	3.754	135.16	5.567	200.41
15.40	40.0	Concrete Stresses	ksi	2.45	0.77	1.26	1.659	59.71		
19.25	50.0	Flexure	kip-ft	462.73	109.59	171.21	1.087	39.14	1.409	50.74

19.25	50.0	Shear	kip	-71.82	0.00	-7.73	5.308	191.08	7.657	275.64
19.25	50.0	Concrete Stresses	ksi	2.45	0.81	1.26	1.635	58.85		
23.10	60.0	Flexure	kip-ft	462.73	105.27	172.00	1.100	39.61	1.426	51.34
23.10	60.0	Shear	kip	-70.23	-2.24	-10.26	3.754	135.16	5.567	200.41
23.10	60.0	Concrete Stresses	ksi	2.45	0.77	1.26	1.659	59.71		
26.95	70.0	Flexure	kip-ft	480.13	92.31	156.13	1.335	48.06	1.730	62.30
26.95	70.0	Shear	kip	-80.21	-4.49	-12.85	3.316	119.38	4.299	154.75
26.95	70.0	Concrete Stresses	ksi	2.45	0.68	1.15	1.931	69.51		
30.80	80.0	Flexure	kip-ft	462.73	70.46	124.85	1.715	61.73	2.223	80.02
30.80	80.0	Shear	kip	-79.93	-6.89	-15.71	2.594	93.38	3.363	121.05
30.80	80.0	Concrete Stresses	ksi	2.45	0.52	0.92	2.633	94.80		
34.65	90.0	Flexure	kip-ft	462.73	39.60	73.09	3.231	116.30	4.188	150.76
34.65	90.0	Shear	kip	-79.93	-9.14	-18.70	2.093	75.36	2.714	97.69
34.65	90.0	Concrete Stresses	ksi	2.45	0.29	0.54	5.026	180.94		
37.02	96.2	Flexure	kip-ft	408.30	16.29	30.61	7.243	260.75	9.389	338.01
37.02	96.2	Shear	kip	-106.69	-10.52	-20.57	2.598	93.53	3.368	121.24
37.02	96.2	Concrete Stresses	ksi	2.45	0.12	0.23	12.955	466.37		
37.39	97.1	Shear	kip	-112.75	-10.73	-20.87	2.720	97.93	3.526	126.95
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	1.08	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 2

Location		Limit State		Units Capacity		DL + Adj-LL*		Inventory	Inventory	Operating	Operating
								Rating	Load Rating	Rating	Load Rating
(ft)	Percent						LL	Factor	(Ton)	Factor	(Ton)

0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	1.08	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	112.73	10.73	18.65	3.044	109.57	3.945	142.04
1.48	3.8	Flexure	kip-ft	408.30	16.29	27.43	8.082	290.94	10.476	377.14
1.48	3.8	Shear	kip	106.69	10.52	18.43	2.901	104.43	3.760	135.37
1.48	3.8	Concrete Stresses	ksi	2.45	0.12	0.20	14.455	520.38		
3.85	10.0	Flexure	kip-ft	462.73	39.60	66.60	3.545	127.63	4.596	165.45
3.85	10.0	Shear	kip	79.93	9.14	17.02	2.301	82.82	2.982	107.36
3.85	10.0	Concrete Stresses	ksi	2.45	0.29	0.49	5.516	198.56		
7.70	20.0	Flexure	kip-ft	462.73	70.46	117.65	1.820	65.51	2.359	84.92
7.70	20.0	Shear	kip	79.93	6.89	14.77	2.758	99.29	3.575	128.71
7.70	20.0	Concrete Stresses	ksi	2.45	0.52	0.86	2.795	100.61		
11.55	30.0	Flexure	kip-ft	462.73	92.31	153.13	1.296	46.66	1.680	60.48
11.55	30.0	Shear	kip	79.93	4.49	12.60	3.372	121.38	4.371	157.35
11.55	30.0	Concrete Stresses	ksi	2.45	0.68	1.13	1.969	70.87		
15.40	40.0	Flexure	kip-ft	462.73	105.27	173.06	1.093	39.36	1.417	51.02
15.40	40.0	Shear	kip	69.26	2.24	10.48	3.623	130.44	5.451	196.25
15.40	40.0	Concrete Stresses	ksi	2.45	0.77	1.27	1.648	59.34		
19.25	50.0	Flexure	kip-ft	462.73	109.59	177.43	1.049	37.77	1.360	48.96
19.25	50.0	Shear	kip	-66.70	0.00	-8.43	4.523	162.82	7.025	252.91
19.25	50.0	Concrete Stresses	ksi	2.45	0.81	1.30	1.577	56.78		
23.10	60.0	Flexure	kip-ft	462.73	105.27	173.06	1.093	39.36	1.417	51.02
23.10	60.0	Shear	kip	-69.26	-2.24	-10.48	3.623	130.44	5.451	196.25
23.10	60.0	Concrete Stresses	ksi	2.45	0.77	1.27	1.648	59.34		
26.95	70.0	Flexure	kip-ft	480.13	92.31	153.13	1.361	49.00	1.764	63.52
26.95	70.0	Shear	kip	-80.21	-4.49	-12.60	3.384	121.84	4.387	157.94
26.95	70.0	Concrete Stresses	ksi	2.45	0.68	1.13	1.969	70.87		
30.80	80.0	Flexure	kip-ft	462.73	70.46	117.65	1.820	65.51	2.359	84.92
30.80	80.0	Shear	kip	-79.93	-6.89	-14.77	2.758	99.29	3.575	128.71
30.80	80.0		ksi	2.45	0.52	0.86	2.795	100.61		

		Concrete Stresses								
34.65	90.0	Flexure	kip-ft	462.73	39.60	66.60	3.545	127.63	4.596	165.45
34.65	90.0	Shear	kip	-79.93	-9.14	-17.02	2.301	82.82	2.982	107.36
34.65	90.0	Concrete Stresses	ksi	2.45	0.29	0.49	5.516	198.56		
37.02	96.2	Flexure	kip-ft	408.30	16.29	27.43	8.082	290.94	10.476	377.14
37.02	96.2	Shear	kip	-106.69	-10.52	-18.43	2.901	104.43	3.760	135.37
37.02	96.2	Concrete Stresses	ksi	2.45	0.12	0.20	14.455	520.38		
37.39	97.1	Shear	kip	-112.75	-10.73	-18.65	3.044	109.58	3.946	142.05
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	1.08	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	2772.00
1.12	2.9	Shear	kip	112.73	10.73	11.46	6.669	186.74
1.48	3.8	Flexure	kip-ft	408.30	16.29	16.68	17.893	501.00
1.48	3.8	Shear	kip	106.69	10.52	11.27	6.382	178.70
3.85	10.0	Flexure	kip-ft	462.73	39.60	38.88	8.175	228.91
3.85	10.0	Shear	kip	79.93	9.14	10.10	5.218	146.10
7.70	20.0	Flexure	kip-ft	462.73	70.46	63.23	4.558	127.63
7.70	20.0	Shear	kip	79.93	6.89	8.21	6.680	187.05
11.55	30.0	Flexure	kip-ft	462.73	92.31	81.45	3.280	91.85
11.55	30.0	Shear	kip	79.93	4.49	7.05	8.107	226.99
15.40	40.0	Flexure	kip-ft	462.73	105.27	91.86	2.773	77.64
15.40	40.0	Shear	kip	79.93	2.24	5.89	10.068	281.90
19.25	50.0	Flexure	kip-ft	462.73	109.59	91.12	2.750	77.00
19.25	50.0	Shear	kip	79.93	0.00	4.73	12.989	363.70
23.10	60.0	Flexure	kip-ft	462.73	105.27	91.86	2.773	77.64
23.10	60.0	Shear	kip	-79.93	-2.24	-5.89	10.068	281.90

26.95	70.0	Flexure	kip-ft	480.13	92.31	81.45	3.445	96.45
26.95	70.0	Shear	kip	-80.21	-4.49	-7.05	8.137	227.84
30.80	80.0	Flexure	kip-ft	462.73	70.46	63.23	4.558	127.63
30.80	80.0	Shear	kip	-79.93	-6.89	-8.21	6.680	187.05
34.65	90.0	Flexure	kip-ft	462.73	39.60	38.88	8.175	228.91
34.65	90.0	Shear	kip	-79.93	-9.14	-10.10	5.218	146.10
37.02	96.2	Flexure	kip-ft	408.30	16.29	16.68	17.893	501.00
37.02	96.2	Shear	kip	-106.69	-10.52	-11.27	6.382	178.70
37.39	97.1	Shear	kip	-112.75	-10.73	-11.46	6.670	186.75
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3628.35
1.12	2.9	Shear	kip	112.73	10.73	16.06	4.756	174.32
1.48	3.8	Flexure	kip-ft	408.30	16.29	23.41	12.747	467.17
1.48	3.8	Shear	kip	106.69	10.52	15.83	4.547	166.63
3.85	10.0	Flexure	kip-ft	462.73	39.60	55.34	5.744	210.50
3.85	10.0	Shear	kip	79.93	9.14	14.37	3.666	134.35
7.70	20.0	Flexure	kip-ft	462.73	70.46	93.36	3.087	113.13
7.70	20.0	Shear	kip	79.93	6.89	12.12	4.524	165.81
11.55	30.0	Flexure	kip-ft	462.73	92.31	114.05	2.343	85.86
11.55	30.0	Shear	kip	79.93	4.49	9.87	5.790	212.19
15.40	40.0	Flexure	kip-ft	462.73	105.27	126.11	2.020	74.03
15.40	40.0	Shear	kip	79.93	2.24	8.19	7.244	265.51
19.25	50.0	Flexure	kip-ft	462.73	109.59	128.76	1.946	71.32
19.25	50.0	Shear	kip	79.93	0.00	6.69	9.192	336.87
23.10	60.0	Flexure	kip-ft	462.73	105.27	126.11	2.020	74.03
23.10	60.0	Shear	kip	-79.93	-2.24	-8.19	7.244	265.51
26.95	70.0	Flexure	kip-ft	480.13	92.31	114.05	2.460	90.16
26.95	70.0	Shear	kip	-80.21	-4.49	-9.87	5.811	212.98
30.80	80.0	Flexure	kip-ft	462.73	70.46	93.36	3.087	113.13
30.80	80.0	Shear	kip	-79.93	-6.89	-12.12	4.524	165.81

34.65	90.0	Flexure	kip-ft	462.73	39.60	55.34	5.744	210.50
34.65	90.0	Shear	kip	-79.93	-9.14	-14.37	3.666	134.35
37.02	96.2	Flexure	kip-ft	408.30	16.29	23.41	12.747	467.17
37.02	96.2	Shear	kip	-106.69	-10.52	-15.83	4.547	166.63
37.39	97.1	Shear	kip	-112.75	-10.73	-16.06	4.757	174.33
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	112.73	10.73	16.08	4.750	190.02
1.48	3.8	Flexure	kip-ft	408.30	16.29	23.46	12.722	508.90
1.48	3.8	Shear	kip	106.69	10.52	15.86	4.538	181.51
3.85	10.0	Flexure	kip-ft	462.73	39.60	55.39	5.739	229.54
3.85	10.0	Shear	kip	79.93	9.14	14.39	3.663	146.51
7.70	20.0	Flexure	kip-ft	462.73	70.46	92.41	3.119	124.75
7.70	20.0	Shear	kip	79.93	6.89	12.00	4.571	182.83
11.55	30.0	Flexure	kip-ft	462.73	92.31	114.81	2.327	93.08
11.55	30.0	Shear	kip	79.93	4.49	9.94	5.751	230.04
15.40	40.0	Flexure	kip-ft	462.73	105.27	128.28	1.986	79.42
15.40	40.0	Shear	kip	79.93	2.24	8.24	7.203	288.14
19.25	50.0	Flexure	kip-ft	462.73	109.59	132.83	1.886	75.46
19.25	50.0	Shear	kip	79.93	0.00	6.32	9.727	389.09
23.10	60.0	Flexure	kip-ft	462.73	105.27	128.28	1.986	79.42
23.10	60.0	Shear	kip	-79.93	-2.24	-8.24	7.203	288.14
26.95	70.0	Flexure	kip-ft	480.13	92.31	114.81	2.444	97.75
26.95	70.0	Shear	kip	-80.21	-4.49	-9.94	5.773	230.90
30.80	80.0	Flexure	kip-ft	462.73	70.46	92.41	3.119	124.75
30.80	80.0	Shear	kip	-79.93	-6.89	-12.00	4.571	182.83
34.65	90.0	Flexure	kip-ft	462.73	39.60	55.39	5.739	229.54
34.65	90.0	Shear	kip	-79.93	-9.14	-14.39	3.663	146.51
37.02	96.2	Flexure	kip-ft	408.30	16.29	23.46	12.722	508.90
37.02	96.2	Shear	kip	-106.69	-10.52	-15.86	4.538	181.51

37.39	97.1	Shear	kip	-112.75	-10.73	-16.08	4.751	190.03
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Permit	Permit
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	5940.00
1.48	3.8	Flexure	kip-ft	408.30	16.29	35.85	9.016	540.99
3.85	10.0	Flexure	kip-ft	462.73	39.60	85.33	4.036	242.14
7.70	20.0	Flexure	kip-ft	462.73	70.46	144.69	2.158	129.47
11.55	30.0	Flexure	kip-ft	462.73	92.31	179.27	1.615	96.87
15.40	40.0	Flexure	kip-ft	462.73	105.27	196.07	1.407	84.45
19.25	50.0	Flexure	kip-ft	462.73	109.59	193.35	1.404	84.24
23.10	60.0	Flexure	kip-ft	462.73	105.27	196.07	1.407	84.45
26.95	70.0	Flexure	kip-ft	480.13	92.31	179.27	1.695	101.73
30.80	80.0	Flexure	kip-ft	462.73	70.46	144.69	2.158	129.47
34.65	90.0	Flexure	kip-ft	462.73	39.60	85.33	4.036	242.14
37.02	96.2	Flexure	kip-ft	408.30	16.29	35.85	9.016	540.99
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3960.00

1.12	2.9	Shear	kip	112.73	10.73	14.69	5.201	208.03
1.48	3.8	Flexure	kip-ft	408.30	16.29	21.47	13.898	555.92
1.48	3.8	Shear	kip	106.69	10.52	14.52	4.957	198.29
3.85	10.0	Flexure	kip-ft	462.73	39.60	51.52	6.170	246.79
3.85	10.0	Shear	kip	79.93	9.14	13.38	3.938	157.51
7.70	20.0	Flexure	kip-ft	462.73	70.46	88.86	3.243	129.72
7.70	20.0	Shear	kip	79.93	6.89	11.54	4.753	190.12
11.55	30.0	Flexure	kip-ft	462.73	92.31	112.03	2.385	95.39
11.55	30.0	Shear	kip	79.93	4.49	9.70	5.894	235.75
15.40	40.0	Flexure	kip-ft	462.73	105.27	125.93	2.023	80.91
15.40	40.0	Shear	kip	79.93	2.24	7.86	7.549	301.96
19.25	50.0	Flexure	kip-ft	462.73	109.59	128.11	1.956	78.24
19.25	50.0	Shear	kip	79.93	0.00	6.02	10.217	408.69
23.10	60.0	Flexure	kip-ft	462.73	105.27	125.93	2.023	80.91
23.10	60.0	Shear	kip	-79.93	-2.24	-7.86	7.549	301.96
26.95	70.0	Flexure	kip-ft	480.13	92.31	112.03	2.504	100.17
26.95	70.0	Shear	kip	-80.21	-4.49	-9.70	5.916	236.64
30.80	80.0	Flexure	kip-ft	462.73	70.46	88.86	3.243	129.72
30.80	80.0	Shear	kip	-79.93	-6.89	-11.54	4.753	190.12
34.65	90.0	Flexure	kip-ft	462.73	39.60	51.52	6.170	246.79
34.65	90.0	Shear	kip	-79.93	-9.14	-13.38	3.938	157.51
37.02	96.2	Flexure	kip-ft	408.30	16.29	21.47	13.898	555.92
37.02	96.2	Shear	kip	-106.69	-10.52	-14.52	4.957	198.28
37.39	97.1	Shear	kip	-112.75	-10.73	-14.69	5.201	208.05
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	1683.00
1.12	2.9	Shear	kip	112.73	10.73	9.87	7.737	131.52
1.48	3.8	Flexure	kip-ft	408.30	16.29	14.44	20.659	351.20
1.48	3.8	Shear	kip	106.69	10.52	9.77	7.369	125.27
3.85	10.0	Flexure	kip-ft	462.73	39.60	34.85	9.121	155.07

3.85	10.0	Shear	kip	79.93	9.14	9.05	5.822	98.97
7.70	20.0	Flexure	kip-ft	462.73	70.46	60.77	4.742	80.62
7.70	20.0	Shear	kip	79.93	6.89	7.89	6.950	118.15
11.55	30.0	Flexure	kip-ft	462.73	92.31	77.77	3.436	58.41
11.55	30.0	Shear	kip	79.93	4.49	6.73	8.491	144.34
15.40	40.0	Flexure	kip-ft	462.73	105.27	85.84	2.968	50.45
15.40	40.0	Shear	kip	79.93	2.24	5.57	10.644	180.94
19.25	50.0	Flexure	kip-ft	462.73	109.59	84.98	2.949	50.13
19.25	50.0	Shear	kip	79.93	0.00	4.41	13.927	236.76
23.10	60.0	Flexure	kip-ft	462.73	105.27	85.84	2.968	50.45
23.10	60.0	Shear	kip	-79.93	-2.24	-5.57	10.644	180.94
26.95	70.0	Flexure	kip-ft	480.13	92.31	77.77	3.608	61.33
26.95	70.0	Shear	kip	-80.21	-4.49	-6.73	8.523	144.88
30.80	80.0	Flexure	kip-ft	462.73	70.46	60.77	4.742	80.62
30.80	80.0	Shear	kip	-79.93	-6.89	-7.89	6.950	118.15
34.65	90.0	Flexure	kip-ft	462.73	39.60	34.85	9.122	155.07
34.65	90.0	Shear	kip	-79.93	-9.14	-9.05	5.822	98.97
37.02	96.2	Flexure	kip-ft	408.30	16.29	14.44	20.659	351.20
37.02	96.2	Shear	kip	-106.69	-10.52	-9.77	7.369	125.27
37.39	97.1	Shear	kip	-112.75	-10.73	-9.88	7.737	131.54
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3267.00
1.12	2.9	Shear	kip	112.73	10.73	18.08	4.225	139.42
1.48	3.8	Flexure	kip-ft	408.30	16.29	26.43	11.289	372.52
1.48	3.8	Shear	kip	106.69	10.52	17.87	4.026	132.87
3.85	10.0	Flexure	kip-ft	462.73	39.60	63.47	5.008	165.27
3.85	10.0	Shear	kip	79.93	9.14	16.49	3.197	105.48
7.70	20.0	Flexure	kip-ft	462.73	70.46	109.61	2.629	86.76
7.70	20.0	Shear	kip	79.93	6.89	14.24	3.853	127.16
11.55	30.0	Flexure	kip-ft	462.73	92.31	138.43	1.930	63.69

11.55	30.0	Shear	kip	79.93	4.49	11.98	4.770	157.41
15.40	40.0	Flexure	kip-ft	462.73	105.27	156.17	1.631	53.83
15.40	40.0	Shear	kip	79.93	2.24	9.73	6.094	201.11
19.25	50.0	Flexure	kip-ft	462.73	109.59	159.70	1.569	51.78
19.25	50.0	Shear	kip	79.93	0.00	7.48	8.215	271.09
23.10	60.0	Flexure	kip-ft	462.73	105.27	156.17	1.631	53.83
23.10	60.0	Shear	kip	-79.93	-2.24	-9.73	6.094	201.11
26.95	70.0	Flexure	kip-ft	480.13	92.31	138.43	2.027	66.89
26.95	70.0	Shear	kip	-80.21	-4.49	-11.98	4.788	158.00
30.80	80.0	Flexure	kip-ft	462.73	70.46	109.61	2.629	86.76
30.80	80.0	Shear	kip	-79.93	-6.89	-14.24	3.853	127.16
34.65	90.0	Flexure	kip-ft	462.73	39.60	63.47	5.008	165.27
34.65	90.0	Shear	kip	-79.93	-9.14	-16.49	3.196	105.48
37.02	96.2	Flexure	kip-ft	408.30	16.29	26.43	11.289	372.52
37.02	96.2	Shear	kip	-106.69	-10.52	-17.87	4.026	132.87
37.39	97.1	Shear	kip	-112.75	-10.73	-18.08	4.225	139.43
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - w/ post Tensioning
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	182.46	0.00	0.00	99.000	3465.00
1.12	2.9	Shear	kip	112.73	10.73	18.95	4.032	141.10
1.48	3.8	Flexure	kip-ft	408.30	16.29	27.70	10.774	377.09
1.48	3.8	Shear	kip	106.69	10.52	18.72	3.843	134.50
3.85	10.0	Flexure	kip-ft	462.73	39.60	66.43	4.785	167.47
3.85	10.0	Shear	kip	79.93	9.14	17.26	3.054	106.89
7.70	20.0	Flexure	kip-ft	462.73	70.46	114.49	2.517	88.10
7.70	20.0	Shear	kip	79.93	6.89	14.87	3.689	129.12
11.55	30.0	Flexure	kip-ft	462.73	92.31	147.43	1.812	63.43
11.55	30.0	Shear	kip	79.93	4.49	12.48	4.580	160.30
15.40	40.0	Flexure	kip-ft	462.73	105.27	168.68	1.510	52.85
15.40	40.0	Shear	kip	79.93	2.24	10.10	5.877	205.68
19.25	50.0	Flexure	kip-ft	462.73	109.59	171.55	1.461	51.12

19.25	50.0	Shear	kip	79.93	0.00	7.71	7.976	279.15
23.10	60.0	Flexure	kip-ft	462.73	105.27	168.68	1.510	52.85
23.10	60.0	Shear	kip	-79.93	-2.24	-10.10	5.877	205.68
26.95	70.0	Flexure	kip-ft	480.13	92.31	147.43	1.903	66.61
26.95	70.0	Shear	kip	-80.21	-4.49	-12.48	4.597	160.90
30.80	80.0	Flexure	kip-ft	462.73	70.46	114.49	2.517	88.10
30.80	80.0	Shear	kip	-79.93	-6.89	-14.87	3.689	129.12
34.65	90.0	Flexure	kip-ft	462.73	39.60	66.43	4.785	167.47
34.65	90.0	Shear	kip	-79.93	-9.14	-17.26	3.054	106.89
37.02	96.2	Flexure	kip-ft	408.30	16.29	27.70	10.774	377.09
37.02	96.2	Shear	kip	-106.69	-10.52	-18.72	3.843	134.50
37.39	97.1	Shear	kip	-112.75	-10.73	-18.95	4.032	141.12
38.50	100.0	Flexure	kip-ft	157.45	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294D
Bridge ID: 874294D

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 20:30:58
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 20:33:15

Structure Definition Name: End Span 1 (or 3) - PS Conc PSU
Member Name: G8
Member Alternative Name: 17"x36" INT PSU - Existing Deteriorated

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 1

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location					DL +					
(ft)	Percent	Limit State	Units	Capacity	Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	129.02	7.72	41.31	1.651	59.44	2.140	77.05
1.69	6.0	Flexure	kip-ft	229.80	13.52	68.34	1.780	64.09	2.308	83.08
1.69	6.0	Shear	kip	118.17	7.42	40.19	1.548	55.74	2.007	72.25
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.50	3.813	137.28		
2.83	10.0	Flexure	kip-ft	268.56	21.61	108.12	1.277	45.96	1.655	59.57
2.83	10.0	Shear	kip	61.52	6.76	37.73	0.804	28.94	1.655	59.58
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.79	2.317	83.40		
5.66	20.0	Flexure	kip-ft	287.73	38.40	184.27	0.743	26.76	0.964	34.69
5.66	20.0	Shear	kip	29.08	5.11	31.70	0.409	14.73	0.815	29.35
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	1.35	1.245	44.84		
8.49	30.0	Flexure	kip-ft	287.73	50.23	228.45	0.563	20.25	0.729	26.26
8.49	30.0	Shear	kip	23.84	3.30	25.78	0.437	15.74	0.795	28.63
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	1.68	0.940	33.83		
11.32	40.0	Flexure	kip-ft	287.73	57.22	240.66	0.513	18.48	0.665	23.96
11.32	40.0	Shear	kip	23.84	1.65	19.96	0.623	22.45	1.044	37.59
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	1.77	0.856	30.81		
14.15	50.0	Flexure	kip-ft	287.73	59.54	221.36	0.551	19.82	0.714	25.69
14.15	50.0	Shear	kip	-24.63	-0.00	-14.26	0.987	35.52	1.781	64.13

14.15	50.0	Concrete Stresses	ksi	1.63	0.44	1.63	0.917	33.02		
16.98	60.0	Flexure	kip-ft	287.73	57.20	240.66	0.513	18.48	0.666	23.96
16.98	60.0	Shear	kip	-23.84	-1.65	-19.96	0.623	22.44	1.044	37.58
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	1.77	0.856	30.81		
19.80	70.0	Flexure	kip-ft	287.73	50.19	228.45	0.563	20.26	0.730	26.26
19.80	70.0	Shear	kip	-23.84	-3.30	-25.78	0.437	15.73	0.795	28.63
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	1.68	0.940	33.84		
22.63	80.0	Flexure	kip-ft	287.73	38.37	184.27	0.743	26.77	0.964	34.70
22.63	80.0	Shear	kip	-29.09	-5.12	-31.70	0.409	14.73	0.815	29.34
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	1.35	1.246	44.84		
25.46	90.0	Flexure	kip-ft	275.54	21.57	108.12	1.314	47.29	1.703	61.31
25.46	90.0	Shear	kip	-58.55	-6.76	-37.73	0.759	27.31	1.599	57.55
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.79	2.317	83.42		
26.81	94.8	Flexure	kip-ft	242.12	11.90	60.52	2.146	77.24	2.781	100.13
26.81	94.8	Shear	kip	-118.33	-7.55	-40.64	1.531	55.11	1.985	71.44
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.44	4.340	156.22		
27.11	95.8	Shear	kip	-125.83	-7.72	-41.29	1.608	57.88	2.084	75.03
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 1

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0		ksi	0.70	-0.00	0.00	99.000	3564.00		

		Concrete Stresses								
1.17	4.1	Shear	kip	129.02	7.72	40.42	1.688	60.75	2.188	78.75
1.69	6.0	Flexure	kip-ft	229.80	13.52	67.18	1.811	65.20	2.348	84.52
1.69	6.0	Shear	kip	118.17	7.42	39.50	1.575	56.71	2.042	73.51
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.49	3.879	139.66		
2.83	10.0	Flexure	kip-ft	268.56	21.61	107.45	1.285	46.25	1.665	59.95
2.83	10.0	Shear	kip	62.22	6.76	37.49	0.820	29.51	1.666	59.96
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.79	2.331	83.92		
5.66	20.0	Flexure	kip-ft	287.73	38.40	189.24	0.724	26.06	0.938	33.78
5.66	20.0	Shear	kip	28.06	5.11	32.58	0.380	13.69	0.759	27.32
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	1.39	1.213	43.66		
8.49	30.0	Flexure	kip-ft	287.73	50.23	245.39	0.524	18.86	0.679	24.44
8.49	30.0	Shear	kip	23.84	3.30	27.77	0.406	14.61	0.663	23.87
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	1.80	0.875	31.50		
11.32	40.0	Flexure	kip- ft	287.73	57.22	275.88	0.448	16.12	0.580	20.90
11.32	40.0	Shear	kip	23.84	1.65	23.07	0.539	19.42	0.747	26.88
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	2.03	0.747	26.88		
14.15	50.0	Flexure	kip- ft	287.73	59.54	280.73	0.434	15.63	0.563	20.26
14.15	50.0	Shear	kip	-23.84	-0.00	-18.49	0.737	26.52	1.013	36.48
14.15	50.0	Concrete Stresses	ksi	1.63	0.44	2.06	0.723	26.04		
16.98	60.0	Flexure	kip- ft	287.73	57.20	275.88	0.448	16.12	0.581	20.90
16.98	60.0	Shear	kip	-23.84	-1.65	-23.07	0.539	19.41	0.746	26.87
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	2.03	0.747	26.88		
19.80	70.0	Flexure	kip-ft	287.73	50.19	245.39	0.524	18.86	0.679	24.45
19.80	70.0	Shear	kip	-23.84	-3.30	-27.77	0.406	14.60	0.663	23.87
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	1.80	0.875	31.51		
22.63	80.0	Flexure	kip-ft	287.73	38.37	189.24	0.724	26.06	0.938	33.79
22.63	80.0	Shear	kip	-28.06	-5.12	-32.58	0.380	13.68	0.759	27.32
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	1.39	1.213	43.66		
25.46	90.0	Flexure	kip-ft	275.54	21.57	107.45	1.322	47.59	1.714	61.69
25.46	90.0	Shear	kip	-59.25	-6.76	-37.49	0.774	27.87	1.609	57.92
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.79	2.332	83.94		

26.81	94.8	Flexure	kip-ft	242.12	11.90	59.38	2.187	78.73	2.835	102.06
26.81	94.8	Shear	kip	-118.33	-7.55	-39.87	1.561	56.18	2.023	72.83
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.44	4.423	159.23		
27.11	95.8	Shear	kip	-125.83	-7.72	-40.40	1.643	59.16	2.130	76.68
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	2772.00
1.17	4.1	Shear	kip	129.02	7.72	22.62	4.059	113.64
1.69	6.0	Flexure	kip-ft	229.80	13.52	37.34	4.386	122.80
1.69	6.0	Shear	kip	118.17	7.42	22.13	3.785	105.99
2.83	10.0	Flexure	kip-ft	268.56	21.61	59.51	3.122	87.42
2.83	10.0	Shear	kip	92.75	6.76	21.03	3.083	86.32
5.66	20.0	Flexure	kip-ft	287.73	38.40	103.67	1.779	49.81
5.66	20.0	Shear	kip	85.08	5.11	18.32	3.304	92.52
8.49	30.0	Flexure	kip-ft	287.73	50.23	132.47	1.306	36.57
8.49	30.0	Shear	kip	76.05	3.30	15.61	3.545	99.26
11.32	40.0	Flexure	kip-ft	287.73	57.22	145.92	1.140	31.91
11.32	40.0	Shear	kip	62.92	1.65	12.89	3.631	101.66
14.15	50.0	Flexure	kip-ft	287.73	59.54	144.02	1.139	31.90
14.15	50.0	Shear	kip	-66.11	-0.00	-10.18	4.994	139.84
16.98	60.0	Flexure	kip-ft	287.73	57.20	145.92	1.140	31.92
16.98	60.0	Shear	kip	-62.92	-1.65	-12.89	3.631	101.66
19.80	70.0	Flexure	kip-ft	287.73	50.19	132.47	1.306	36.58
19.80	70.0	Shear	kip	-76.08	-3.30	-15.61	3.546	99.29
22.63	80.0	Flexure	kip-ft	287.73	38.37	103.67	1.779	49.82
22.63	80.0	Shear	kip	-85.08	-5.12	-18.32	3.304	92.51
25.46	90.0	Flexure	kip-ft	275.54	21.57	59.51	3.213	89.97

25.46	90.0	Shear	kip	-89.88	-6.76	-21.03	2.978	83.37
26.81	94.8	Flexure	kip-ft	242.12	11.90	33.03	5.292	148.19
26.81	94.8	Shear	kip	-118.33	-7.55	-22.33	3.751	105.04
27.11	95.8	Shear	kip	-125.83	-7.72	-22.61	3.952	110.66
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3628.35
1.17	4.1	Shear	kip	129.02	7.72	31.76	2.891	105.94
1.69	6.0	Flexure	kip-ft	229.80	13.52	51.99	3.150	115.46
1.69	6.0	Shear	kip	118.17	7.42	30.81	2.719	99.65
2.83	10.0	Flexure	kip-ft	268.56	21.61	82.09	2.263	82.96
2.83	10.0	Shear	kip	92.75	6.76	29.02	2.235	81.91
5.66	20.0	Flexure	kip-ft	287.73	38.40	144.31	1.278	46.83
5.66	20.0	Shear	kip	64.26	5.11	25.50	1.746	63.98
8.49	30.0	Flexure	kip-ft	287.73	50.23	186.66	0.927	33.97
8.49	30.0	Shear	kip	43.25	3.30	21.99	1.369	50.17
11.32	40.0	Flexure	kip-ft	287.73	57.22	209.15	0.795	29.14
11.32	40.0	Shear	kip	37.57	1.65	18.48	1.478	54.17
14.15	50.0	Flexure	kip-ft	287.73	59.54	211.77	0.775	28.40
14.15	50.0	Shear	kip	-37.74	-0.00	-14.97	1.939	71.07
16.98	60.0	Flexure	kip-ft	287.73	57.20	209.15	0.795	29.15
16.98	60.0	Shear	kip	-37.57	-1.65	-18.48	1.478	54.16
19.80	70.0	Flexure	kip-ft	287.73	50.19	186.66	0.927	33.98
19.80	70.0	Shear	kip	-43.26	-3.30	-21.99	1.369	50.17
22.63	80.0	Flexure	kip-ft	287.73	38.37	144.31	1.278	46.84
22.63	80.0	Shear	kip	-64.27	-5.12	-25.50	1.746	63.98
25.46	90.0	Flexure	kip-ft	275.54	21.57	82.09	2.329	85.37
25.46	90.0	Shear	kip	-89.88	-6.76	-29.02	2.159	79.11
26.81	94.8	Flexure	kip-ft	242.12	11.90	46.14	3.788	138.84
26.81	94.8	Shear	kip	-118.33	-7.55	-31.19	2.685	98.41
27.11	95.8	Shear	kip	-125.83	-7.72	-31.75	2.815	103.17

28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3628.35
-------	-------	---------	--------	-------	------	------	--------	---------

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.02	7.72	31.90	2.878	115.13
1.69	6.0	Flexure	kip-ft	229.80	13.52	52.61	3.113	124.53
1.69	6.0	Shear	kip	118.17	7.42	31.17	2.687	107.48
2.83	10.0	Flexure	kip-ft	268.56	21.61	83.64	2.221	88.86
2.83	10.0	Shear	kip	92.75	6.76	29.56	2.193	87.74
5.66	20.0	Flexure	kip-ft	287.73	38.40	144.70	1.274	50.98
5.66	20.0	Shear	kip	63.93	5.11	25.57	1.731	69.24
8.49	30.0	Flexure	kip-ft	287.73	50.23	183.19	0.945	37.78
8.49	30.0	Shear	kip	44.39	3.30	21.58	1.435	57.41
11.32	40.0	Flexure	kip-ft	287.73	57.22	199.10	0.835	33.41
11.32	40.0	Shear	kip	40.03	1.65	17.59	1.660	66.42
14.15	50.0	Flexure	kip-ft	287.73	59.54	209.06	0.785	31.39
14.15	50.0	Shear	kip	-38.66	-0.00	-13.61	2.185	87.39
16.98	60.0	Flexure	kip-ft	287.73	57.20	199.10	0.835	33.42
16.98	60.0	Shear	kip	-40.04	-1.65	-17.59	1.660	66.40
19.80	70.0	Flexure	kip-ft	287.73	50.19	183.19	0.945	37.79
19.80	70.0	Shear	kip	-44.40	-3.30	-21.58	1.435	57.41
22.63	80.0	Flexure	kip-ft	287.73	38.37	144.70	1.275	50.98
22.63	80.0	Shear	kip	-63.94	-5.12	-25.57	1.731	69.24
25.46	90.0	Flexure	kip-ft	275.54	21.57	83.64	2.286	91.45
25.46	90.0	Shear	kip	-89.88	-6.76	-29.56	2.119	84.74
26.81	94.8	Flexure	kip-ft	242.12	11.90	46.55	3.755	150.22
26.81	94.8	Shear	kip	-118.33	-7.55	-31.47	2.662	106.47
27.11	95.8	Shear	kip	-125.83	-7.72	-31.89	2.803	112.11
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3960.00

Detailed Rating Results

**17"x36" INT PSU - Existing Deteriorated
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane**

Span 1

							Permit Rating	Permit Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	5940.00
1.69	6.0	Flexure	kip-ft	229.80	13.52	82.89	2.140	128.42
2.83	10.0	Flexure	kip-ft	268.56	21.61	130.88	1.538	92.28
5.66	20.0	Flexure	kip-ft	287.73	38.40	221.65	0.901	54.08
8.49	30.0	Flexure	kip-ft	287.73	50.23	272.30	0.688	41.30
11.32	40.0	Flexure	kip-ft	287.73	57.22	282.85	0.637	38.22
14.15	50.0	Flexure	kip-ft	287.73	59.54	253.93	0.700	42.00
16.98	60.0	Flexure	kip-ft	287.73	57.20	282.85	0.637	38.22
19.80	70.0	Flexure	kip-ft	287.73	50.19	272.30	0.689	41.31
22.63	80.0	Flexure	kip-ft	287.73	38.37	221.65	0.901	54.09
25.46	90.0	Flexure	kip-ft	275.54	21.57	130.88	1.583	94.96
26.81	94.8	Flexure	kip-ft	242.12	11.90	73.43	2.579	154.73
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	5940.00

**Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane**

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.02	7.72	31.15	2.947	117.90
1.69	6.0	Flexure	kip-ft	229.80	13.52	51.25	3.196	127.83
1.69	6.0	Shear	kip	118.17	7.42	30.37	2.758	110.34
2.83	10.0	Flexure	kip-ft	268.56	21.61	81.00	2.294	91.76

2.83	10.0	Shear	kip	92.75	6.76	28.63	2.265	90.60
5.66	20.0	Flexure	kip-ft	287.73	38.40	137.61	1.340	53.60
5.66	20.0	Shear	kip	70.68	5.11	24.32	2.034	81.35
8.49	30.0	Flexure	kip-ft	287.73	50.23	169.84	1.019	40.75
8.49	30.0	Shear	kip	49.43	3.30	20.01	1.742	69.68
11.32	40.0	Flexure	kip-ft	287.73	57.22	189.17	0.879	35.16
11.32	40.0	Shear	kip	43.13	1.65	15.70	2.012	80.49
14.15	50.0	Flexure	kip-ft	287.73	59.54	189.87	0.864	34.56
14.15	50.0	Shear	kip	-43.86	-0.00	-12.33	2.735	109.41
16.98	60.0	Flexure	kip-ft	287.73	57.20	189.17	0.879	35.17
16.98	60.0	Shear	kip	-43.13	-1.65	-15.70	2.012	80.48
19.80	70.0	Flexure	kip-ft	287.73	50.19	169.84	1.019	40.76
19.80	70.0	Shear	kip	-49.44	-3.30	-20.01	1.742	69.68
22.63	80.0	Flexure	kip-ft	287.73	38.37	137.61	1.340	53.61
22.63	80.0	Shear	kip	-70.70	-5.12	-24.32	2.034	81.36
25.46	90.0	Flexure	kip-ft	275.54	21.57	81.00	2.361	94.43
25.46	90.0	Shear	kip	-89.88	-6.76	-28.63	2.188	87.51
26.81	94.8	Flexure	kip-ft	242.12	11.90	45.39	3.851	154.05
26.81	94.8	Shear	kip	-118.33	-7.55	-30.68	2.730	109.19
27.11	95.8	Shear	kip	-125.83	-7.72	-31.14	2.870	114.81
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load
(ft)	Percent	Limit	Units	Capacity	DL + Adj	LL	Factor	Rating
		State			-LL*			(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	1683.00
1.17	4.1	Shear	kip	129.02	7.72	21.61	4.249	72.24
1.69	6.0	Flexure	kip-ft	229.80	13.52	35.63	4.596	78.14
1.69	6.0	Shear	kip	118.17	7.42	21.11	3.967	67.45
2.83	10.0	Flexure	kip-ft	268.56	21.61	56.64	3.281	55.77
2.83	10.0	Shear	kip	92.75	6.76	20.02	3.239	55.07
5.66	20.0	Flexure	kip-ft	287.73	38.40	97.92	1.883	32.01
5.66	20.0	Shear	kip	85.08	5.11	17.31	3.498	59.47
8.49	30.0	Flexure	kip-ft	287.73	50.23	123.85	1.397	23.75

8.49	30.0	Shear	kip	85.08	3.30	14.59	4.268	72.55
11.32	40.0	Flexure	kip-ft	287.73	57.22	134.43	1.237	21.03
11.32	40.0	Shear	kip	73.19	1.65	11.88	4.606	78.31
14.15	50.0	Flexure	kip-ft	287.73	59.54	129.66	1.265	21.51
14.15	50.0	Shear	kip	-81.47	-0.00	-9.17	6.837	116.23
16.98	60.0	Flexure	kip-ft	287.73	57.20	134.43	1.237	21.03
16.98	60.0	Shear	kip	-73.20	-1.65	-11.88	4.606	78.31
19.80	70.0	Flexure	kip-ft	287.73	50.19	123.85	1.397	23.76
19.80	70.0	Shear	kip	-85.08	-3.30	-14.59	4.267	72.55
22.63	80.0	Flexure	kip-ft	287.73	38.37	97.92	1.884	32.02
22.63	80.0	Shear	kip	-85.08	-5.12	-17.31	3.498	59.46
25.46	90.0	Flexure	kip-ft	275.54	21.57	56.64	3.376	57.40
25.46	90.0	Shear	kip	-89.88	-6.76	-20.02	3.129	53.19
26.81	94.8	Flexure	kip-ft	242.12	11.90	31.53	5.545	94.26
26.81	94.8	Shear	kip	-118.33	-7.55	-21.31	3.930	66.81
27.11	95.8	Shear	kip	-125.83	-7.72	-21.60	4.138	70.34
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3267.00
1.17	4.1	Shear	kip	129.02	7.72	38.49	2.386	78.73
1.69	6.0	Flexure	kip-ft	229.80	13.52	63.33	2.586	85.34
1.69	6.0	Shear	kip	118.17	7.42	37.53	2.232	73.66
2.83	10.0	Flexure	kip-ft	268.56	21.61	100.16	1.855	61.22
2.83	10.0	Shear	kip	92.75	6.76	35.40	1.832	60.44
5.66	20.0	Flexure	kip-ft	287.73	38.40	170.52	1.081	35.69
5.66	20.0	Shear	kip	48.49	5.11	30.14	1.075	35.47
8.49	30.0	Flexure	kip-ft	287.73	50.23	211.09	0.820	27.05
8.49	30.0	Shear	kip	36.73	3.30	24.87	1.009	33.28
11.32	40.0	Flexure	kip-ft	287.73	57.22	236.48	0.703	23.21
11.32	40.0	Shear	kip	32.38	1.65	19.60	1.190	39.27
14.15	50.0	Flexure	kip-ft	287.73	59.54	239.38	0.685	22.62

14.15	50.0	Shear	kip	-32.67	-0.00	-14.97	1.678	55.39
16.98	60.0	Flexure	kip-ft	287.73	57.20	236.48	0.703	23.21
16.98	60.0	Shear	kip	-32.38	-1.65	-19.60	1.190	39.26
19.80	70.0	Flexure	kip-ft	287.73	50.19	211.09	0.820	27.06
19.80	70.0	Shear	kip	-36.74	-3.30	-24.87	1.009	33.28
22.63	80.0	Flexure	kip-ft	287.73	38.37	170.52	1.082	35.69
22.63	80.0	Shear	kip	-48.50	-5.12	-30.14	1.075	35.47
25.46	90.0	Flexure	kip-ft	275.54	21.57	100.16	1.909	63.00
25.46	90.0	Shear	kip	-89.88	-6.76	-35.40	1.769	58.38
26.81	94.8	Flexure	kip-ft	242.12	11.90	56.09	3.117	102.85
26.81	94.8	Shear	kip	-118.33	-7.55	-37.92	2.209	72.90
27.11	95.8	Shear	kip	-125.83	-7.72	-38.47	2.323	76.66
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	83.08	0.00	0.00	99.000	3465.00
1.17	4.1	Shear	kip	129.02	7.72	40.09	2.290	80.16
1.69	6.0	Flexure	kip-ft	229.80	13.52	65.94	2.484	86.93
1.69	6.0	Shear	kip	118.17	7.42	39.07	2.144	75.03
2.83	10.0	Flexure	kip-ft	268.56	21.61	104.17	1.784	62.43
2.83	10.0	Shear	kip	92.75	6.76	36.82	1.761	61.64
5.66	20.0	Flexure	kip-ft	287.73	38.40	176.73	1.043	36.52
5.66	20.0	Shear	kip	45.97	5.11	31.23	0.975	34.12
8.49	30.0	Flexure	kip-ft	287.73	50.23	225.32	0.768	26.88
8.49	30.0	Shear	kip	33.93	3.30	25.65	0.894	31.29
11.32	40.0	Flexure	kip-ft	287.73	57.22	257.95	0.645	22.57
11.32	40.0	Shear	kip	29.18	1.65	20.27	1.029	36.03
14.15	50.0	Flexure	kip-ft	287.73	59.54	258.96	0.634	22.18
14.15	50.0	Shear	kip	-29.65	-0.00	-15.79	1.444	50.54
16.98	60.0	Flexure	kip-ft	287.73	57.20	257.95	0.645	22.57
16.98	60.0	Shear	kip	-29.18	-1.65	-20.27	1.029	36.02
19.80	70.0	Flexure	kip-ft	287.73	50.19	225.32	0.768	26.88

19.80	70.0	Shear	kip	-33.93	-3.30	-25.65	0.894	31.29
22.63	80.0	Flexure	kip-ft	287.73	38.37	176.73	1.044	36.53
22.63	80.0	Shear	kip	-45.98	-5.12	-31.23	0.975	34.12
25.46	90.0	Flexure	kip-ft	275.54	21.57	104.17	1.836	64.25
25.46	90.0	Shear	kip	-89.88	-6.76	-36.82	1.701	59.54
26.81	94.8	Flexure	kip-ft	242.12	11.90	58.40	2.993	104.75
26.81	94.8	Shear	kip	-118.33	-7.55	-39.48	2.121	74.25
27.11	95.8	Shear	kip	-125.83	-7.72	-40.07	2.230	78.06
28.29	100.0	Flexure	kip-ft	81.43	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294D
Bridge ID: 874294D

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 11:44:40
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 11:45:40

Structure Definition Name: End Span 1 (or 3) - PS Conc PSU
Member Name: G9
Member Alternative Name: 17"x36" INT PSU - w/ Conc Repair + Post Tensioning

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 1

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location					DL +					
(ft)	Percent	Limit State	Units	Capacity	Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	129.09	7.72	20.37	3.351	120.64	4.344	156.39
1.69	6.0	Flexure	kip-ft	243.32	13.52	33.69	3.841	138.27	4.979	179.24
1.69	6.0	Shear	kip	118.17	7.42	19.81	3.141	113.07	4.072	146.57
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.25	7.736	278.50		
2.83	10.0	Flexure	kip-ft	284.36	21.61	53.30	2.759	99.33	3.577	128.76
2.83	10.0	Shear	kip	92.75	6.76	18.60	2.590	93.25	3.358	120.88
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.700	169.19		
5.66	20.0	Flexure	kip-ft	304.65	38.40	90.83	1.615	58.13	2.093	75.35
5.66	20.0	Shear	kip	85.08	5.11	15.62	2.878	103.61	3.731	134.31
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	0.67	2.527	90.96		
8.49	30.0	Flexure	kip-ft	304.65	50.23	112.61	1.227	44.18	1.591	57.27
8.49	30.0	Shear	kip	59.51	3.30	12.71	2.491	89.69	4.720	169.93
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	0.83	1.907	68.64		
11.32	40.0	Flexure	kip-ft	304.65	57.22	118.63	1.123	40.43	1.456	52.41
11.32	40.0	Shear	kip	54.86	1.65	9.84	3.066	110.39	6.250	225.00
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	0.87	1.736	62.51		
14.15	50.0	Flexure		304.65	59.54	109.11	1.206	43.40	1.563	56.26

14.15	50.0	Shear	kip-ft	-64.58	-0.00	-7.03	5.251	189.03	8.967	322.81
14.15	50.0	Concrete Stresses	ksi	1.63	0.44	0.80	1.861	67.00		
16.98	60.0	Flexure	kip-ft	304.65	57.20	118.63	1.123	40.43	1.456	52.41
16.98	60.0	Shear	kip	-54.87	-1.65	-9.84	3.066	110.38	6.249	224.98
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	0.87	1.737	62.51		
19.80	70.0	Flexure	kip-ft	304.65	50.19	112.61	1.228	44.19	1.591	57.29
19.80	70.0	Shear	kip	-59.53	-3.30	-12.71	2.492	89.71	4.720	169.91
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	0.83	1.907	68.66		
22.63	80.0	Flexure	kip-ft	304.65	38.37	90.83	1.615	58.13	2.093	75.36
22.63	80.0	Shear	kip	-85.08	-5.12	-15.62	2.878	103.60	3.730	134.30
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	0.67	2.527	90.97		
25.46	90.0	Flexure	kip-ft	291.74	21.57	53.30	2.839	102.20	3.680	132.49
25.46	90.0	Shear	kip	-89.88	-6.76	-18.60	2.502	90.07	3.243	116.75
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.701	169.23		
26.81	94.8	Flexure	kip-ft	256.36	11.90	29.83	4.626	166.53	5.996	215.87
26.81	94.8	Shear	kip	-118.33	-7.55	-20.03	3.106	111.81	4.026	144.94
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.22	8.804	316.93		
27.11	95.8	Shear	kip	-125.83	-7.72	-20.35	3.262	117.43	4.228	152.22
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 1

Location						Inventory		Inventory		Operating		Operating	
						Rating	Load Rating	Rating	Load Rating	Rating	Load Rating	Rating	Load Rating
(ft)	Percent		Units	Capacity	LL	Factor	(Ton)	Factor	(Ton)	Factor	(Ton)	Factor	(Ton)

		Limit State			DL + Adj- LL*					
0.00	0.0	Flexure	kip- ft	88.32	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.70	-0.00	0.00	99.000	3564.00		
1.17	4.1	Shear	kip	129.09	7.72	19.93	3.425	123.31	4.440	159.85
1.69	6.0	Flexure	kip-ft	243.32	13.52	33.11	3.907	140.67	5.065	182.34
1.69	6.0	Shear	kip	118.17	7.42	19.47	3.196	115.05	4.143	149.13
1.69	6.0	Concrete Stresses	ksi	1.63	0.10	0.24	7.870	283.33		
2.83	10.0	Flexure	kip-ft	284.36	21.61	52.96	2.777	99.96	3.599	129.57
2.83	10.0	Shear	kip	92.75	6.76	18.48	2.607	93.85	3.379	121.65
2.83	10.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.729	170.26		
5.66	20.0	Flexure	kip- ft	304.65	38.40	93.28	1.572	56.60	2.038	73.37
5.66	20.0	Shear	kip	85.08	5.11	16.06	2.801	100.82	3.630	130.69
5.66	20.0	Concrete Stresses	ksi	1.63	0.28	0.69	2.460	88.57		
8.49	30.0	Flexure	kip- ft	304.65	50.23	120.96	1.143	41.13	1.481	53.32
8.49	30.0	Shear	kip	53.03	3.30	13.69	2.042	73.50	4.381	157.72
8.49	30.0	Concrete Stresses	ksi	1.63	0.37	0.89	1.775	63.90		
11.32	40.0	Flexure	kip- ft	304.65	57.22	135.99	0.980	35.27	1.270	45.71
11.32	40.0	Shear	kip	45.04	1.65	11.37	2.159	77.74	4.245	152.83
11.32	40.0	Concrete Stresses	ksi	1.63	0.42	1.00	1.515	54.53		
14.15	50.0	Flexure	kip- ft	304.65	59.54	138.38	0.951	34.23	1.232	44.37
14.15	50.0	Shear	kip	-44.95	-0.00	-9.11	2.818	101.46	5.444	195.99
14.15	50.0	Concrete Stresses	ksi	1.63	0.44	1.02	1.467	52.83		
16.98	60.0	Flexure	kip- ft	304.65	57.20	135.99	0.980	35.27	1.270	45.72
16.98	60.0	Shear	kip	-45.04	-1.65	-11.37	2.159	77.73	4.245	152.83
16.98	60.0	Concrete Stresses	ksi	1.63	0.42	1.00	1.515	54.53		
19.80	70.0	Flexure	kip- ft	304.65	50.19	120.96	1.143	41.14	1.481	53.33
19.80	70.0	Shear	kip	-53.04	-3.30	-13.69	2.042	73.50	4.381	157.70
19.80	70.0	Concrete Stresses	ksi	1.63	0.37	0.89	1.775	63.92		
22.63	80.0	Flexure		304.65	38.37	93.28	1.572	56.61	2.038	73.38

22.63	80.0	Shear	kip-ft	-85.08	-5.12	-16.06	2.800	100.81	3.630	130.68
22.63	80.0	Concrete Stresses	ksi	1.63	0.28	0.69	2.461	88.58		
25.46	90.0	Flexure	kip-ft	291.74	21.57	52.96	2.857	102.85	3.703	133.32
25.46	90.0	Shear	kip	-89.88	-6.76	-18.48	2.518	90.64	3.264	117.50
25.46	90.0	Concrete Stresses	ksi	1.63	0.16	0.39	4.730	170.30		
26.81	94.8	Flexure	kip-ft	256.36	11.90	29.27	4.715	169.73	6.112	220.02
26.81	94.8	Shear	kip	-118.33	-7.55	-19.65	3.166	113.97	4.104	147.74
26.81	94.8	Concrete Stresses	ksi	1.63	0.09	0.22	8.973	323.03		
27.11	95.8	Shear	kip	-125.83	-7.72	-19.91	3.334	120.01	4.321	155.57
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3564.00	99.000	3564.00
28.29	100.0	Concrete Stresses	ksi	0.82	-0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	2772.00
1.17	4.1	Shear	kip	129.09	7.72	11.15	8.238	230.67
1.69	6.0	Flexure	kip-ft	243.32	13.52	18.41	9.462	264.94
1.69	6.0	Shear	kip	118.17	7.42	10.91	7.679	215.03
2.83	10.0	Flexure	kip-ft	284.36	21.61	29.33	6.749	188.96
2.83	10.0	Shear	kip	92.75	6.76	10.37	6.254	175.13
5.66	20.0	Flexure	kip-ft	304.65	38.40	51.10	3.864	108.18
5.66	20.0	Shear	kip	85.08	5.11	9.03	6.703	187.69
8.49	30.0	Flexure	kip-ft	304.65	50.23	65.30	2.849	79.78
8.49	30.0	Shear	kip	85.08	3.30	7.69	8.095	226.66
11.32	40.0	Flexure	kip-ft	304.65	57.22	71.93	2.493	69.81
11.32	40.0	Shear	kip	85.08	1.65	6.36	10.048	281.34
14.15	50.0	Flexure	kip-ft	304.65	59.54	70.99	2.495	69.85

14.15	50.0	Shear	kip	-85.08	-0.00	-5.02	13.040	365.13
16.98	60.0	Flexure	kip-ft	304.65	57.20	71.93	2.493	69.82
16.98	60.0	Shear	kip	-85.08	-1.65	-6.36	10.047	281.31
19.80	70.0	Flexure	kip-ft	304.65	50.19	65.30	2.850	79.80
19.80	70.0	Shear	kip	-85.08	-3.30	-7.69	8.094	226.64
22.63	80.0	Flexure	kip-ft	304.65	38.37	51.10	3.864	108.20
22.63	80.0	Shear	kip	-85.08	-5.12	-9.03	6.702	187.67
25.46	90.0	Flexure	kip-ft	291.74	21.57	29.33	6.944	194.42
25.46	90.0	Shear	kip	-89.88	-6.76	-10.37	6.041	169.14
26.81	94.8	Flexure	kip-ft	256.36	11.90	16.28	11.410	319.48
26.81	94.8	Shear	kip	-118.33	-7.55	-11.01	7.610	213.09
27.11	95.8	Shear	kip	-125.83	-7.72	-11.15	8.018	224.49
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3628.35
1.17	4.1	Shear	kip	129.09	7.72	15.66	5.867	215.02
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.63	6.797	249.10
1.69	6.0	Shear	kip	118.17	7.42	15.19	5.516	202.17
2.83	10.0	Flexure	kip-ft	284.36	21.61	40.46	4.892	179.30
2.83	10.0	Shear	kip	92.75	6.76	14.30	4.534	166.17
5.66	20.0	Flexure	kip-ft	304.65	38.40	71.13	2.775	101.72
5.66	20.0	Shear	kip	85.08	5.11	12.57	4.815	176.48
8.49	30.0	Flexure	kip-ft	304.65	50.23	92.01	2.022	74.11
8.49	30.0	Shear	kip	85.08	3.30	10.84	5.745	210.55
11.32	40.0	Flexure	kip-ft	304.65	57.22	103.09	1.739	63.75
11.32	40.0	Shear	kip	85.08	1.65	9.11	7.010	256.93
14.15	50.0	Flexure	kip-ft	304.65	59.54	104.38	1.697	62.18
14.15	50.0	Shear	kip	-85.08	-0.00	-7.38	8.869	325.04
16.98	60.0	Flexure	kip-ft	304.65	57.20	103.09	1.740	63.76
16.98	60.0	Shear	kip	-85.08	-1.65	-9.11	7.010	256.90
19.80	70.0	Flexure	kip-ft	304.65	50.19	92.01	2.022	74.12

19.80	70.0	Shear	kip	-85.08	-3.30	-10.84	5.744	210.53
22.63	80.0	Flexure	kip-ft	304.65	38.37	71.13	2.776	101.73
22.63	80.0	Shear	kip	-85.08	-5.12	-12.57	4.815	176.46
25.46	90.0	Flexure	kip-ft	291.74	21.57	40.46	5.034	184.49
25.46	90.0	Shear	kip	-89.88	-6.76	-14.30	4.379	160.50
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.74	8.167	299.32
26.81	94.8	Shear	kip	-118.33	-7.55	-15.38	5.447	199.65
27.11	95.8	Shear	kip	-125.83	-7.72	-15.65	5.711	209.30
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

Location							Legal Rating	Legal Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.09	7.72	15.73	5.842	233.70
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.93	6.717	268.67
1.69	6.0	Shear	kip	118.17	7.42	15.37	5.451	218.06
2.83	10.0	Flexure	kip-ft	284.36	21.61	41.23	4.802	192.06
2.83	10.0	Shear	kip	92.75	6.76	14.57	4.450	178.00
5.66	20.0	Flexure	kip-ft	304.65	38.40	71.33	2.768	110.72
5.66	20.0	Shear	kip	85.08	5.11	12.61	4.802	192.09
8.49	30.0	Flexure	kip-ft	304.65	50.23	90.30	2.060	82.42
8.49	30.0	Shear	kip	85.08	3.30	10.64	5.854	234.15
11.32	40.0	Flexure	kip-ft	304.65	57.22	98.14	1.827	73.09
11.32	40.0	Shear	kip	85.08	1.65	8.67	7.364	294.57
14.15	50.0	Flexure	kip-ft	304.65	59.54	103.05	1.719	68.74
14.15	50.0	Shear	kip	-85.08	-0.00	-6.71	9.756	390.22
16.98	60.0	Flexure	kip-ft	304.65	57.20	98.14	1.827	73.10
16.98	60.0	Shear	kip	-85.08	-1.65	-8.67	7.364	294.54
19.80	70.0	Flexure	kip-ft	304.65	50.19	90.30	2.061	82.43
19.80	70.0	Shear	kip	-85.08	-3.30	-10.64	5.853	234.13
22.63	80.0	Flexure	kip-ft	304.65	38.37	71.33	2.768	110.73
22.63	80.0	Shear	kip	-85.08	-5.12	-12.61	4.802	192.07
25.46	90.0	Flexure	kip-ft	291.74	21.57	41.23	4.940	197.62

25.46	90.0	Shear	kip	-89.88	-6.76	-14.57	4.298	171.92
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.94	8.096	323.85
26.81	94.8	Shear	kip	-118.33	-7.55	-15.51	5.400	216.01
27.11	95.8	Shear	kip	-125.83	-7.72	-15.72	5.686	227.44
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Permit	Permit
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	5940.00
1.69	6.0	Flexure	kip-ft	243.32	13.52	40.86	4.618	277.07
2.83	10.0	Flexure	kip-ft	284.36	21.61	64.51	3.324	199.45
5.66	20.0	Flexure	kip-ft	304.65	38.40	109.25	1.958	117.46
8.49	30.0	Flexure	kip-ft	304.65	50.23	134.22	1.502	90.10
11.32	40.0	Flexure	kip-ft	304.65	57.22	139.42	1.393	83.60
14.15	50.0	Flexure	kip-ft	304.65	59.54	125.17	1.533	91.97
16.98	60.0	Flexure	kip-ft	304.65	57.20	139.42	1.394	83.61
19.80	70.0	Flexure	kip-ft	304.65	50.19	134.22	1.502	90.12
22.63	80.0	Flexure	kip-ft	304.65	38.37	109.25	1.958	117.47
25.46	90.0	Flexure	kip-ft	291.74	21.57	64.51	3.420	205.22
26.81	94.8	Flexure	kip-ft	256.36	11.90	36.20	5.560	333.58
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating

(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3960.00
1.17	4.1	Shear	kip	129.09	7.72	15.36	5.983	239.30
1.69	6.0	Flexure	kip-ft	243.32	13.52	25.26	6.895	275.80
1.69	6.0	Shear	kip	118.17	7.42	14.97	5.596	223.84
2.83	10.0	Flexure	kip-ft	284.36	21.61	39.92	4.958	198.33
2.83	10.0	Shear	kip	92.75	6.76	14.11	4.595	183.81
5.66	20.0	Flexure	kip-ft	304.65	38.40	67.83	2.911	116.42
5.66	20.0	Shear	kip	85.08	5.11	11.99	5.050	201.99
8.49	30.0	Flexure	kip-ft	304.65	50.23	83.72	2.222	88.89
8.49	30.0	Shear	kip	85.08	3.30	9.86	6.314	252.56
11.32	40.0	Flexure	kip-ft	304.65	57.22	93.25	1.923	76.92
11.32	40.0	Shear	kip	85.08	1.65	7.74	8.252	330.08
14.15	50.0	Flexure	kip-ft	304.65	59.54	93.59	1.892	75.69
14.15	50.0	Shear	kip	-85.08	-0.00	-6.08	10.765	430.60
16.98	60.0	Flexure	kip-ft	304.65	57.20	93.25	1.923	76.93
16.98	60.0	Shear	kip	-85.08	-1.65	-7.74	8.251	330.04
19.80	70.0	Flexure	kip-ft	304.65	50.19	83.72	2.223	88.91
19.80	70.0	Shear	kip	-85.08	-3.30	-9.86	6.313	252.53
22.63	80.0	Flexure	kip-ft	304.65	38.37	67.83	2.911	116.44
22.63	80.0	Shear	kip	-85.08	-5.12	-11.99	5.049	201.97
25.46	90.0	Flexure	kip-ft	291.74	21.57	39.92	5.102	204.07
25.46	90.0	Shear	kip	-89.88	-6.76	-14.11	4.438	177.53
26.81	94.8	Flexure	kip-ft	256.36	11.90	22.37	8.303	332.11
26.81	94.8	Shear	kip	-118.33	-7.55	-15.13	5.538	221.51
27.11	95.8	Shear	kip	-125.83	-7.72	-15.35	5.823	232.91
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	1683.00
1.17	4.1	Shear	kip	129.09	7.72	10.65	8.625	146.63

1.69	6.0	Flexure	kip-ft	243.32	13.52	17.56	9.917	168.59
1.69	6.0	Shear	kip	118.17	7.42	10.41	8.049	136.83
2.83	10.0	Flexure	kip-ft	284.36	21.61	27.92	7.091	120.54
2.83	10.0	Shear	kip	92.75	6.76	9.87	6.572	111.72
5.66	20.0	Flexure	kip-ft	304.65	38.40	48.27	4.090	69.54
5.66	20.0	Shear	kip	85.08	5.11	8.53	7.097	120.64
8.49	30.0	Flexure	kip-ft	304.65	50.23	61.05	3.047	51.81
8.49	30.0	Shear	kip	85.08	3.30	7.19	8.658	147.19
11.32	40.0	Flexure	kip-ft	304.65	57.22	66.26	2.706	46.01
11.32	40.0	Shear	kip	85.08	1.65	5.86	10.907	185.42
14.15	50.0	Flexure	kip-ft	304.65	59.54	63.91	2.771	47.11
14.15	50.0	Shear	kip	-85.08	-0.00	-4.52	14.485	246.24
16.98	60.0	Flexure	kip-ft	304.65	57.20	66.26	2.707	46.01
16.98	60.0	Shear	kip	-85.08	-1.65	-5.86	10.906	185.40
19.80	70.0	Flexure	kip-ft	304.65	50.19	61.05	3.048	51.82
19.80	70.0	Shear	kip	-85.08	-3.30	-7.19	8.657	147.18
22.63	80.0	Flexure	kip-ft	304.65	38.37	48.27	4.091	69.54
22.63	80.0	Shear	kip	-85.08	-5.12	-8.53	7.096	120.63
25.46	90.0	Flexure	kip-ft	291.74	21.57	27.92	7.296	124.03
25.46	90.0	Shear	kip	-89.88	-6.76	-9.87	6.347	107.90
26.81	94.8	Flexure	kip-ft	256.36	11.90	15.54	11.954	203.21
26.81	94.8	Shear	kip	-118.33	-7.55	-10.51	7.973	135.54
27.11	95.8	Shear	kip	-125.83	-7.72	-10.65	8.394	142.71
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3267.00
1.17	4.1	Shear	kip	129.09	7.72	18.97	4.842	159.80
1.69	6.0	Flexure	kip-ft	243.32	13.52	31.22	5.579	184.12
1.69	6.0	Shear	kip	118.17	7.42	18.50	4.528	149.43
2.83	10.0	Flexure	kip-ft	284.36	21.61	49.37	4.009	132.31
2.83	10.0	Shear	kip	92.75	6.76	17.45	3.716	122.62

5.66	20.0	Flexure	kip-ft	304.65	38.40	84.06	2.349	77.51
5.66	20.0	Shear	kip	85.08	5.11	14.86	4.075	134.48
8.49	30.0	Flexure	kip-ft	304.65	50.23	104.05	1.788	59.01
8.49	30.0	Shear	kip	85.08	3.30	12.26	5.080	167.65
11.32	40.0	Flexure	kip-ft	304.65	57.22	116.56	1.538	50.77
11.32	40.0	Shear	kip	85.08	1.65	9.66	6.609	218.10
14.15	50.0	Flexure	kip-ft	304.65	59.54	118.00	1.501	49.53
14.15	50.0	Shear	kip	-85.08	-0.00	-7.38	8.869	292.67
16.98	60.0	Flexure	kip-ft	304.65	57.20	116.56	1.539	50.77
16.98	60.0	Shear	kip	-85.08	-1.65	-9.66	6.609	218.08
19.80	70.0	Flexure	kip-ft	304.65	50.19	104.05	1.788	59.02
19.80	70.0	Shear	kip	-85.08	-3.30	-12.26	5.080	167.63
22.63	80.0	Flexure	kip-ft	304.65	38.37	84.06	2.349	77.52
22.63	80.0	Shear	kip	-85.08	-5.12	-14.86	4.075	134.46
25.46	90.0	Flexure	kip-ft	291.74	21.57	49.37	4.125	136.14
25.46	90.0	Shear	kip	-89.88	-6.76	-17.45	3.589	118.44
26.81	94.8	Flexure	kip-ft	256.36	11.90	27.65	6.719	221.73
26.81	94.8	Shear	kip	-118.33	-7.55	-18.69	4.482	147.89
27.11	95.8	Shear	kip	-125.83	-7.72	-18.96	4.713	155.53
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc Repair + Post Tensioning
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 1

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj -LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	88.32	0.00	0.00	99.000	3465.00
1.17	4.1	Shear	kip	129.09	7.72	19.76	4.649	162.71
1.69	6.0	Flexure	kip-ft	243.32	13.52	32.50	5.359	187.56
1.69	6.0	Shear	kip	118.17	7.42	19.26	4.349	152.22
2.83	10.0	Flexure	kip-ft	284.36	21.61	51.35	3.855	134.94
2.83	10.0	Shear	kip	92.75	6.76	18.15	3.573	125.06
5.66	20.0	Flexure	kip-ft	304.65	38.40	87.11	2.266	79.32
5.66	20.0	Shear	kip	85.08	5.11	15.40	3.932	137.62
8.49	30.0	Flexure	kip-ft	304.65	50.23	111.07	1.675	58.63
8.49	30.0	Shear	kip	85.08	3.30	12.64	4.926	172.42

11.32	40.0	Flexure	kip-ft	304.65	57.22	127.15	1.410	49.36
11.32	40.0	Shear	kip	84.27	1.65	9.99	6.330	221.56
14.15	50.0	Flexure	kip-ft	304.65	59.54	127.65	1.387	48.56
14.15	50.0	Shear	kip	-85.08	-0.00	-7.78	8.408	294.29
16.98	60.0	Flexure	kip-ft	304.65	57.20	127.15	1.411	49.37
16.98	60.0	Shear	kip	-84.29	-1.65	-9.99	6.331	221.58
19.80	70.0	Flexure	kip-ft	304.65	50.19	111.07	1.675	58.64
19.80	70.0	Shear	kip	-85.08	-3.30	-12.64	4.926	172.40
22.63	80.0	Flexure	kip-ft	304.65	38.37	87.11	2.267	79.33
22.63	80.0	Shear	kip	-85.08	-5.12	-15.40	3.932	137.61
25.46	90.0	Flexure	kip-ft	291.74	21.57	51.35	3.967	138.84
25.46	90.0	Shear	kip	-89.88	-6.76	-18.15	3.451	120.79
26.81	94.8	Flexure	kip-ft	256.36	11.90	28.79	6.452	225.84
26.81	94.8	Shear	kip	-118.33	-7.55	-19.46	4.304	150.63
27.11	95.8	Shear	kip	-125.83	-7.72	-19.75	4.525	158.36
28.29	100.0	Flexure	kip-ft	86.22	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294D
Bridge ID: 874294D

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 20:33:28
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 20:35:00

Structure Definition Name: INT Span 2 - PS Conc PSU
Member Name: G8
Member Alternative Name: 17"x36" INT PSU - Existing Deteriorated

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory	Inventory	Operating	Operating
Location							Rating	Load Rating	Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip- ft	127.58	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.86	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	94.16	10.73	48.82	0.945	34.03	1.225	44.11
1.48	3.8	Flexure	kip-ft	277.16	16.30	71.63	2.048	73.74	2.655	95.59
1.48	3.8	Shear	kip	89.01	10.52	48.15	0.900	32.40	1.167	42.01
1.48	3.8	Concrete Stresses	ksi	1.77	0.12	0.53	3.928	141.41		
3.85	10.0	Flexure	kip-ft	325.50	39.61	171.07	0.922	33.19	1.195	43.02
3.85	10.0	Shear	kip	28.01	9.14	43.77	0.216	7.79	0.522	18.79
3.85	10.0	Concrete Stresses	ksi	1.77	0.29	1.26	1.474	53.08		
7.70	20.0	Flexure	kip-ft	325.50	70.48	292.21	0.464	16.71	0.602	21.66
7.70	20.0	Shear	kip	17.93	6.90	36.77	0.145	5.21	0.229	8.25
7.70	20.0	Concrete Stresses	ksi	1.77	0.52	2.15	0.731	26.32		
11.55	30.0	Flexure	kip-ft	325.50	92.34	365.43	0.328	11.83	0.426	15.33
11.55	30.0	Shear	kip	17.93	4.49	30.09	0.234	8.42	0.303	10.92
11.55	30.0	Concrete Stresses	ksi	1.77	0.68	2.69	0.510	18.35		
15.40	40.0	Flexure	kip- ft	325.50	105.30	402.57	0.275	9.91	0.357	12.84
15.40	40.0	Shear	kip	17.93	2.24	24.02	0.360	12.96	0.466	16.79
15.40	40.0	Concrete Stresses	ksi	1.77	0.77	2.96	0.423	15.21		
19.25	50.0	Flexure	kip- ft	325.50	109.62	400.72	0.269	9.68	0.348	12.54
19.25	50.0	Shear	kip	-17.93	0.00	-18.10	0.566	20.38	0.734	26.42

19.25	50.0	Concrete Stresses	ksi	1.77	0.81	2.95	0.411	14.80		
23.10	60.0	Flexure	kip-ft	325.50	105.30	402.57	0.275	9.91	0.357	12.84
23.10	60.0	Shear	kip	-17.93	-2.24	-24.02	0.360	12.96	0.466	16.79
23.10	60.0	Concrete Stresses	ksi	1.77	0.77	2.96	0.423	15.21		
26.95	70.0	Flexure	kip-ft	341.96	92.34	365.43	0.354	12.75	0.459	16.53
26.95	70.0	Shear	kip	-18.03	-4.49	-30.09	0.236	8.49	0.311	11.19
26.95	70.0	Concrete Stresses	ksi	1.77	0.68	2.69	0.510	18.35		
30.80	80.0	Flexure	kip-ft	325.50	70.48	292.21	0.464	16.71	0.602	21.66
30.80	80.0	Shear	kip	-17.93	-6.90	-36.77	0.145	5.21	0.229	8.25
30.80	80.0	Concrete Stresses	ksi	1.77	0.52	2.15	0.731	26.32		
34.65	90.0	Flexure	kip-ft	325.50	39.61	171.07	0.922	33.19	1.195	43.02
34.65	90.0	Shear	kip	-28.01	-9.14	-43.77	0.216	7.79	0.522	18.79
34.65	90.0	Concrete Stresses	ksi	1.77	0.29	1.26	1.474	53.08		
37.02	96.2	Flexure	kip-ft	277.16	16.30	71.63	2.048	73.74	2.655	95.59
37.02	96.2	Shear	kip	-89.01	-10.52	-48.15	0.900	32.40	1.167	42.01
37.02	96.2	Concrete Stresses	ksi	1.77	0.12	0.53	3.928	141.41		
37.38	97.1	Shear	kip	-94.28	-10.73	-48.83	0.946	34.07	1.227	44.16
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	0.86	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory	Inventory	Operating	Operating
Location							Rating	Load Rating	Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip- ft	127.58	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0		ksi	0.86	-0.00	0.00	99.000	3564.00		

		Concrete Stresses								
1.12	2.9	Shear	kip	94.16	10.73	43.63	1.058	38.07	1.371	49.35
1.48	3.8	Flexure	kip-ft	277.16	16.30	64.20	2.286	82.28	2.963	106.66
1.48	3.8	Shear	kip	89.01	10.52	43.13	1.005	36.18	1.303	46.90
1.48	3.8	Concrete Stresses	ksi	1.77	0.12	0.47	4.383	157.78		
3.85	10.0	Flexure	kip-ft	325.50	39.61	155.89	1.012	36.42	1.311	47.21
3.85	10.0	Shear	kip	32.15	9.14	39.82	0.297	10.71	0.729	26.24
3.85	10.0	Concrete Stresses	ksi	1.77	0.29	1.15	1.618	58.25		
7.70	20.0	Flexure	kip-ft	325.50	70.48	275.36	0.493	17.74	0.639	22.99
7.70	20.0	Shear	kip	17.93	6.90	34.58	0.154	5.54	0.278	10.00
7.70	20.0	Concrete Stresses	ksi	1.77	0.52	2.02	0.776	27.93		
11.55	30.0	Flexure	kip-ft	325.50	92.34	358.42	0.335	12.06	0.434	15.63
11.55	30.0	Shear	kip	17.93	4.49	29.48	0.239	8.60	0.310	11.14
11.55	30.0	Concrete Stresses	ksi	1.77	0.68	2.64	0.520	18.71		
15.40	40.0	Flexure	kip- ft	325.50	105.30	405.06	0.273	9.85	0.355	12.76
15.40	40.0	Shear	kip	17.93	2.24	24.53	0.352	12.69	0.457	16.44
15.40	40.0	Concrete Stresses	ksi	1.77	0.77	2.98	0.420	15.12		
19.25	50.0	Flexure	kip- ft	325.50	109.62	415.29	0.259	9.34	0.336	12.10
19.25	50.0	Shear	kip	-17.93	0.00	-19.73	0.519	18.70	0.673	24.24
19.25	50.0	Concrete Stresses	ksi	1.77	0.81	3.05	0.397	14.28		
23.10	60.0	Flexure	kip- ft	325.50	105.30	405.06	0.273	9.85	0.355	12.76
23.10	60.0	Shear	kip	-17.93	-2.24	-24.53	0.352	12.69	0.457	16.44
23.10	60.0	Concrete Stresses	ksi	1.77	0.77	2.98	0.420	15.12		
26.95	70.0	Flexure	kip-ft	341.96	92.34	358.42	0.361	13.00	0.468	16.85
26.95	70.0	Shear	kip	-18.03	-4.49	-29.48	0.241	8.66	0.328	11.79
26.95	70.0	Concrete Stresses	ksi	1.77	0.68	2.64	0.520	18.71		
30.80	80.0	Flexure	kip-ft	325.50	70.48	275.36	0.493	17.74	0.639	22.99
30.80	80.0	Shear	kip	-17.93	-6.90	-34.58	0.154	5.54	0.278	10.00
30.80	80.0	Concrete Stresses	ksi	1.77	0.52	2.02	0.776	27.93		
34.65	90.0	Flexure	kip-ft	325.50	39.61	155.89	1.012	36.42	1.311	47.21
34.65	90.0	Shear	kip	-32.15	-9.14	-39.82	0.297	10.71	0.729	26.24
34.65	90.0	Concrete Stresses	ksi	1.77	0.29	1.15	1.618	58.25		

37.02	96.2	Flexure	kip-ft	277.16	16.30	64.20	2.286	82.28	2.963	106.66
37.02	96.2	Shear	kip	-89.01	-10.52	-43.13	1.005	36.18	1.303	46.90
37.02	96.2	Concrete Stresses	ksi	1.77	0.12	0.47	4.383	157.78		
37.38	97.1	Shear	kip	-94.28	-10.73	-43.64	1.059	38.12	1.373	49.41
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	0.86	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	2772.00
1.12	2.9	Shear	kip	94.16	10.73	26.80	2.317	64.89
1.48	3.8	Flexure	kip-ft	277.16	16.30	39.03	5.060	141.69
1.48	3.8	Shear	kip	89.01	10.52	26.39	2.211	61.91
3.85	10.0	Flexure	kip-ft	325.50	39.61	91.00	2.333	65.32
3.85	10.0	Shear	kip	70.05	9.14	23.64	1.908	53.42
7.70	20.0	Flexure	kip-ft	325.50	70.48	147.98	1.234	34.55
7.70	20.0	Shear	kip	56.12	6.90	19.22	1.901	53.23
11.55	30.0	Flexure	kip-ft	325.50	92.34	190.63	0.848	23.73
11.55	30.0	Shear	kip	34.48	4.49	16.51	1.345	37.67
15.40	40.0	Flexure	kip-ft	325.50	105.30	215.01	0.694	19.42
15.40	40.0	Shear	kip	28.84	2.24	13.79	1.452	40.66
19.25	50.0	Flexure	kip-ft	325.50	109.62	213.27	0.680	19.03
19.25	50.0	Shear	kip	-29.24	0.00	-11.08	2.030	56.84
23.10	60.0	Flexure	kip-ft	325.50	105.30	215.01	0.694	19.42
23.10	60.0	Shear	kip	-28.84	-2.24	-13.79	1.452	40.66
26.95	70.0	Flexure	kip-ft	341.96	92.34	190.63	0.914	25.59
26.95	70.0	Shear	kip	-38.79	-4.49	-16.51	1.546	43.29
30.80	80.0	Flexure	kip-ft	325.50	70.48	147.98	1.234	34.55
30.80	80.0	Shear	kip	-56.12	-6.90	-19.22	1.901	53.23
34.65	90.0	Flexure	kip-ft	325.50	39.61	91.00	2.333	65.32
34.65	90.0	Shear	kip	-70.05	-9.14	-23.64	1.908	53.42

37.02	96.2	Flexure	kip-ft	277.16	16.30	39.03	5.060	141.69
37.02	96.2	Shear	kip	-89.01	-10.52	-26.39	2.211	61.91
37.38	97.1	Shear	kip	-94.28	-10.73	-26.81	2.320	64.96
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	3628.35
1.12	2.9	Shear	kip	94.16	10.73	37.58	1.653	60.57
1.48	3.8	Flexure	kip-ft	277.16	16.30	54.79	3.605	132.12
1.48	3.8	Shear	kip	89.01	10.52	37.04	1.575	57.73
3.85	10.0	Flexure	kip-ft	325.50	39.61	129.53	1.639	60.07
3.85	10.0	Shear	kip	70.05	9.14	33.65	1.340	49.12
7.70	20.0	Flexure	kip-ft	325.50	70.48	218.51	0.836	30.63
7.70	20.0	Shear	kip	30.43	6.90	28.38	0.591	21.66
11.55	30.0	Flexure	kip-ft	325.50	92.34	266.94	0.605	22.19
11.55	30.0	Shear	kip	22.81	4.49	23.11	0.573	20.98
15.40	40.0	Flexure	kip-ft	325.50	105.30	295.17	0.505	18.52
15.40	40.0	Shear	kip	19.93	2.24	19.17	0.687	25.19
19.25	50.0	Flexure	kip-ft	325.50	109.62	301.38	0.481	17.63
19.25	50.0	Shear	kip	-19.60	0.00	-15.66	0.963	35.29
23.10	60.0	Flexure	kip-ft	325.50	105.30	295.17	0.505	18.52
23.10	60.0	Shear	kip	-19.93	-2.24	-19.17	0.687	25.19
26.95	70.0	Flexure	kip-ft	341.96	92.34	266.94	0.653	23.92
26.95	70.0	Shear	kip	-26.73	-4.49	-23.11	0.703	25.77
30.80	80.0	Flexure	kip-ft	325.50	70.48	218.51	0.836	30.63
30.80	80.0	Shear	kip	-30.43	-6.90	-28.38	0.591	21.66
34.65	90.0	Flexure	kip-ft	325.50	39.61	129.53	1.639	60.07
34.65	90.0	Shear	kip	-70.05	-9.14	-33.65	1.340	49.12
37.02	96.2	Flexure	kip-ft	277.16	16.30	54.79	3.605	132.12
37.02	96.2	Shear	kip	-89.01	-10.52	-37.04	1.575	57.73
37.38	97.1	Shear	kip	-94.28	-10.73	-37.59	1.655	60.64
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
C 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	94.16	10.73	37.63	1.651	66.02
1.48	3.8	Flexure	kip-ft	277.16	16.30	54.90	3.598	143.92
1.48	3.8	Shear	kip	89.01	10.52	37.11	1.572	62.89
3.85	10.0	Flexure	kip-ft	325.50	39.61	129.65	1.638	65.50
3.85	10.0	Shear	kip	70.05	9.14	33.67	1.339	53.57
7.70	20.0	Flexure	kip-ft	325.50	70.48	216.28	0.844	33.77
7.70	20.0	Shear	kip	30.85	6.90	28.09	0.609	24.35
11.55	30.0	Flexure	kip-ft	325.50	92.34	268.72	0.601	24.05
11.55	30.0	Shear	kip	22.63	4.49	23.27	0.563	22.51
15.40	40.0	Flexure	kip-ft	325.50	105.30	300.26	0.497	19.87
15.40	40.0	Shear	kip	19.55	2.24	19.28	0.668	26.72
19.25	50.0	Flexure	kip-ft	325.50	109.62	310.88	0.466	18.65
19.25	50.0	Shear	kip	-18.99	0.00	-14.79	0.987	39.49
23.10	60.0	Flexure	kip-ft	325.50	105.30	300.26	0.497	19.87
23.10	60.0	Shear	kip	-19.55	-2.24	-19.28	0.668	26.72
26.95	70.0	Flexure	kip-ft	341.96	92.34	268.72	0.648	25.94
26.95	70.0	Shear	kip	-26.54	-4.49	-23.27	0.692	27.68
30.80	80.0	Flexure	kip-ft	325.50	70.48	216.28	0.844	33.77
30.80	80.0	Shear	kip	-30.85	-6.90	-28.09	0.609	24.35
34.65	90.0	Flexure	kip-ft	325.50	39.61	129.65	1.638	65.50
34.65	90.0	Shear	kip	-70.05	-9.14	-33.67	1.339	53.57
37.02	96.2	Flexure	kip-ft	277.16	16.30	54.90	3.598	143.92
37.02	96.2	Shear	kip	-89.01	-10.52	-37.11	1.572	62.89
37.38	97.1	Shear	kip	-94.28	-10.73	-37.64	1.653	66.10
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
FL120 Span < 200ft

Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Permit	Permit
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	5940.00
1.48	3.8	Flexure	kip-ft	277.16	16.30	84.85	2.522	151.31
3.85	10.0	Flexure	kip-ft	325.50	39.61	201.93	1.139	68.34
7.70	20.0	Flexure	kip-ft	325.50	70.48	342.42	0.578	34.66
11.55	30.0	Flexure	kip-ft	325.50	92.34	424.27	0.413	24.76
15.40	40.0	Flexure	kip-ft	325.50	105.30	464.01	0.348	20.89
19.25	50.0	Flexure	kip-ft	325.50	109.62	457.59	0.343	20.59
23.10	60.0	Flexure	kip-ft	325.50	105.30	464.01	0.348	20.89
26.95	70.0	Flexure	kip-ft	341.96	92.34	424.27	0.445	26.70
30.80	80.0	Flexure	kip-ft	325.50	70.48	342.42	0.578	34.66
34.65	90.0	Flexure	kip-ft	325.50	39.61	201.93	1.139	68.34
37.02	96.2	Flexure	kip-ft	277.16	16.30	84.85	2.522	151.31
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated

ST 5

Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	94.16	10.73	34.37	1.807	72.28
1.48	3.8	Flexure	kip-ft	277.16	16.30	50.25	3.931	157.22
1.48	3.8	Shear	kip	89.01	10.52	33.97	1.717	68.70
3.85	10.0	Flexure	kip-ft	325.50	39.61	120.59	1.761	70.42
3.85	10.0	Shear	kip	70.05	9.14	31.32	1.440	57.59
7.70	20.0	Flexure	kip-ft	325.50	70.48	207.99	0.878	35.12

7.70	20.0	Shear	kip	32.53	6.90	27.01	0.681	27.24
11.55	30.0	Flexure	kip-ft	325.50	92.34	262.21	0.616	24.65
11.55	30.0	Shear	kip	23.31	4.49	22.70	0.600	23.99
15.40	40.0	Flexure	kip-ft	325.50	105.30	294.75	0.506	20.24
15.40	40.0	Shear	kip	20.02	2.24	18.39	0.720	28.80
19.25	50.0	Flexure	kip-ft	325.50	109.62	299.85	0.483	19.34
19.25	50.0	Shear	kip	-19.83	0.00	-14.08	1.083	43.33
23.10	60.0	Flexure	kip-ft	325.50	105.30	294.75	0.506	20.24
23.10	60.0	Shear	kip	-20.02	-2.24	-18.39	0.720	28.80
26.95	70.0	Flexure	kip-ft	341.96	92.34	262.21	0.665	26.58
26.95	70.0	Shear	kip	-27.25	-4.49	-22.70	0.733	29.33
30.80	80.0	Flexure	kip-ft	325.50	70.48	207.99	0.878	35.12
30.80	80.0	Shear	kip	-32.53	-6.90	-27.01	0.681	27.24
34.65	90.0	Flexure	kip-ft	325.50	39.61	120.59	1.761	70.42
34.65	90.0	Shear	kip	-70.05	-9.14	-31.32	1.440	57.59
37.02	96.2	Flexure	kip-ft	277.16	16.30	50.25	3.931	157.22
37.02	96.2	Shear	kip	-89.01	-10.52	-33.97	1.717	68.70
37.38	97.1	Shear	kip	-94.28	-10.73	-34.38	1.809	72.37
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	1683.00
1.12	2.9	Shear	kip	94.16	10.73	23.11	2.688	45.70
1.48	3.8	Flexure	kip-ft	277.16	16.30	33.81	5.843	99.32
1.48	3.8	Shear	kip	89.01	10.52	22.86	2.553	43.40
3.85	10.0	Flexure	kip-ft	325.50	39.61	81.56	2.603	44.25
3.85	10.0	Shear	kip	70.05	9.14	21.19	2.129	36.19
7.70	20.0	Flexure	kip-ft	325.50	70.48	142.24	1.284	21.83
7.70	20.0	Shear	kip	60.86	6.90	18.47	2.175	36.98
11.55	30.0	Flexure	kip-ft	325.50	92.34	182.02	0.888	15.09
11.55	30.0	Shear	kip	36.63	4.49	15.76	1.514	25.74
15.40	40.0	Flexure	kip-ft	325.50	105.30	200.90	0.742	12.62

15.40	40.0	Shear	kip	31.22	2.24	13.05	1.675	28.48
19.25	50.0	Flexure	kip-ft	325.50	109.62	198.90	0.729	12.39
19.25	50.0	Shear	kip	-31.73	0.00	-10.33	2.362	40.16
23.10	60.0	Flexure	kip-ft	325.50	105.30	200.90	0.742	12.62
23.10	60.0	Shear	kip	-31.22	-2.24	-13.05	1.675	28.48
26.95	70.0	Flexure	kip-ft	341.96	92.34	182.02	0.957	16.28
26.95	70.0	Shear	kip	-40.95	-4.49	-15.76	1.725	29.33
30.80	80.0	Flexure	kip-ft	325.50	70.48	142.24	1.284	21.83
30.80	80.0	Shear	kip	-60.86	-6.90	-18.47	2.175	36.98
34.65	90.0	Flexure	kip-ft	325.50	39.61	81.56	2.603	44.25
34.65	90.0	Shear	kip	-70.05	-9.14	-21.19	2.129	36.19
37.02	96.2	Flexure	kip-ft	277.16	16.30	33.81	5.843	99.32
37.02	96.2	Shear	kip	-89.01	-10.52	-22.86	2.553	43.40
37.38	97.1	Shear	kip	-94.28	-10.73	-23.11	2.691	45.75
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	3267.00
1.12	2.9	Shear	kip	94.16	10.73	42.31	1.468	48.44
1.48	3.8	Flexure	kip-ft	277.16	16.30	61.87	3.193	105.35
1.48	3.8	Shear	kip	89.01	10.52	41.83	1.395	46.03
3.85	10.0	Flexure	kip-ft	325.50	39.61	148.55	1.429	47.16
3.85	10.0	Shear	kip	61.06	9.14	38.58	0.990	32.65
7.70	20.0	Flexure	kip-ft	325.50	70.48	256.55	0.712	23.49
7.70	20.0	Shear	kip	24.68	6.90	33.32	0.371	12.23
11.55	30.0	Flexure	kip-ft	325.50	92.34	323.99	0.499	16.46
11.55	30.0	Shear	kip	18.01	4.49	28.05	0.340	11.22
15.40	40.0	Flexure	kip-ft	325.50	105.30	365.51	0.408	13.46
15.40	40.0	Shear	kip	17.93	2.24	22.78	0.511	16.85
19.25	50.0	Flexure	kip-ft	325.50	109.62	373.79	0.388	12.80
19.25	50.0	Shear	kip	-17.93	0.00	-17.52	0.787	25.98
23.10	60.0	Flexure	kip-ft	325.50	105.30	365.51	0.408	13.46

23.10	60.0	Shear	kip	-17.93	-2.24	-22.78	0.511	16.85
26.95	70.0	Flexure	kip-ft	341.96	92.34	323.99	0.538	17.75
26.95	70.0	Shear	kip	-21.67	-4.49	-28.05	0.440	14.54
30.80	80.0	Flexure	kip-ft	325.50	70.48	256.55	0.712	23.49
30.80	80.0	Shear	kip	-24.68	-6.90	-33.32	0.371	12.23
34.65	90.0	Flexure	kip-ft	325.50	39.61	148.55	1.429	47.16
34.65	90.0	Shear	kip	-61.06	-9.14	-38.58	0.990	32.65
37.02	96.2	Flexure	kip-ft	277.16	16.30	61.87	3.193	105.35
37.02	96.2	Shear	kip	-89.01	-10.52	-41.83	1.395	46.03
37.38	97.1	Shear	kip	-94.28	-10.73	-42.32	1.470	48.50
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - Existing Deteriorated
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	127.58	0.00	0.00	99.000	3465.00
1.12	2.9	Shear	kip	94.16	10.73	44.34	1.401	49.03
1.48	3.8	Flexure	kip-ft	277.16	16.30	64.83	3.047	106.64
1.48	3.8	Shear	kip	89.01	10.52	43.83	1.331	46.60
3.85	10.0	Flexure	kip-ft	325.50	39.61	155.49	1.365	47.79
3.85	10.0	Shear	kip	54.81	9.14	40.39	0.826	28.92
7.70	20.0	Flexure	kip-ft	325.50	70.48	267.96	0.681	23.85
7.70	20.0	Shear	kip	23.34	6.90	34.80	0.325	11.39
11.55	30.0	Flexure	kip-ft	325.50	92.34	345.07	0.468	16.39
11.55	30.0	Shear	kip	17.93	4.49	29.21	0.324	11.35
15.40	40.0	Flexure	kip-ft	325.50	105.30	394.80	0.378	13.22
15.40	40.0	Shear	kip	17.93	2.24	23.63	0.492	17.24
19.25	50.0	Flexure	kip-ft	325.50	109.62	401.52	0.361	12.64
19.25	50.0	Shear	kip	-17.93	0.00	-18.04	0.765	26.76
23.10	60.0	Flexure	kip-ft	325.50	105.30	394.80	0.378	13.22
23.10	60.0	Shear	kip	-17.93	-2.24	-23.63	0.492	17.23
26.95	70.0	Flexure	kip-ft	341.96	92.34	345.07	0.505	17.67
26.95	70.0	Shear	kip	-20.25	-4.49	-29.21	0.386	13.50
30.80	80.0	Flexure	kip-ft	325.50	70.48	267.96	0.681	23.85

30.80	80.0	Shear	kip	-23.34	-6.90	-34.80	0.325	11.39
34.65	90.0	Flexure	kip-ft	325.50	39.61	155.49	1.365	47.79
34.65	90.0	Shear	kip	-54.81	-9.14	-40.39	0.826	28.92
37.02	96.2	Flexure	kip-ft	277.16	16.30	64.83	3.047	106.64
37.02	96.2	Shear	kip	-89.01	-10.52	-43.83	1.331	46.60
37.38	97.1	Shear	kip	-94.28	-10.73	-44.35	1.402	49.09
38.50	100.0	Flexure	kip-ft	102.41	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.

Bridge Name: Matheson Hmck Bridge over Matheson Hammock Canal
NBI Structure ID: 874294D
Bridge ID: 874294D

Analyzed By: BrR
Analyze Date: Wednesday, October 06, 2021 10:33:34
Analysis Engine: AASHTO LRFR Engine Version 6.8.4.3002
Analysis Preference Setting: None

Report By: BrR
Report Date: Wednesday, October 06, 2021 10:41:31

Structure Definition Name: INT Span 2 - PS Conc PSU
Member Name: G10
Member Alternative Name: 17"x36" INT PSU - w/ Conc. Repair + Post Tensioning

Report by Action: ☒ Flexure ☒ Concrete Stresses ☒ Shear ☒ Critical

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
HL-93 (US)
Truck + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.86	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	94.16	10.73	20.86	2.212	79.64	2.868	103.23
1.12	2.9	Shear	kip	445.93	-5.24	67.36	6.698	241.12	9.343	336.35
1.48	3.8	Flexure	kip-ft	293.46	16.30	30.61	5.099	183.55	6.609	237.94
1.48	3.8	Shear	kip	89.01	10.52	20.57	2.107	75.84	2.731	98.32
1.48	3.8	Shear	kip	436.13	4.78	85.59	5.040	181.43	7.371	265.36
1.48	3.8	Concrete Stresses	ksi	1.77	0.12	0.23	9.193	330.96		
3.85	10.0	Flexure	kip-ft	344.64	39.61	73.09	2.307	83.06	2.991	107.68
3.85	10.0	Shear	kip	70.05	9.14	18.70	1.791	64.49	2.322	83.60
3.85	10.0	Shear	kip	424.83	54.28	180.89	2.049	73.75	2.753	99.11
3.85	10.0	Concrete Stresses	ksi	1.77	0.29	0.54	3.451	124.23		
7.70	20.0	Flexure	kip-ft	344.64	70.48	124.85	1.174	42.27	1.522	54.79
7.70	20.0	Shear	kip	44.94	6.90	15.71	1.321	47.56	2.897	104.28
7.70	20.0	Shear	kip	424.83	93.06	265.36	1.250	45.01	1.664	59.89
7.70	20.0	Concrete Stresses	ksi	1.77	0.52	0.92	1.711	61.60		
11.55	30.0	Flexure	kip-ft	344.64	92.34	156.13	0.839	30.20	1.087	39.15
11.55	30.0	Shear	kip	30.63	4.49	12.85	1.112	40.04	2.168	78.03
11.55	30.0	Shear	kip	424.83	120.65	313.56	0.970	34.92	1.283	46.19
11.55	30.0	Concrete Stresses	ksi	1.77	0.68	1.15	1.193	42.96		
15.40	40.0	Flexure		344.64	105.30	172.00	0.708	25.48	0.917	33.03

			kip- ft							
15.40	40.0	Shear	kip	26.59	2.24	10.26	1.325	47.69	2.415	86.93
15.40	40.0	Shear	kip	424.83	135.52	336.40	0.860	30.96	1.138	40.96
15.40	40.0	Concrete Stresses	ksi	1.77	0.77	1.26	0.989	35.61		
19.25	50.0	Flexure	kip- ft	344.64	109.62	171.21	0.693	24.95	0.898	32.34
19.25	50.0	Shear	kip	-26.93	0.00	-7.73	1.990	71.66	3.511	126.41
19.25	50.0	Shear	kip	424.83	137.84	329.53	0.871	31.35	1.120	40.33
19.25	50.0	Concrete Stresses	ksi	1.77	0.81	1.26	0.962	34.63		
23.10	60.0	Flexure	kip- ft	344.64	105.30	172.00	0.708	25.48	0.917	33.03
23.10	60.0	Shear	kip	-26.59	-2.24	-10.26	1.325	47.69	2.415	86.93
23.10	60.0	Shear	kip	424.83	135.52	336.40	0.860	30.96	1.138	40.96
23.10	60.0	Concrete Stresses	ksi	1.77	0.77	1.26	0.989	35.61		
26.95	70.0	Flexure	kip- ft	362.07	92.34	156.13	0.903	32.50	1.170	42.13
26.95	70.0	Shear	kip	-34.86	-4.49	-12.85	1.300	46.81	2.412	86.83
26.95	70.0	Shear	kip	441.60	118.83	312.68	1.032	37.16	1.367	49.23
26.95	70.0	Concrete Stresses	ksi	1.77	0.68	1.15	1.193	42.96		
30.80	80.0	Flexure	kip- ft	344.64	70.48	124.85	1.174	42.27	1.522	54.79
30.80	80.0	Shear	kip	-44.94	-6.90	-15.71	1.321	47.56	2.897	104.28
30.80	80.0	Shear	kip	424.83	93.06	265.36	1.250	45.01	1.664	59.89
30.80	80.0	Concrete Stresses	ksi	1.77	0.52	0.92	1.711	61.60		
34.65	90.0	Flexure	kip-ft	344.64	39.61	73.09	2.307	83.06	2.991	107.68
34.65	90.0	Shear	kip	-70.05	-9.14	-18.70	1.791	64.49	2.322	83.60
34.65	90.0	Shear	kip	424.83	54.28	180.89	2.049	73.75	2.753	99.11
34.65	90.0	Concrete Stresses	ksi	1.77	0.29	0.54	3.451	124.23		
37.02	96.2	Flexure	kip-ft	293.46	16.30	30.61	5.099	183.56	6.610	237.94
37.02	96.2	Shear	kip	-89.01	-10.52	-20.57	2.107	75.84	2.731	98.32
37.02	96.2	Shear	kip	436.13	4.78	85.59	5.040	181.43	7.371	265.36
37.02	96.2	Concrete Stresses	ksi	1.77	0.12	0.23	9.193	330.97		
37.38	97.1	Shear	kip	-94.28	-10.73	-20.86	2.215	79.73	2.871	103.36
37.38	97.1	Shear	kip	446.33	-5.46	66.97	6.747	242.88	9.399	338.38
38.50	100.0	Flexure	kip- ft	108.44	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	0.86	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
HL-93 (US)
Tandem + Lane
Impact: With Impact
Lane: Single Lane

Span 2

							Inventory Rating	Inventory Load Rating	Operating Rating	Operating Load Rating
Location										
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3564.00	99.000	3564.00
0.00	0.0	Concrete Stresses	ksi	0.86	-0.00	0.00	99.000	3564.00		
1.12	2.9	Shear	kip	94.16	10.73	18.64	2.475	89.11	3.209	115.51
1.12	2.9	Shear	kip	445.93	-3.06	57.34	7.831	281.92	10.728	386.19
1.48	3.8	Flexure	kip-ft	293.46	16.30	27.43	5.689	204.81	7.375	265.49
1.48	3.8	Shear	kip	89.01	10.52	18.43	2.352	84.68	3.049	109.77
1.48	3.8	Shear	kip	436.13	4.78	72.19	5.975	215.10	8.391	302.09
1.48	3.8	Concrete Stresses	ksi	1.77	0.12	0.20	10.258	369.29		
3.85	10.0	Flexure	kip-ft	344.64	39.61	66.60	2.532	91.16	3.282	118.17
3.85	10.0	Shear	kip	70.05	9.14	17.02	1.969	70.88	2.552	91.88
3.85	10.0	Shear	kip	424.83	54.28	162.82	2.276	81.93	3.071	110.55
3.85	10.0	Concrete Stresses	ksi	1.77	0.29	0.49	3.787	136.33		
7.70	20.0	Flexure	kip-ft	344.64	70.48	117.65	1.246	44.86	1.615	58.15
7.70	20.0	Shear	kip	49.78	6.90	14.77	1.592	57.31	3.080	110.88
7.70	20.0	Shear	kip	424.83	92.32	249.52	1.333	47.98	1.778	64.00
7.70	20.0	Concrete Stresses	ksi	1.77	0.52	0.86	1.816	65.37		
11.55	30.0	Flexure	kip-ft	344.64	92.34	153.13	0.855	30.79	1.109	39.92
11.55	30.0	Shear	kip	31.38	4.49	12.60	1.169	42.09	2.286	82.29
11.55	30.0	Shear	kip	424.83	120.44	307.44	0.990	35.64	1.311	47.21
11.55	30.0	Concrete Stresses	ksi	1.77	0.68	1.13	1.217	43.80		
15.40	40.0	Flexure	kip-ft	344.64	105.30	173.06	0.703	25.32	0.912	32.82
15.40	40.0	Shear	kip	26.38	2.24	10.48	1.285	46.27	2.342	84.31

15.40	40.0	Shear	kip	424.83	135.61	338.85	0.854	30.73	1.130	40.67
15.40	40.0	Concrete Stresses	ksi	1.77	0.77	1.27	0.983	35.39		
19.25	50.0	Flexure	kip-ft	344.64	109.62	177.43	0.669	24.07	0.867	31.20
19.25	50.0	Shear	kip	-25.78	0.00	-8.43	1.748	62.93	3.074	110.67
19.25	50.0	Shear	kip	424.83	138.07	342.40	0.838	30.15	1.082	38.96
19.25	50.0	Concrete Stresses	ksi	1.77	0.81	1.30	0.928	33.42		
23.10	60.0	Flexure	kip-ft	344.64	105.30	173.06	0.703	25.32	0.912	32.82
23.10	60.0	Shear	kip	-26.38	-2.24	-10.48	1.285	46.27	2.342	84.31
23.10	60.0	Shear	kip	424.83	135.61	338.85	0.854	30.73	1.130	40.67
23.10	60.0	Concrete Stresses	ksi	1.77	0.77	1.27	0.983	35.39		
26.95	70.0	Flexure	kip-ft	362.07	92.34	153.13	0.920	33.13	1.193	42.95
26.95	70.0	Shear	kip	-35.63	-4.49	-12.60	1.362	49.04	2.533	91.17
26.95	70.0	Shear	kip	441.60	118.62	306.50	1.054	37.94	1.398	50.31
26.95	70.0	Concrete Stresses	ksi	1.77	0.68	1.13	1.217	43.80		
30.80	80.0	Flexure	kip-ft	344.64	70.48	117.65	1.246	44.86	1.615	58.15
30.80	80.0	Shear	kip	-49.78	-6.90	-14.77	1.592	57.31	3.080	110.88
30.80	80.0	Shear	kip	424.83	92.32	249.52	1.333	47.98	1.778	64.00
30.80	80.0	Concrete Stresses	ksi	1.77	0.52	0.86	1.816	65.37		
34.65	90.0	Flexure	kip-ft	344.64	39.61	66.60	2.532	91.16	3.282	118.17
34.65	90.0	Shear	kip	-70.05	-9.14	-17.02	1.969	70.88	2.552	91.88
34.65	90.0	Shear	kip	424.83	54.28	162.82	2.276	81.93	3.071	110.55
34.65	90.0	Concrete Stresses	ksi	1.77	0.29	0.49	3.787	136.33		
37.02	96.2	Flexure	kip-ft	293.46	16.30	27.43	5.689	204.81	7.375	265.49
37.02	96.2	Shear	kip	-89.01	-10.52	-18.43	2.352	84.68	3.049	109.77
37.02	96.2	Shear	kip	436.13	4.78	72.19	5.975	215.10	8.391	302.09
37.02	96.2	Concrete Stresses	ksi	1.77	0.12	0.20	10.258	369.29		
37.38	97.1	Shear	kip	-94.28	-10.73	-18.65	2.478	89.22	3.212	115.65
37.38	97.1	Shear	kip	446.33	-3.18	57.07	7.877	283.57	10.795	388.61
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3564.00	99.000	3564.00
38.50	100.0	Concrete Stresses	ksi	0.86	0.00	0.00	99.000	3564.00		

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning

C 3
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	2772.00
1.12	2.9	Shear	kip	94.16	10.73	11.45	5.424	151.88
1.12	2.9	Shear	kip	445.93	14.71	18.70	23.057	645.59
1.48	3.8	Flexure	kip-ft	293.46	16.30	16.68	12.596	352.68
1.48	3.8	Shear	kip	89.01	10.52	11.27	5.175	144.91
1.48	3.8	Shear	kip	436.13	19.99	24.38	17.070	477.97
3.85	10.0	Flexure	kip-ft	344.64	39.61	38.88	5.839	163.49
3.85	10.0	Shear	kip	70.05	9.14	10.10	4.465	125.03
3.85	10.0	Shear	kip	424.83	54.28	58.80	6.302	176.46
7.70	20.0	Flexure	kip-ft	344.64	70.48	63.23	3.121	87.39
7.70	20.0	Shear	kip	70.05	6.90	8.21	5.755	161.13
7.70	20.0	Shear	kip	424.83	92.25	90.04	3.694	103.43
11.55	30.0	Flexure	kip-ft	344.64	92.34	81.45	2.165	60.61
11.55	30.0	Shear	kip	70.05	4.49	7.05	7.029	196.82
11.55	30.0	Shear	kip	424.83	119.98	116.90	2.608	73.02
15.40	40.0	Flexure	kip-ft	344.64	105.30	91.86	1.784	49.94
15.40	40.0	Shear	kip	70.05	2.24	5.89	8.778	245.79
15.40	40.0	Shear	kip	424.83	136.02	132.69	2.176	60.94
19.25	50.0	Flexure	kip-ft	344.64	109.62	91.12	1.753	49.08
19.25	50.0	Shear	kip	70.05	0.00	4.73	11.384	318.75
19.25	50.0	Shear	kip	424.83	140.50	132.96	2.139	59.88
23.10	60.0	Flexure	kip-ft	344.64	105.30	91.86	1.784	49.94
23.10	60.0	Shear	kip	-70.05	-2.24	-5.89	8.778	245.79
23.10	60.0	Shear	kip	424.83	136.02	132.69	2.177	60.94
26.95	70.0	Flexure	kip-ft	362.07	92.34	81.45	2.329	65.22
26.95	70.0	Shear	kip	-70.42	-4.49	-7.05	7.069	197.94
26.95	70.0	Shear	kip	441.60	119.34	116.31	2.771	77.58
30.80	80.0	Flexure	kip-ft	344.64	70.48	63.23	3.121	87.39
30.80	80.0	Shear	kip	-70.05	-6.90	-8.21	5.755	161.13
30.80	80.0	Shear	kip	424.83	92.25	90.04	3.694	103.43
34.65	90.0	Flexure	kip-ft	344.64	39.61	38.88	5.839	163.49
34.65	90.0	Shear	kip	-70.05	-9.14	-10.10	4.465	125.03
34.65	90.0	Shear	kip	424.83	54.28	58.80	6.302	176.46

37.02	96.2	Flexure	kip-ft	293.46	16.30	16.68	12.596	352.68
37.02	96.2	Shear	kip	-89.01	-10.52	-11.27	5.175	144.91
37.02	96.2	Shear	kip	436.13	19.99	24.38	17.071	477.98
37.38	97.1	Shear	kip	-94.28	-10.73	-11.45	5.430	152.05
37.38	97.1	Shear	kip	446.33	14.60	18.58	23.237	650.64
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	2772.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
C 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3628.35
1.12	2.9	Shear	kip	94.16	10.73	16.06	3.868	141.77
1.12	2.9	Shear	kip	445.93	8.71	31.65	13.814	506.27
1.48	3.8	Flexure	kip-ft	293.46	16.30	23.41	8.973	328.87
1.48	3.8	Shear	kip	89.01	10.52	15.83	3.687	135.12
1.48	3.8	Shear	kip	436.13	14.06	39.54	10.674	391.20
3.85	10.0	Flexure	kip-ft	344.64	39.61	55.34	4.102	150.34
3.85	10.0	Shear	kip	70.05	9.14	14.37	3.137	114.97
3.85	10.0	Shear	kip	424.83	54.28	92.85	3.991	146.27
7.70	20.0	Flexure	kip-ft	344.64	70.48	93.36	2.114	77.47
7.70	20.0	Shear	kip	70.05	6.90	12.12	3.897	142.84
7.70	20.0	Shear	kip	424.83	89.96	139.88	2.394	87.74
11.55	30.0	Flexure	kip-ft	344.64	92.34	114.05	1.546	56.66
11.55	30.0	Shear	kip	70.05	4.49	9.87	5.020	183.98
11.55	30.0	Shear	kip	424.83	116.31	165.94	1.859	68.14
15.40	40.0	Flexure	kip-ft	344.64	105.30	126.11	1.299	47.62
15.40	40.0	Shear	kip	59.28	2.24	8.19	5.304	194.41
15.40	40.0	Shear	kip	424.83	133.38	182.99	1.593	58.37
19.25	50.0	Flexure	kip-ft	344.64	109.62	128.76	1.240	45.46
19.25	50.0	Shear	kip	-57.11	0.00	-6.69	6.568	240.71
19.25	50.0	Shear	kip	424.83	138.44	187.41	1.528	56.01
23.10	60.0	Flexure	kip-ft	344.64	105.30	126.11	1.299	47.62
23.10	60.0	Shear	kip	-59.28	-2.24	-8.19	5.304	194.41
23.10	60.0	Shear	kip	424.83	133.38	182.99	1.593	58.37

26.95	70.0	Flexure	kip-ft	362.07	92.34	114.05	1.664	60.97
26.95	70.0	Shear	kip	-70.42	-4.49	-9.87	5.049	185.03
26.95	70.0	Shear	kip	441.60	115.66	165.11	1.974	72.35
30.80	80.0	Flexure	kip-ft	344.64	70.48	93.36	2.114	77.47
30.80	80.0	Shear	kip	-70.05	-6.90	-12.12	3.897	142.84
30.80	80.0	Shear	kip	424.83	89.96	139.88	2.394	87.74
34.65	90.0	Flexure	kip-ft	344.64	39.61	55.34	4.102	150.34
34.65	90.0	Shear	kip	-70.05	-9.14	-14.37	3.137	114.97
34.65	90.0	Shear	kip	424.83	54.28	92.85	3.991	146.27
37.02	96.2	Flexure	kip-ft	293.46	16.30	23.41	8.973	328.87
37.02	96.2	Shear	kip	-89.01	-10.52	-15.83	3.687	135.12
37.02	96.2	Shear	kip	436.13	14.06	39.54	10.674	391.21
37.38	97.1	Shear	kip	-94.28	-10.73	-16.06	3.873	141.93
37.38	97.1	Shear	kip	446.33	8.60	31.48	13.905	509.61
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3628.35

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
C 5

Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	94.16	10.73	16.08	3.863	154.53
1.12	2.9	Shear	kip	445.93	8.69	31.72	13.785	551.38
1.48	3.8	Flexure	kip-ft	293.46	16.30	23.46	8.956	358.24
1.48	3.8	Shear	kip	89.01	10.52	15.86	3.680	147.19
1.48	3.8	Shear	kip	436.13	14.02	39.64	10.648	425.91
3.85	10.0	Flexure	kip-ft	344.64	39.61	55.39	4.099	163.94
3.85	10.0	Shear	kip	70.05	9.14	14.39	3.134	125.37
3.85	10.0	Shear	kip	424.83	54.28	92.95	3.987	159.47
7.70	20.0	Flexure	kip-ft	344.64	70.48	92.41	2.136	85.42
7.70	20.0	Shear	kip	70.05	6.90	12.00	3.938	157.50
7.70	20.0	Shear	kip	424.83	89.96	138.23	2.423	96.90
11.55	30.0	Flexure	kip-ft	344.64	92.34	114.81	1.536	61.43
11.55	30.0	Shear	kip	70.05	4.49	9.94	4.987	199.46
11.55	30.0	Shear	kip	424.83	116.22	167.09	1.847	73.88

15.40	40.0	Flexure	kip-ft	344.64	105.30	128.28	1.277	51.09
15.40	40.0	Shear	kip	57.66	2.24	8.24	5.123	204.94
15.40	40.0	Shear	kip	424.83	133.39	186.01	1.567	62.67
19.25	50.0	Flexure	kip-ft	344.64	109.62	132.83	1.202	48.09
19.25	50.0	Shear	kip	-54.70	0.00	-6.32	6.658	266.30
19.25	50.0	Shear	kip	424.83	139.00	192.50	1.485	59.39
23.10	60.0	Flexure	kip-ft	344.64	105.30	128.28	1.277	51.09
23.10	60.0	Shear	kip	-57.66	-2.24	-8.24	5.123	204.94
23.10	60.0	Shear	kip	424.83	133.39	186.01	1.567	62.67
26.95	70.0	Flexure	kip-ft	362.07	92.34	114.81	1.652	66.10
26.95	70.0	Shear	kip	-70.42	-4.49	-9.94	5.015	200.60
26.95	70.0	Shear	kip	441.60	115.57	166.25	1.961	78.44
30.80	80.0	Flexure	kip-ft	344.64	70.48	92.41	2.136	85.42
30.80	80.0	Shear	kip	-70.05	-6.90	-12.00	3.938	157.50
30.80	80.0	Shear	kip	424.83	89.96	138.23	2.423	96.90
34.65	90.0	Flexure	kip-ft	344.64	39.61	55.39	4.099	163.94
34.65	90.0	Shear	kip	-70.05	-9.14	-14.39	3.134	125.37
34.65	90.0	Shear	kip	424.83	54.28	92.95	3.987	159.47
37.02	96.2	Flexure	kip-ft	293.46	16.30	23.46	8.956	358.24
37.02	96.2	Shear	kip	-89.01	-10.52	-15.86	3.680	147.19
37.02	96.2	Shear	kip	436.13	14.02	39.64	10.648	425.91
37.38	97.1	Shear	kip	-94.28	-10.73	-16.08	3.868	154.72
37.38	97.1	Shear	kip	446.33	8.57	31.55	13.876	555.03
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
FL120 Span < 200ft
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Permit	Permit
Location							Rating	Load
(ft)	Percent	Limit	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	5940.00
1.12	2.9	Shear	kip	445.93	0.11	50.24	8.873	532.40
1.48	3.8	Flexure	kip-ft	293.46	16.30	35.85	6.347	380.83
1.48	3.8	Shear	kip	436.13	5.52	61.36	7.018	421.08
3.85	10.0	Flexure	kip-ft	344.64	39.61	85.33	2.882	172.94
3.85	10.0	Shear	kip	424.83	54.28	141.29	2.623	157.36

7.70	20.0	Flexure	kip-ft	344.64	70.48	144.69	1.478	88.65
7.70	20.0	Shear	kip	424.83	89.96	209.42	1.599	95.94
11.55	30.0	Flexure	kip-ft	344.64	92.34	179.27	1.065	63.93
11.55	30.0	Shear	kip	424.83	117.79	246.37	1.246	74.78
15.40	40.0	Flexure	kip-ft	344.64	105.30	196.07	0.905	54.32
15.40	40.0	Shear	kip	424.83	132.33	262.21	1.116	66.93
19.25	50.0	Flexure	kip-ft	344.64	109.62	193.35	0.895	53.69
19.25	50.0	Shear	kip	424.83	137.71	257.32	1.116	66.95
23.10	60.0	Flexure	kip-ft	344.64	105.30	196.07	0.905	54.32
23.10	60.0	Shear	kip	424.83	132.33	262.21	1.116	66.93
26.95	70.0	Flexure	kip-ft	362.07	92.34	179.27	1.146	68.79
26.95	70.0	Shear	kip	441.60	116.18	245.09	1.328	79.67
30.80	80.0	Flexure	kip-ft	344.64	70.48	144.69	1.478	88.65
30.80	80.0	Shear	kip	424.83	89.96	209.42	1.599	95.94
34.65	90.0	Flexure	kip-ft	344.64	39.61	85.33	2.882	172.94
34.65	90.0	Shear	kip	424.83	54.28	141.29	2.623	157.36
37.02	96.2	Flexure	kip-ft	293.46	16.30	35.85	6.347	380.83
37.02	96.2	Shear	kip	436.13	5.52	61.36	7.018	421.09
37.38	97.1	Shear	kip	446.33	-0.01	50.00	8.926	535.58
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	5940.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
ST 5
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3960.00
1.12	2.9	Shear	kip	94.16	10.73	14.69	4.229	169.18
1.12	2.9	Shear	kip	445.93	10.50	27.85	15.637	625.49
1.48	3.8	Flexure	kip-ft	293.46	16.30	21.47	9.784	391.34
1.48	3.8	Shear	kip	89.01	10.52	14.52	4.020	160.79
1.48	3.8	Shear	kip	436.13	15.76	35.17	11.951	478.03
3.85	10.0	Flexure	kip-ft	344.64	39.61	51.52	4.406	176.26
3.85	10.0	Shear	kip	70.05	9.14	13.38	3.370	134.79
3.85	10.0	Shear	kip	424.83	54.28	84.94	4.363	174.50
7.70	20.0	Flexure	kip-ft	344.64	70.48	88.86	2.221	88.83

7.70	20.0	Shear	kip	70.05	6.90	11.54	4.094	163.78
7.70	20.0	Shear	kip	424.83	89.96	132.11	2.535	101.39
11.55	30.0	Flexure	kip-ft	344.64	92.34	112.03	1.574	62.95
11.55	30.0	Shear	kip	70.05	4.49	9.70	5.110	204.41
11.55	30.0	Shear	kip	424.83	116.53	162.91	1.893	75.70
15.40	40.0	Flexure	kip-ft	344.64	105.30	125.93	1.301	52.05
15.40	40.0	Shear	kip	59.67	2.24	7.86	5.566	222.66
15.40	40.0	Shear	kip	424.83	133.78	182.35	1.596	63.85
19.25	50.0	Flexure	kip-ft	344.64	109.62	128.11	1.247	49.86
19.25	50.0	Shear	kip	-58.06	0.00	-6.02	7.422	296.87
19.25	50.0	Shear	kip	424.83	139.22	185.71	1.538	61.52
23.10	60.0	Flexure	kip-ft	344.64	105.30	125.93	1.301	52.05
23.10	60.0	Shear	kip	-59.67	-2.24	-7.86	5.566	222.66
23.10	60.0	Shear	kip	424.83	133.78	182.35	1.596	63.85
26.95	70.0	Flexure	kip-ft	362.07	92.34	112.03	1.694	67.74
26.95	70.0	Shear	kip	-70.42	-4.49	-9.70	5.140	205.58
26.95	70.0	Shear	kip	441.60	115.89	162.09	2.009	80.38
30.80	80.0	Flexure	kip-ft	344.64	70.48	88.86	2.221	88.83
30.80	80.0	Shear	kip	-70.05	-6.90	-11.54	4.094	163.78
30.80	80.0	Shear	kip	424.83	89.96	132.11	2.535	101.39
34.65	90.0	Flexure	kip-ft	344.64	39.61	51.52	4.406	176.26
34.65	90.0	Shear	kip	-70.05	-9.14	-13.38	3.370	134.79
34.65	90.0	Shear	kip	424.83	54.28	84.94	4.363	174.50
37.02	96.2	Flexure	kip-ft	293.46	16.30	21.47	9.784	391.35
37.02	96.2	Shear	kip	-89.01	-10.52	-14.52	4.020	160.79
37.02	96.2	Shear	kip	436.13	15.76	35.17	11.951	478.03
37.38	97.1	Shear	kip	-94.28	-10.73	-14.69	4.235	169.38
37.38	97.1	Shear	kip	446.33	10.39	27.69	15.745	629.81
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3960.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
SU 2
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
Location							Rating	Load Rating
(ft)	Percent	Limit State	Units	Capacity	DL + Adj-LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	1683.00

1.12	2.9	Shear	kip	94.16	10.73	9.87	6.291	106.96
1.12	2.9	Shear	kip	445.93	16.77	14.32	29.967	509.43
1.48	3.8	Flexure	kip-ft	293.46	16.30	14.44	14.543	247.23
1.48	3.8	Shear	kip	89.01	10.52	9.77	5.975	101.58
1.48	3.8	Shear	kip	436.13	21.95	19.35	21.406	363.90
3.85	10.0	Flexure	kip-ft	344.64	39.61	34.85	6.515	110.75
3.85	10.0	Shear	kip	70.05	9.14	9.05	4.982	84.70
3.85	10.0	Shear	kip	424.83	54.28	50.46	7.344	124.85
7.70	20.0	Flexure	kip-ft	344.64	70.48	60.77	3.247	55.20
7.70	20.0	Shear	kip	70.05	6.90	7.89	5.987	101.78
7.70	20.0	Shear	kip	424.83	92.66	86.20	3.853	65.51
11.55	30.0	Flexure	kip-ft	344.64	92.34	77.77	2.267	38.54
11.55	30.0	Shear	kip	70.05	4.49	6.73	7.362	125.15
11.55	30.0	Shear	kip	424.83	120.40	111.36	2.734	46.47
15.40	40.0	Flexure	kip-ft	344.64	105.30	85.84	1.909	32.45
15.40	40.0	Shear	kip	70.05	2.24	5.57	9.280	157.76
15.40	40.0	Shear	kip	424.83	136.44	123.89	2.328	39.57
19.25	50.0	Flexure	kip-ft	344.64	109.62	84.98	1.879	31.95
19.25	50.0	Shear	kip	70.05	0.00	4.41	12.206	207.50
19.25	50.0	Shear	kip	424.83	140.92	124.00	2.290	38.92
23.10	60.0	Flexure	kip-ft	344.64	105.30	85.84	1.909	32.45
23.10	60.0	Shear	kip	-70.05	-2.24	-5.57	9.280	157.76
23.10	60.0	Shear	kip	424.83	136.44	123.89	2.328	39.57
26.95	70.0	Flexure	kip-ft	362.07	92.34	77.77	2.440	41.47
26.95	70.0	Shear	kip	-70.42	-4.49	-6.73	7.404	125.87
26.95	70.0	Shear	kip	441.60	119.75	110.79	2.905	49.38
30.80	80.0	Flexure	kip-ft	344.64	70.48	60.77	3.247	55.20
30.80	80.0	Shear	kip	-70.05	-6.90	-7.89	5.987	101.78
30.80	80.0	Shear	kip	424.83	92.66	86.20	3.853	65.51
34.65	90.0	Flexure	kip-ft	344.64	39.61	34.85	6.515	110.75
34.65	90.0	Shear	kip	-70.05	-9.14	-9.05	4.982	84.69
34.65	90.0	Shear	kip	424.83	54.28	50.46	7.344	124.85
37.02	96.2	Flexure	kip-ft	293.46	16.30	14.44	14.543	247.23
37.02	96.2	Shear	kip	-89.01	-10.52	-9.77	5.975	101.58
37.02	96.2	Shear	kip	436.13	21.95	19.35	21.406	363.90
37.38	97.1	Shear	kip	-94.28	-10.73	-9.87	6.299	107.09
37.38	97.1	Shear	kip	446.33	16.66	14.21	30.232	513.94
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	1683.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
SU 3
Axle Load
Impact: With Impact

Lane: Single Lane

Span 2

							Legal Rating	Legal Load Rating
Location								
(ft)	Percent	Limit State	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3267.00
1.12	2.9	Shear	kip	94.16	10.73	18.08	3.436	113.37
1.12	2.9	Shear	kip	445.93	6.08	37.39	11.765	388.24
1.48	3.8	Flexure	kip-ft	293.46	16.30	26.43	7.947	262.24
1.48	3.8	Shear	kip	89.01	10.52	17.87	3.265	107.75
1.48	3.8	Shear	kip	436.13	11.39	46.35	9.163	302.38
3.85	10.0	Flexure	kip-ft	344.64	39.61	63.47	3.577	118.04
3.85	10.0	Shear	kip	70.05	9.14	16.49	2.735	90.27
3.85	10.0	Shear	kip	424.83	54.28	109.65	3.379	111.52
7.70	20.0	Flexure	kip-ft	344.64	70.48	109.61	1.800	59.41
7.70	20.0	Shear	kip	70.05	6.90	14.24	3.319	109.54
7.70	20.0	Shear	kip	424.83	89.96	168.00	1.993	65.78
11.55	30.0	Flexure	kip-ft	344.64	92.34	138.43	1.274	42.03
11.55	30.0	Shear	kip	55.12	4.49	11.98	3.177	104.85
11.55	30.0	Shear	kip	424.83	115.19	202.93	1.526	50.35
15.40	40.0	Flexure	kip-ft	344.64	105.30	156.17	1.049	34.63
15.40	40.0	Shear	kip	43.05	2.24	9.73	3.180	104.94
15.40	40.0	Shear	kip	424.83	132.50	225.69	1.295	42.74
19.25	50.0	Flexure	kip-ft	344.64	109.62	159.70	1.000	33.00
19.25	50.0	Shear	kip	-41.98	0.00	-7.48	4.315	142.38
19.25	50.0	Shear	kip	424.83	138.48	230.42	1.243	41.01
23.10	60.0	Flexure	kip-ft	344.64	105.30	156.17	1.049	34.63
23.10	60.0	Shear	kip	-43.05	-2.24	-9.73	3.180	104.94
23.10	60.0	Shear	kip	424.83	132.50	225.69	1.295	42.74
26.95	70.0	Flexure	kip-ft	362.07	92.34	138.43	1.371	45.23
26.95	70.0	Shear	kip	-58.59	-4.49	-11.98	3.401	112.22
26.95	70.0	Shear	kip	441.60	113.94	201.66	1.625	53.62
30.80	80.0	Flexure	kip-ft	344.64	70.48	109.61	1.800	59.41
30.80	80.0	Shear	kip	-70.05	-6.90	-14.24	3.319	109.54
30.80	80.0	Shear	kip	424.83	89.96	168.00	1.993	65.78
34.65	90.0	Flexure	kip-ft	344.64	39.61	63.47	3.577	118.04
34.65	90.0	Shear	kip	-70.05	-9.14	-16.49	2.735	90.27
34.65	90.0	Shear	kip	424.83	54.28	109.65	3.379	111.52
37.02	96.2	Flexure	kip-ft	293.46	16.30	26.43	7.947	262.24
37.02	96.2	Shear	kip	-89.01	-10.52	-17.87	3.265	107.75
37.02	96.2	Shear	kip	436.13	11.39	46.35	9.163	302.38

37.38	97.1	Shear	kip	-94.28	-10.73	-18.08	3.440	113.51
37.38	97.1	Shear	kip	446.33	5.96	37.19	11.840	390.72
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3267.00

Detailed Rating Results
17"x36" INT PSU - w/ Conc. Repair + Post Tensioning
SU 4
Axle Load
Impact: With Impact
Lane: Single Lane

Span 2

							Legal	Legal
							Rating	Load
Location								Rating
(ft)	Percent	Limit	Units	Capacity	DL + Adj- LL*	LL	Factor	(Ton)
0.00	0.0	Flexure	kip-ft	135.08	0.00	0.00	99.000	3465.00
1.12	2.9	Shear	kip	94.16	10.73	18.94	3.279	114.75
1.12	2.9	Shear	kip	445.93	4.95	39.82	11.074	387.60
1.48	3.8	Flexure	kip-ft	293.46	16.30	27.70	7.584	265.45
1.48	3.8	Shear	kip	89.01	10.52	18.72	3.116	109.07
1.48	3.8	Shear	kip	436.13	10.28	49.20	8.656	302.96
3.85	10.0	Flexure	kip-ft	344.64	39.61	66.43	3.417	119.61
3.85	10.0	Shear	kip	70.05	9.14	17.26	2.613	91.47
3.85	10.0	Shear	kip	424.83	54.28	115.78	3.200	112.02
7.70	20.0	Flexure	kip-ft	344.64	70.48	114.49	1.724	60.33
7.70	20.0	Shear	kip	70.05	6.90	14.87	3.178	111.23
7.70	20.0	Shear	kip	424.83	89.96	176.43	1.898	66.43
11.55	30.0	Flexure	kip-ft	344.64	92.34	147.43	1.196	41.86
11.55	30.0	Shear	kip	49.78	4.49	12.48	2.722	95.28
11.55	30.0	Shear	kip	424.83	116.12	216.90	1.423	49.81
15.40	40.0	Flexure	kip-ft	344.64	105.30	168.68	0.971	34.00
15.40	40.0	Shear	kip	38.99	2.24	10.10	2.757	96.49
15.40	40.0	Shear	kip	424.83	132.50	243.11	1.202	42.09
19.25	50.0	Flexure	kip-ft	344.64	109.62	171.55	0.931	32.58
19.25	50.0	Shear	kip	-38.35	0.00	-7.71	3.827	133.94
19.25	50.0	Shear	kip	424.83	138.59	246.79	1.160	40.60
23.10	60.0	Flexure	kip-ft	344.64	105.30	168.68	0.971	34.00
23.10	60.0	Shear	kip	-38.99	-2.24	-10.10	2.757	96.49
23.10	60.0	Shear	kip	424.83	132.50	243.11	1.202	42.09
26.95	70.0	Flexure	kip-ft	362.07	92.34	147.43	1.287	45.04
26.95	70.0	Shear	kip	-53.70	-4.49	-12.48	2.964	103.73
26.95	70.0	Shear	kip	441.60	114.73	215.57	1.516	53.07

30.80	80.0	Flexure	kip-ft	344.64	70.48	114.49	1.724	60.33
30.80	80.0	Shear	kip	-70.05	-6.90	-14.87	3.178	111.23
30.80	80.0	Shear	kip	424.83	89.96	176.43	1.898	66.43
34.65	90.0	Flexure	kip-ft	344.64	39.61	66.43	3.417	119.61
34.65	90.0	Shear	kip	-70.05	-9.14	-17.26	2.613	91.47
34.65	90.0	Shear	kip	424.83	54.28	115.78	3.200	112.02
37.02	96.2	Flexure	kip-ft	293.46	16.30	27.70	7.584	265.45
37.02	96.2	Shear	kip	-89.01	-10.52	-18.72	3.116	109.07
37.02	96.2	Shear	kip	436.13	10.28	49.20	8.656	302.96
37.38	97.1	Shear	kip	-94.28	-10.73	-18.95	3.283	114.89
37.38	97.1	Shear	kip	446.33	4.83	39.62	11.144	390.04
38.50	100.0	Flexure	kip-ft	108.44	0.00	0.00	99.000	3465.00

Note:

*Adj-LL is only applicable for Permit load rating.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Nov-21
Checked By: MP
Check Date: Nov-21

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD MOMENT & SHEAR REACTIONS (SPAN 2)

DEAD LOAD MOMENT REACTIONS FROM AASHTOWARE BrR (SPAN 2)								
	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	Total DC Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit (KIP-FT)
Location								
0	0	0	0	0	0	0	0	0.00
1.48	12.5	0.1	0.3	0.7	2.6	12.9	3.3	16.20
3.85	30.5	0.3	0.7	1.8	6.3	31.5	8.1	39.60
7.7	54.2	0.5	1.4	3.2	11.2	56.1	14.4	70.50
11.55	71.1	0.7	1.6	4.2	14.7	73.4	18.9	92.30
15.4	81.3	0.8	1.6	4.8	16.8	83.7	21.6	105.30
19.25	84.7	0.8	1.6	5	17.5	87.1	22.5	109.60
23.1	81.3	0.8	1.6	4.8	16.8	83.7	21.6	105.30
26.95	71.1	0.7	1.6	4.2	14.7	73.4	18.9	92.30
30.8	54.2	0.5	1.4	3.2	11.2	56.1	14.4	70.50
34.65	30.5	0.3	0.7	1.8	6.3	31.5	8.1	39.60
37.02	12.5	0.1	0.3	0.7	2.6	12.9	3.3	16.20
38.5	0	0	0	0	0	0	0	0.00

** Existing condition assumes the removal of 7 strands, and 1 exterior stirrup leg to account for the controlling deterioration along the bottom face of the slab units.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Nov-21
Checked By: MP
Check Date: Nov-21

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD MOMENT & SHEAR REACTIONS (SPAN 2)

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR (SPAN 2)								
	Self Weight (Slab Unit) (KIP)	% of DC Slab Unitx (KIP)	Self Weight (Interior diagrams) (KIP)	DC - Railing (KIP)	DC - Curb/ Sidewalk (KIP)	Total DC Selfweight of Slab Unit alone (per Slab Unit) (KIP)	Total DC (Railing + Sidewalk) per Slab Unit (KIP)	Total DC per Slab Unit (KIP)
Location								
0	8.8	0.09	0.49	0.52	1.82	9.38	2.34	11.72
1.48	8.12	0.08	0.16	0.48	1.68	8.36	2.16	10.52
3.85	7.04	0.07	0.16	0.41	1.45	7.27	1.86	9.13
7.7	5.28	0.05	0.16	0.31	1.09	5.49	1.4	6.89
11.55	3.52	0.04	0	0.21	0.73	3.56	0.94	4.50
15.4	1.76	0.02	0	0.1	0.36	1.78	0.46	2.24
19.25	0	0	0	0	0	0	0	0.00
23.1	-1.76	-0.02	0	-0.1	-0.36	-1.78	-0.46	-2.24
26.95	-3.52	-0.04	0	-0.21	-0.73	-3.56	-0.94	-4.50
30.8	-5.28	-0.05	-0.16	-0.31	-1.09	-5.49	-1.4	-6.89
34.65	-7.04	-0.07	-0.16	-0.41	-1.45	-7.27	-1.86	-9.13
37.02	-8.12	-0.08	-0.16	-0.48	-1.68	-8.36	-2.16	-10.52
38.5	-8.8	-0.09	-0.49	-0.52	-1.82	-9.38	-2.34	-11.72

** Existing condition assumes the removal of 7 strands, and 1 exterior stirrup leg to account for the controlling deterioration along the bottom face of the slab units.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DESIGN CAPACITY

LOAD RATING SUMMARY - CONTROLLING LEGAL LOAD (Assuming Post Tensioning)								
Span 2 - INTERIOR PSU-8 (LRFR) - SU4								
Location	Condition Factor	Unfactored DL Moment (kip-ft)	Unfactored SU4 Truck LL Moment (kip-ft)	Flexural Operating Rating Factor	Existing Flexural Capacity (kip-ft) **	Existing Shear Capacity (kip) **	Required Flexural Capacity (kip-ft) *	Required Shear Capacity (kip) *
0.00	0.90	0	0	99	135.08	-	-	-
1.12		-	-	-	-	94.16	-	-
1.48		16.30	27.70	7.58	293.46	89.01	-	-
3.85		39.61	66.43	3.42	344.64	70.05	-	-
7.7		70.48	114.49	1.72	344.64	70.05	-	-
11.55		92.34	147.43	1.20	344.64	49.78	-	-
15.4		105.30	168.68	0.97	344.64	38.99	359.34	-
19.25		109.62	171.55	0.93	344.64	-38.35	368.62	-
23.1		105.30	168.68	0.97	344.64	-38.99	359.34	-
26.95		92.34	147.43	1.29	362.07	-53.70	-	-
30.8		70.48	114.49	1.72	344.64	-70.05	-	-
34.65		39.61	66.43	3.42	344.64	-70.05	-	-
37.02		16.30	27.70	7.58	293.46	-89.01	-	-
37.39		-	-	-	-	-94.28	-	-
38.5		0.00	0.00	99.00	108.44	-	-	-

* Minimum Required capacity to meet a minimum Inventory Rating Factor of 1.1, conservatively.

** Existing condition assumes the removal of 7 strands, and 1 exterior stirrup leg to account for the controlling deterioration along the bottom face of the slab units.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Nov-21
Checked By: MP
Check Date: Nov-21

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DESIGN CAPACITY

Notes:

- 1) Gross Section Properties from AASHTOWare Bridge Rating Software:

PS Box Beam - Circular Void

Name:	17"x36" PSU	
Description:	17"x36" Prestressed Slab Unit (Typ.)	
Sl Or Us Type:	US Customary	
Box Beam Type:	Circular Void	
Top Width:	35.0000	in
Number Circular Voids:	2	
Three Void Box Shape Indicator:	FALSE	
Ctc Distance Voids:	16.0000	in
Void Diameter:	10.0000	in
Interior Void Diameter:		in
Exterior Void Diameter:		in
Depth:	17.0000	in
Distance To Cg Void Bot:	9.0000	in
Bot Width:	36.0000	in
Shear Key Vertical Loc:	2.0000	in
Shear Key Height:	6.0000	in
Shear Key Depth:	1.5000	in
Area:	438.822	in^2
Nominal Weight Or Mass:	457.107	lb/ft
Ixx:	13330.101	in^4
Distance Y To Cg:	8.1667	in
Sxx Top:	1509.078	in^3
Sxx Bot:	1632.246	in^3
Nominal Depth:	17.0000	in
Volume Surface Ratio:	3.175	in
Half Depth Area Pos Flex:		in^2
Half Depth Area Neg Flex:		in^2
St Venant Torsional Constant:	14593.772	in^4



Project #: D210107FL00.00
Designed By: YRA
Design Date: Nov-21
Checked By: MP
Check Date: Nov-21

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DESIGN CAPACITY

Concrete Material

Name:	Class P (5000)
Description:	Class 5000 cement concrete
Si Or Us Type:	US Customary
28 Day Compressive Strength:	5.000 ksi
Initial Compressive Strength:	4.000 ksi
Density For DL:	0.150 kcf
Density For Modulus Of Elasticity:	0.145 kcf
Std Modulus Of Elasticity:	4074.28 ksi
Std Initial Modulus Of Elasticity:	3644.15 ksi
Coefficient Of Thermal Expansion:	0.0000060000 1/F
Poissons Ratio:	0.200
Composition Type:	Normal
Modulus Of Rupture:	0.537 ksi
Shear Factor:	1.000



Project #: D210107FL00.00
Designed By: YRA
Design Date: Nov-21
Checked By: MP
Check Date: Nov-21

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DESIGN CAPACITY

Reinforcing Steel Material

Name: Grade 40
Description: 40 ksi reinforcing steel
Si Or Us Type: US Customary
Yield Strength: 40.000 ksi
Modulus Of Elasticity: 29000.00 ksi
Ultimate Strength: 70.000 ksi
Reinforcing Bar Type: Plain

Prestress Strand Material

Name: 7/16" (7W-250) SR
Description: Stress relieved 7/16"/Seven Wire/fpu = 250
Si Or Us Type: US Customary
Strand Diameter: 0.4375 in
Strand Area: 0.108 in^2
Strand Type: Stress Relieved
Ultimate Tensile Strength: 250.000 ksi
Yield Strength: 212.500 ksi
Modulus Of Elasticity: 28500.00 ksi
Transfer Length Std: 21.8750 in
Transfer Length LRPD: 26.2500 in
Unit Load Per Length: 0.367 lb/ft
Epoxy Coated Indicator: FALSE

2.0 SONOVOID SLAB UNIT STRENGTHENING - CFRP WRAPS EVALUATION

OBJECTIVE

Design of externally bonded Carbon FRP reinforcement in order to increase the Flexural Capacity of Sonovoid Slab Units 2-8 and 2-9, Bridge No.874294. Load rate CFRP strengthened slab units using LRFR Strength II for controlling FL-Legal Truck (SU4).

CODES AND SPECIFICATIONS

- "FDOT Bridge Load Rating Manual, "Florida Department of Transportation (FDOT) ", January 2021, FDOT BLRM , 2021 edition used for project consistency
- "FDOT Structures Design Guidelines (SDG). Structures Manual Vol.1", January 2021, FDOT
- "AASHTO LRFD Bridge Design Specifications, "American Association of State Highway and Transportation Officials (AASHTO), 9th Edition 2020
- "Fiber Reinforced Polymer Guidelines (FRPG). Structures Design Manual Vol.4", January 2021, FDOT
- "Guide for the Design and Construction of Externally Bonded FRP Systems for Strengthening Concrete Structures ", ACI 440.2R-08, ACI, 2008

Assumptions/Notes:

1. Assume all prestressing strands are bonded for flexural analysis
2. Calculations are an addendum to the AASHTOWare BrR Analysis
3. CFRP Strengthening will use the U-Wrap Method described in ([ACI 440.2R-08, Chapter 11](#)) and Flexural Strengthening analysis techniques in ([ACI 440.2R-08, Chapter 10](#))

Procedure:

1. Input Original Beam Geometry, Material Properties, Strength and Load Effects
2. AASHTOWARE BrR Refined Analysis Results Input
 - a. Moment
3. FRP Reinforcement Properties
4. Design of Externally Bonded FRP Reinforcement
 - a. Development Length of FRP
 - b. Flexural Capacity
 - c. Service Check
 - d. FRP Fatigue Check
5. Calculate Operating Ratings
6. Summary

Legend:

INPUT

<-----Data Input

OUTPUT

<-----Reference Checks and Design Results Output

INPUT DATA

Resistance factor for FRP (ACI 440.2R-08, Table 11.1)

$$\psi_f := 0.85$$

System Factor (FDOT BLRM Table 6A.4.2.4-1)

$$\phi_S := 1.0$$

Condition Factor for Shear (AASHTO MBE 6A.4.2.3)

$$\phi_C := 0.90$$

Load Factors per Table 6A.4.2.2-1 FDOT Load Rating Manual, January 2021

Load factor for Dead Load

$$\gamma_{DC} := 1.25$$

Load factor for Live Load - Inventory (1.75) and FL-120 (1.35)

$$\gamma_{INV} := 1.75$$

Load factor for Live Load - Operating

$$\gamma_{OPT} := 1.35$$

Load factor for Live Load - FL-120

$$\gamma_{FL120} := 1.35$$

Load factor for Live Load - Legal - Operating

$$\gamma_{FLSU_OPT} := 1.35$$

Material Properties

Concrete Information:

Correction factor for source of aggregate. (AASHTO 5.4.2.4-1. & FDOT SDG. 1.4.1-A)

$$K_1 := 1.0$$

Nominal compressive strength of concrete Slab Unit (non-composite).

$$f'_{c_bm} := 5.0 \cdot \text{ksi}$$

Slab Unit concrete strength at final (FDOT BLRM Table 6A.5.2.1-1)

$$f_c := 5.0 \text{ ksi}$$

Deck Slab concrete strength at final (FDOT BLRM Table 6A.5.2.1-1)

$$f_{cslab} := 0 \text{ ksi}$$

Weight of concrete and humidity (AASHTO Table 3.5.1-1 & FDOT SDG 1.4.1-A & 4.6.6)

$$w_c := 0.145 \frac{\text{kip}}{\text{ft}^3}$$

$$\text{Humidity} := 75$$

Modulus of elasticity for normalweight concrete Deck Slab. (AASHTO 5.4.2.4-2).

$$E_c := 120000 \cdot K_1 \cdot \left(w_c \cdot \frac{\text{ft}^3}{\text{kip}} \right)^{2.0} \cdot \left(f_{cslab} \cdot \frac{1}{\text{ksi}} \right)^{0.33} \cdot \text{ksi} = 0 \cdot \text{ksi}$$

Modulus of elasticity for normalweight concrete Slab Unit. (AASHTO 5.4.2.4-2).

$$E_{c_bm} := 120000 \cdot K_1 \cdot \left(w_c \cdot \frac{\text{ft}^3}{\text{kip}} \right)^{2.0} \cdot \left(f'_{c_bm} \cdot \frac{1}{\text{ksi}} \right)^{0.33} \cdot \text{ksi} = 4.291 \times 10^3 \cdot \text{ksi}$$

Modular Ratio
$$n_{trans} := \frac{E_c}{E_{c_bm}} = 0$$

Concrete cracking stress (AASHTO 5.4.2.6)
$$f_T := 0.24 \cdot \sqrt{\frac{f_c \cdot b_m}{ksi}} \cdot ksi = 0.537 \cdot ksi$$

Geometry Information:

Span length (CL bearing to CL bearing, Span 2)

$$L_{Span} := 38.50ft$$

(See Asbuilt Plans
PG. 8 of 13 of pdf)

Slab Section Properties - [Not Applicable to this Design]

Deck thickness (Assumed for Asphalt W.S.)

$$t_{slab} := 0in$$

Effective Deck Width

$$b_s := 0.0ft$$

Transformed Width

$$b_{transf} := n_{trans} \cdot b_s = 0 \cdot in$$

Height of the section (Slab Unit + Deck Slab)

$$h_c := 17in + t_{slab} = 17 \cdot in$$

Transformed Area

$$A_{ts} := t_{slab} \cdot b_{transf} = 0 \cdot in^2$$

Slab Unit Properties

Non-composite

(Tranformed) Composite

Slab Unit height

$$h_{nc} := 17in$$

$$h_c = 17 \cdot in$$

Size of Void

$$d_{void} := 10in$$

Bottom flange width

$$b_{f_bot} := 36in$$

Top flange width

$$b_{f_top} := 35in$$

Web width (assume effective web width)

$$b_w := b_{f_top} - 2 \cdot 1in - 2 \cdot \left(\frac{\pi \cdot d_{void}}{4} \right)$$

$$b_w = 17.292 \cdot in$$

Cross sectional area (From AASHTOWARE BrR)

$$A_{nc} := 438.822in^2$$

$$A_{ww} := A_{nc} + b_{transf} \cdot t_{slab}$$

$$A = 438.822 \cdot in^2$$

Moment of inertia

$$I_{nc} := 13330.101in^4$$

$$I := 13330.101in^4$$

C.G (from bottom)

$$y_{b_nc} := 8.1667in$$

$$y_b := 8.1667in$$

Top fiber to C.G.

$$y_{t_nc} := h_{nc} - y_{b_nc} = 8.833 \cdot in$$

$$y_t := h_c - y_b = 8.833 \cdot in$$

Section modulus at top fiber

$$S_{t_nc} := \frac{I_{nc}}{y_{t_nc}} = 1.509 \times 10^3 \cdot in^3$$

$$S_t := \frac{I}{y_t} = 1.509 \times 10^3 \cdot in^3$$

Section modulus at top of slab unit once section becomes composite

$$S_{top_girder_c} := \frac{I}{y_t - t_{slab}} = 1.509 \times 10^3 \cdot in^3$$

Section modulus at bottom fiber

$$S_{b_nc} := \frac{I_{nc}}{y_{b_nc}} = 1.632 \times 10^3 \cdot \text{in}^3 \quad S_b := \frac{I}{y_b} = 1.632 \times 10^3 \cdot \text{in}^3$$

Radius of gyration

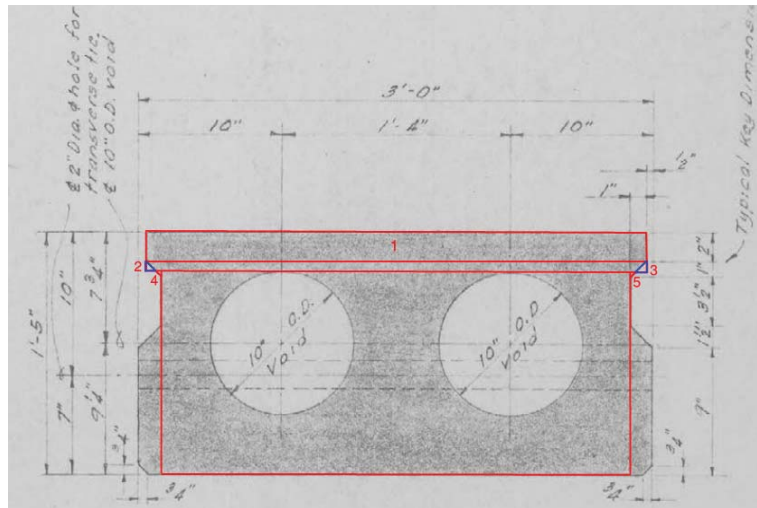
$$r := \sqrt{\frac{I_{nc}}{A_{nc}}} = 5.512 \cdot \text{in}$$

▣ Slab Unit/Girder Dimensions (For Nominal Bending Strength)

Slab Unit Dimensions (Used for Flexural Design):

17"x36" Slab Unit:

<u>Base</u>	<u>Height</u>
$b_1 := 35\text{in}$	$h_1 := 2.0\text{in}$
$b_2 := 0.75\text{in}$	$h_2 := 0.75\text{in}$
$b_3 := 0.75\text{in}$	$h_3 := 0.75\text{in}$
$b_4 := 0.25\text{in}$	$h_4 := 0.25\text{in}$
$b_5 := 0.25\text{in}$	$h_5 := 0.25\text{in}$



▣ Slab Unit/Girder Dimensions (For Nominal Bending Strength)

Steel Information:

Strand Info: (7/16" seven-wire strand, Grade 250)

Strand diameter. (7/16")

$$d_s := 0.4375\text{in}$$

Strand area.

$$A_s := 0.108\text{in}^2$$

Specified tensile strength of prestressing steel (ksi).
(MBE Table 6A.5.2.3-1)

$$f_{pu} := 250\text{ksi}$$

Yield strength of prestressing steel (ksi).

$$f_{py} := 0.9 \cdot f_{pu} = 225 \cdot \text{ksi}$$

Modulus of elasticity for prestressing strands (ksi).
(MBE Table 6A.5.2.3-1)

$$E_p := 28500\text{ksi}$$

Total number of strands at critical section

$$N_{\text{Total_str}} := 15$$

Area of existing prestressing steel.

$$A_{ps} := N_{\text{Total_str}} \cdot A_s = 1.62 \cdot \text{in}^2$$

Total Losses to prestressing steel (Assumed).

$$\Delta f_{pT} := 0.75 \cdot f_{pu} \cdot 13.43\% = 25.181 \cdot \text{ksi}$$

Effective stress in prestressing steel after losses.

$$f_{pe} := 0.75f_{pu} - \Delta f_{pT} = 162.319 \cdot \text{ksi}$$

Effective force in prestressing steel after losses.

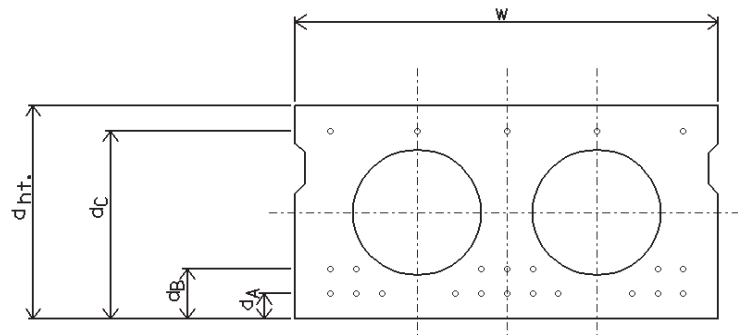
$$P_{pe} := A_{ps} \cdot f_{pe} = 262.956 \cdot \text{kip}$$

Effective prestress strain.

$$\epsilon_{pe} := \frac{f_{pe}}{E_p} = 0.0057$$

Strand Layout - Interior Units 2-8 & 2-9:

(Note: Assumed strand layout for Design, accounting for removal of severed/deteriorated strands per damages reported in the most current Inspection Reports, plus 50% of the adjacent strands)



Strand Locations (Measured inches From the Bottom)

"Location"	"From Bottom"	"No. Strands"
"Top Row"	14.5	4
"3rd Row"	6.5	0
"2nd Row"	4.5	5
"Bottom Row"	2.5	10

C.G. of PS to bottom fiber of slab unit at mid-span

$$y_{ps} := \frac{A_s \cdot (d_{strand_{3,2}} \cdot d_{strand_{3,1}} + d_{strand_{4,2}} \cdot d_{strand_{4,1}})}{(d_{strand_{3,2}} + d_{strand_{4,2}}) \cdot A_s} = 3.17 \cdot \text{in}$$

Prestressing strand eccentricity.

$$e_{nc} := y_{b_nc} - y_{ps} = 5.00 \cdot \text{in} \quad e_{ps} := y_b - y_{ps} = 5.00 \cdot \text{in}$$

Distance from the extreme compression fiber to the centroid of prestressing tendons.

$$d_{p_nc} := h_{nc} - y_{ps} = 13.83 \cdot \text{in} \quad d_p := h_c - y_{ps} = 13.83 \cdot \text{in}$$

Area of transverse reinforcement #4 stirrups
(Assume 3-legs of Transverse reinforcement)

$$A_v := 3(0.2) \text{ in}^2 = 0.6 \cdot \text{in}^2$$

Yield strength of stirrups (FDOT BLRM Table 6A.5.2.2-1)

$$f_y := 40 \text{ ksi}$$

▼ AASHTOWARE BrR-Inputs (Moment)

B. Moments (AASHTOWARE BrR Analysis Results):

(Note: *HL93 Truck LL Not Applicable to this Design*)

$$M_g := (87.1 \text{ kip}\cdot\text{ft})$$

$g := 0$
Moment due to self weight of the slab unit (Midspan).
(Total DC Self weight moment from AASHTOWare BrR)

$$M_{\text{pre_DC}} := (0 \text{ kip}\cdot\text{ft})$$

Moment due to additional precast components

$$M_{\text{pc}} := (0 \text{ kip}\cdot\text{ft})$$

Moment due dead load of deck slab
[Not Applicable]

$$M_c := (22.5 \text{ kip}\cdot\text{ft})$$

Moment due to additional structural components
(Total DC Railing & Sidewalk/Curb moment from
AASHTOWare BrR)

$$M_{\text{DC}} := M_g + M_{\text{pre_DC}} + M_{\text{pc}} + M_c = (109.6) \cdot \text{kip}\cdot\text{ft}$$

Dead load moment from structural components and
non-structural attachments.

$$M_{\text{DW}} := (0 \text{ kip}\cdot\text{ft})$$

Moment due to future wearing surface DL.

$$\text{LLDF}_{M_HL93} := (0.0)$$

[Not Applicable]

$$\text{LLDF}_{M_FL.Legal} := (0.256)$$

Live load distribution factor for moment from
AASHTOWare BrR Refined Analysis
(Note: Distribution Factor assuming post-tensioning is
repaired/restored)

$$M_{\text{LL_HL93}} := (0.0 \text{ kip}\cdot\text{ft})$$

Live load moment from controlling HL-93 truck.
[Not Applicable]

$$M_{\text{LL_FL.Legal}} := (171.55 \text{ kip}\cdot\text{ft})$$

Live load moment from controlling FL-Legal truck: SU4.

Design Load Combinations:

(Note: *HL93 Truck LL Not Applicable to this Design*)

$$M_{\text{Ser_FL.Legal}} := 1.0 \cdot M_{\text{DC}} + 1.0 \cdot M_{\text{DW}} + 1.0 \cdot M_{\text{LL_FL.Legal}} = (281.1) \cdot \text{kip}\cdot\text{ft}$$

Service moment (Service I).
AASHTO LRFD Table 3.4.1-1.

$$M_{\text{Str_FL.Legal}} := 1.25 \cdot M_{\text{DC}} + 1.5 \cdot M_{\text{DW}} + 1.35 \cdot M_{\text{LL_FL.Legal}} = (368.6) \cdot \text{kip}\cdot\text{ft}$$

Strength moment (Strength II).
AASHTO LRFD Table 3.4.1-1.

$$\phi M_{n_no_wrap} := (344.64 \text{ kip}\cdot\text{ft})$$

Capacity of member before FRP wrap is applied

▲ AASHTOWARE BrR-Inputs (Moment)

3. CFRP Reinforcement Properties

The amount of the CFRP reinforcement and its material properties are given as per net-fiber.

Thickness of the CFRP strip (*V-WrapTM - C200HM*)

$$t_f := 0.04 \text{ in}$$

Ultimate tensile strength of the CFRP

$$f_{fu_pre} := 155 \text{ ksi}$$

Rupture strain

$$\epsilon_{fu_pre} := 0.011$$

Modulus of elasticity of CFRP

$$E_f := 14 \cdot 10^6 \text{ psi} = 14000 \cdot \text{ksi}$$

Number of plies of CFRP sheets (Per preliminary recommendations)

$$n := 2$$

Width of the CFRP sheet (36" per preliminary recommendation from Structural Technologies)

$$w_f := 36 \text{ in}$$

CFRP orientation

$$\alpha_f := 90 \text{ deg}$$

Spacing of CFRP [Not Applicable]

$$s_{FRP} := 0 \text{ in}$$

Area of FRP for shear . (ACI 440.2R Eq. 11-4) [Not Applicable]

$$A_{fv} := 0 \text{ in}^2$$

Area of FRP for flexure (U-wrap)

$$A_{ff} := n \cdot t_f \cdot b_{f_bot} = 2.88 \cdot \text{in}^2$$

Environmental reduction factor for CFRP. (ACI 440.2R Table 9.1)

$$C_E := 0.85$$

Design ultimate tensile strength of CFRP. (ACI 440.2R Eq. 9-3)

$$f_{fu} := C_E \cdot f_{fu_pre} = 131.75 \cdot \text{ksi}$$

Ultimate rupture strain of CFRP reinforcement.
(ACI 440.2R Eq. 9-4)

$$\epsilon_{fu} := C_E \cdot \epsilon_{fu_pre} = 0.0093 \cdot \frac{\text{in}}{\text{in}}$$

4. DESIGN OF EXTERNALLY BONDED FRP REINFORCEMENT (ACI 440.2R-08, Chapter 11)

The CFRP sheets will be applied along the bottom face of the deteriorated slab units, along the full length and across the entire width of the slab units.

☒ FRP Strength Criteria (Moment)

$$\text{Check_FRP_Stength_Criteria_Moment}_g := \begin{cases} \text{"OK"} & \text{if } \left(\left(\phi M_{n_no_wrap_g} \geq 1.1 M_{DC_g} + 1.0 M_{LL_HL93_g} \right) \right) \text{ [NOT APPLICABLE]} \\ & \left(\left(\phi M_{n_no_wrap_g} \geq 1.1 \cdot M_{DC_g} + 1.0 M_{LL_FL_Legal_g} \right) \right) \\ \text{"Not Good"} & \text{otherwise } \text{FDOT FRPG Section 4.2.C} \\ & \text{(For multiple girder Strengthening)} \end{cases}$$

$$\text{Check_FRP_Stength_Criteria_Moment} = (\text{"OK"})$$

▲ FRP Strength Criteria (Moment)

▼ CFRP Development Length

FRP Reinforcement - Development Length

Determine length of CFRP needed to develop full bond capacity. Overlap length of CFRP sheets must be provided by manufacturer [ACI 440.2R-08 13.2](#)

$$l_{df} := 0.057 \cdot \sqrt{\frac{n \cdot E_f \cdot t_f}{\frac{f_{c_bm}}{\text{psi}}}} \cdot \text{in} = 7.174 \cdot \text{in}$$

Development length needed to develop full bond strength of CFRP [ACI 440.2R-08 \(13-2\)](#)

▲ CFRP Development Length

▼ Ultimate Flexural Strength Pt.1

FRP Reinforcement - Flexural Capacity

Design material properties:

$$f_{fu} = 131.75 \cdot \text{ksi}$$

$$\epsilon_{fu} = 9.35 \times 10^{-3}$$

Area of the CFRP reinforcement

$$A_{fv} = 5.76 \cdot \text{in}^2$$

Effective depth of CFRP ([ACI 440.2R-08 Fig 11.2](#))

$$d_{vFRP} := (d_p - t_{slab} - 2\text{in}) = 11.833 \cdot \text{in}$$

Active bond length ([ACI 440.2R-08 11.4.1.2](#))

$$L_e := \frac{2500\text{in}}{\left(n \cdot \frac{t_f}{\text{in}} \cdot \frac{E_f}{\text{psi}}\right)^{0.58}} = 0.775 \cdot \text{in}$$

Bond reduction coefficients ([ACI 440.2R-08 11.4.1.2](#))

$$k_1 := \left(\frac{f_c}{\text{psi} \cdot 4000}\right)^{\frac{2}{3}} = 1.16$$

$$k_2 := \frac{d_{vFRP} - L_e}{d_{vFRP}} = 0.934 \quad \text{for U-Wrap}$$

$$\kappa_v := \frac{k_1 \cdot k_2 \cdot \frac{L_e}{\text{in}}}{468 \cdot \epsilon_{fu}} = 0.192$$

$$\kappa_v := \min(0.75, \kappa_v) = 0.192$$

Effective strain of the CFRP reinforcement

$$\epsilon_{fe} := \min(\kappa_v \cdot \epsilon_{fu}, 0.004) = 0.0018$$

([ACI 440.2R-08 11.4.1.2](#))

Effective strength of the CFRP reinforcement
(ACI 440.2R Eq. 11-5)

$$f_{fe} := \epsilon_{fe} \cdot E_f = 25.145 \cdot \text{ksi}$$

Determine the existing state of strain

Determine strain at soffit during installation of CFRP. Tension is positive and compression is negative.

$$\epsilon_{bi} := \frac{-P_{pe}}{E_{c_bm} \cdot A_{nc}} + \frac{-P_{pe} \cdot e_{nc} + M_g + M_{pc}}{E_{c_bm} \cdot S_{b_nc}} + \frac{M_c}{E_{c_bm} \cdot S_b} = (-1.396 \times 10^{-4})$$

Determine the design strain of the FRP system

Determine strain at which debonding of CFRP may occur

$$\epsilon_{fd} := \min \left(0.083 \cdot \sqrt{\frac{f_{c_bm} \cdot \text{psi} \cdot \text{in}}{n \cdot E_f \cdot t_f \cdot \text{psi}}}, 0.9 \cdot \epsilon_{fu} \right) = 5.546 \times 10^{-3} \quad \text{ACI 440.2R-08 (10-2)}$$

Determine flexure capacity of section

The determination of flexural capacity for prestressed slab units repaired with CFRP wraps makes use of strain compatibility which is an iterative process. Each iteration involves the assumption of a neutral axis depth. Once an assumption is made, the strains in the compressive concrete face, CFRP wrap, and strands are determined based on a linear strain relationship. The calculated strains are then converted into compressive and tensile forces that are used to check if equilibrium within the cross section is obtained, iterations continue until equilibrium is reached. **It is assumed all strands are bonded at the section of interest.**

Guess neutral axis depth (reasonable guess is 0.1*depth of section):

$$c := (6.475 \text{ in})$$

Assumed depth from top of section to neutral axis

Determine the effective level of strain in the CFRP reinforcement:

$$d_f := h_c = 17 \cdot \text{in}$$

Depth from top of section to CFRP reinforcement

$$\epsilon_{c_i} := \text{for } i \in g$$

$$\epsilon_{fe_i} \leftarrow \min \left[0.003 \cdot \left(\frac{d_f - c_i}{c_i} \right) - \epsilon_{bi_i}, \epsilon_{fd} \right]$$

Strain in CFRP reinforcement
ACI 440.2R-08 (10-16)

$$\epsilon_{fe} = (5.016 \times 10^{-3})$$

Controlling_Failure := for i ∈ g

$$\left| \begin{array}{l} \text{Controlling_Failure}_i \leftarrow \text{"CFRP debonding/rupture controls"} \text{ if } |\epsilon_{fe_i}| = \epsilon_{fd} \\ \text{Controlling_Failure}_i \leftarrow \text{"Concrete crushing controls"} \text{ otherwise} \end{array} \right.$$

Controlling_Failure = ("Concrete crushing controls")

Determine strain at extreme compression fiber based on controlling failure type:

$\epsilon_c :=$ for i ∈ g

$$\left| \begin{array}{l} \epsilon_{c_i} \leftarrow (\epsilon_{fe_i} + \epsilon_{bi_i}) \cdot \frac{c_i}{d_f - c_i} \text{ if } \epsilon_{fe_i} = \epsilon_{fd} \\ \epsilon_{c_i} \leftarrow 0.003 \text{ otherwise} \end{array} \right.$$

CFRP debonding/rupture

Concrete crushing

$$\epsilon_c = (3 \times 10^{-3})$$

Strain at extreme compression fiber

Calculate the strain in the existing prestressing steel:

Net tensile strain in prestressing steel beyond decompression, at nominal strength

$\epsilon_{pnet} :=$ for i ∈ g

$$\left| \begin{array}{l} \epsilon_{pnet_i} \leftarrow (\epsilon_{fe_i} + \epsilon_{bi_i}) \cdot \left(\frac{d_p - c_i}{d_f - c_i} \right) \text{ if } \epsilon_{fe_i} = \epsilon_{fd} \\ \epsilon_{pnet_i} \leftarrow 0.003 \cdot \frac{d_p - c_g}{c_g} \text{ otherwise} \end{array} \right.$$

CFRP debonding/rupture
ACI 440.2R-08 (10-23b)

Concrete crushing
ACI 440.2R-08 (10-23a)

$$\epsilon_{pnet} = (3.409 \times 10^{-3})$$

$\epsilon_{ps} :=$ for i ∈ g

$= (9.359 \times 10^{-3})$ Strain in prestressing steel
ACI 440.2R-08 (10-22)

$$\epsilon_{ps_i} \leftarrow \min \left[\epsilon_{pe} + \frac{P_{pe}}{A_{nc} \cdot E_{c_bm}} \cdot \left(1 + \frac{e_{nc}^2}{r^2} \right) + \epsilon_{pnet_i}, 0.035 \right]$$

$$\text{Check_steel_rupture}_g := \begin{cases} \text{"Need to consider steel rupture"} & \text{if } \epsilon_{ps_g} \geq 0.035 \\ \text{"Steel rupture does not control OK"} & \text{otherwise} \end{cases}$$

Check if steel rupture controls
[ACI 440.2R-08 \(10-22\)](#)

$$\text{Check_steel_rupture} = (\text{"Steel rupture does not control OK"})$$

Calculate the stress level in prestressing steel and CFRP:

$$f_{ps_g} := \begin{pmatrix} 28500 \cdot \epsilon_{ps} & \text{if } \epsilon_{ps_g} \leq 0.0076 \\ 250 - \frac{0.04}{\epsilon_{ps_g} - 0.0064} & \text{otherwise} \end{pmatrix} \cdot \text{ksi}$$

Stress in prestressing steel (applicable for Grade 250 ksi steel)
[ACI 440.2R-08 \(10-24b\)](#)

$$f_{ps_g} = 236.483 \cdot \text{ksi}$$

$$f_{fe} := E_f \cdot \epsilon_{fe} = (70.224) \cdot \text{ksi}$$

Stress in CFRP Reinforcement
[ACI 440.2R-08 \(10-21\)](#)

Calculate the internal force resultants and check equilibrium:

Use Whitney Stress Block to model stress if concrete crushing controls. If CFRP debonding/rupture controls use approximate stress block factors based on parabolic stress-strain relationship for concrete (see [ACI 440.2R-08 15.5 Step 9](#))

$$\beta_{1_g} := \begin{cases} \text{if } \epsilon_{fe_g} = \epsilon_{fd} \\ \begin{cases} \epsilon'_c \leftarrow \frac{1.7 \cdot f'_{c_bm}}{E_{c_bm}} \\ \beta_1 \leftarrow \frac{4 \cdot \epsilon'_c - \epsilon_{c_g}}{6 \cdot \epsilon'_c - 2 \cdot \epsilon_{c_g}} \end{cases} \\ \text{if } \epsilon_{c_g} = 0.003 \\ \begin{cases} \beta_1 \leftarrow \max \left(0.85 - \frac{f'_{c_bm} - 4000 \text{psi}}{1000 \cdot \text{psi}} \cdot 0.05, 0.65 \right) & \text{if } f'_{c_bm} > 4000 \text{psi} \\ \beta_1 \leftarrow 0.85 & \text{if } f'_{c_bm} \leq 4000 \text{psi} \end{cases} \end{cases}$$

Approximate stress block β factor based on parabolic stress-strain relationship [ACI 440.2R-08 15.5 Step 9](#)

Stress block β factor based on Whitney Stress Block

$$\beta_1 = (0.8)$$

$$\beta_{1_g} = 0.8$$

$$\alpha_{1g} := \begin{cases} \alpha_1 \leftarrow 0.85 & \text{if } \epsilon_{cg} = 0.003 \\ \text{otherwise} \\ \epsilon'_c \leftarrow \frac{1.7 \cdot f_{c_bm}}{E_{c_bm}} \\ \alpha_1 \leftarrow \frac{3 \cdot \epsilon'_c \cdot \epsilon_{cg} - (\epsilon_{cg})^2}{3 \cdot \beta_{1g} \cdot \epsilon'^2_c} \end{cases}$$

$$\alpha_1 = (0.85)$$

$$\alpha_{1g} = 0.85$$

Stress block α factor based on Whitney Stress Block

Approximate stress block α factor based on parabolic stress-strain relationship [ACI 440.2R-08 15.5 Step 9](#)

▲ Ultimate Flexural Strength Pt.1

▼ Strain Compatability Calcs

$$f_{w_transf} := \frac{b_1 \cdot (h_1 + h_2) - \left(2 \cdot \frac{1}{2} \cdot b_2 \cdot h_2 \right)}{b_1 \cdot (h_1 + h_2)} \cdot b_1 = 34.795 \cdot \text{in}$$

Use transformed girder flange width if stress block lies on or beyond first tapered section of girder flange

```

Ten_Com := for i ∈ g
    if  $\beta_{1_i} \cdot c_i \leq t_{slab}$  Stress block in deck
        Comi ←  $\alpha_{1_i} \cdot f_{c\_bm} \cdot b_{transf} \cdot \beta_{1_i} \cdot c_i$ 
        Teni ←  $A_{ps} \cdot f_{ps_i} + A_{ff} \cdot f_{fe_i}$ 
    if  $\beta_{1_i} \cdot c_i > t_{slab} \wedge \beta_{1_i} \cdot c_i \leq h_1 + t_{slab}$  Stress block in top of flange
        Comi ←  $\alpha_{1_i} \cdot f_{c\_bm} \cdot b_{transf} \cdot t_{slab} + \alpha_{1_i} \cdot f_{c\_bm} \cdot b_1 \cdot (\beta_{1_i} \cdot c_i - t_{slab})$ 
        Teni ←  $A_{ps} \cdot f_{ps_i} + A_{ff} \cdot f_{fe_i}$ 
    if  $\beta_{1_i} \cdot c_i > h_1 + t_{slab} \wedge \beta_{1_i} \cdot c_i \leq h_1 + h_2 + t_{slab}$  Stress block in first tapered section of flange
        Comi ←  $\alpha_{1_i} \cdot f_{c\_bm} \cdot b_{transf} \cdot t_{slab} + \alpha_{1_i} \cdot f_{c\_bm} \cdot f_{w\_transf} \cdot (\beta_{1_i} \cdot c_i - t_{slab})$ 
        Teni ←  $A_{ps} \cdot f_{ps_i} + A_{ff} \cdot f_{fe_i}$ 
    if  $\beta_{1_i} \cdot c_i > h_1 + h_2 + t_{slab} \wedge \beta_{1_i} \cdot c_i \leq h_1 + h_2 + h_4 + t_{slab}$  Stress block in second tapered section of flange
        Comi ←  $\alpha_{1_i} \cdot f_{c\_bm} \cdot b_{transf} \cdot t_{slab} + \alpha_{1_i} \cdot f_{c\_bm} \cdot (h_1 + h_2) \cdot f_{w\_transf} + \alpha_{1_i} \cdot f_{c\_bm} \cdot (\beta_{1_i} \cdot c_i - t_{slab} - h_1 - h_2) \cdot (b_w + b_4)$ 
        Teni ←  $A_{ps} \cdot f_{ps_i} + A_{ff} \cdot f_{fe_i}$ 
    if  $\beta_{1_i} \cdot c_i > h_1 + h_2 + h_4 + t_{slab}$  Stress block in web
        Comi ←  $\alpha_{1_i} \cdot f_{c\_bm} \cdot b_{transf} \cdot t_{slab} + \alpha_{1_i} \cdot f_{c\_bm} \cdot (h_1 + h_2) \cdot f_{w\_transf} + \alpha_{1_i} \cdot f_{c\_bm} \cdot (h_4 \cdot b_w + h_4 \cdot b_4) \dots$ 
         $+ \alpha_{1_i} \cdot f_{c\_bm} \cdot [\beta_{1_i} \cdot c_i - t_{slab} - (h_1 + h_2 + h_4)] \cdot b_w$ 
        Teni ←  $A_{ps} \cdot f_{ps_i} + A_{ff} \cdot f_{fe_i}$ 
return augment(Ten, Com)

```

▼ Ultimate Flexural Capacity Pt.2

$$T_{en_Com} = (585.349 \ 585.521) \cdot \text{kip}$$

Check if section is in equilibrium

	<u>Tension</u>	<u>Compression</u>
Equilibrium :=	for $i \in g$	
	$\text{Equilibrium}_i \leftarrow \text{"Equilibrium achieved"} \quad \text{if} \quad \left \frac{T_{en_Com_{i,0}} - T_{en_Com_{i,1}}}{T_{en_Com_{i,0}}} \right \leq 1\%$	
	$\text{Equilibrium}_i \leftarrow \text{"Equilibrium not achieved, adjust c value"} \quad \text{if} \quad \left \frac{T_{en_Com_{i,0}} - T_{en_Com_{i,1}}}{T_{en_Com_{i,0}}} \right > 1\%$	
	return Equilibrium	

$$\text{Equilibrium} = (\text{"Equilibrium achieved"})$$

Nominal flexural strength:

$$M_{np} := \left[A_{ps} \cdot f_{ps} \cdot \left(d_p - \frac{\beta_1 \cdot c}{2} \right) \right] = (358.946) \cdot \text{kip} \cdot \text{ft}$$

Prestressing steel contribution to flexural strength

Percent difference of calculated nominal strength of section without CFRP vs Conspan flexural capacity.
Use nominal section strength for check since AASHTO uses $\phi = 1.0$ and ACI use $\phi = 0.9$

$$\left| \frac{M_{np_g} - \phi M_{n_no_wrap_g}}{\phi M_{n_no_wrap_g}} \right| = 4.151\%$$

$$M_{nf} := \left[A_{ff} \cdot f_{fe} \cdot \left(d_f - \frac{\beta_1 \cdot c}{2} \right) \right] = (242.864) \cdot \text{kip} \cdot \text{ft}$$

CFRP contribution to flexural strength

Design flexural strength:

$$\phi_g := \begin{cases} \phi \leftarrow 0.9 & \text{if } \epsilon_{ps_g} \geq 0.013 \\ \phi \leftarrow 0.65 + \frac{0.25 \cdot (\epsilon_{ps_g} - 0.010)}{0.013 - 0.010} & \text{if } \epsilon_{ps_g} > 0.010 \wedge \epsilon_{ps_g} < 0.013 \\ \phi \leftarrow 0.65 & \text{if } \epsilon_{ps_g} \leq 0.01 \end{cases}$$

Strength reduction factor
[ACI 440.2R-08 \(10-19\)](#)

$$\phi = (0.65)$$

$$\phi M_n := \left[\phi \cdot (M_{np} + \psi_f \cdot M_{nf}) \right] = (367.497) \cdot \text{kip} \cdot \text{ft}$$

Design strength of composite section with CFRP wrap
[ACI 440.2R-08 \(10-26\)](#)

▲ Ultimate Flexural Capacity Pt.2

▼ Service I

FRP Reinforcement - Service Check

Check service stresses using Service I load combinations: SDG Vol 4. 4.2

Check if section will crack under service loads

$$f_D := \frac{-P_{pe}}{A_{nc}} + \frac{-P_{pe} \cdot e_{nc} + M_g + M_{pc}}{S_{b_nc}} + \frac{M_c}{S_b} = (-0.599) \cdot \text{ksi}$$

Stress at soffit due to dead load.
Tension is positive and compression
is negative

Check if section is cracked due to live load moment:

Is_section_cracked := for i ∈ g

$$\left| \begin{array}{l} \text{Is_section_cracked}_i \leftarrow \text{"Section is cracked; CFRP Strengthening Required"} \quad \text{if } f_{D_i} + \frac{M_{LL_FL_Legal}_i}{S_b} \geq f_r \\ \text{Is_section_cracked}_i \leftarrow \text{"Section is not cracked OK"} \quad \text{otherwise} \end{array} \right.$$

Is_section_cracked = ("Section is cracked; CFRP Strengthening Required")

Check stress in prestressing steel

Strain in prestressing steel. Tension is positive and compression is negative.

$$\epsilon_{ps_s} := \epsilon_{pe} - \frac{P_{pe}}{A_{nc} \cdot E_{c_bm}} \cdot \left(1 + \frac{e_{nc}^2}{r^2} \right) + \frac{(M_g + M_{pc}) \cdot e_{nc}}{I_{nc} \cdot E_{c_bm}} + \frac{(M_c + M_{LL_FL_Legal}) \cdot e}{I \cdot E_{c_bm}} = (5.736 \times 10^{-3})$$

f_{ps_s} := for i ∈ g

$$\left| \begin{array}{l} f_{ps_s_i} \leftarrow 28500 \cdot \epsilon_{ps_s_i} \cdot \text{ksi} \quad \text{if } \epsilon_{ps_s_i} \leq 0.0076 \\ f_{ps_s_i} \leftarrow \left(250 - \frac{0.04}{|\epsilon_{ps_s_i}| - 0.0064} \right) \cdot \text{ksi} \quad \text{if } \epsilon_{ps_s_i} > 0.0076 \end{array} \right.$$

Stress in prestressing steel
(applicable for 250 grade steel)
ACI 440.2R-08 (10-24b)

$$f_{ps_s} = (163.468) \cdot \text{ksi}$$

Check_steel_stress := for $i \in g$

$$\left| \begin{array}{l} \text{Check_steel_stress}_i \leftarrow \text{"OK"} \quad \text{if } \left| f_{ps_s_i} \right| \leq 0.82 \cdot f_{py} \wedge \left| f_{ps_s_i} \right| \leq 0.74 \cdot f_{pu} \\ \text{Check_steel_stress}_i \leftarrow \text{"NOT OK"} \quad \text{otherwise} \end{array} \right.$$

Check if stress in prestressing
steel satisfies
ACI 440.2R-08 (10-20a) & (10-20b)

Check_steel_stress = ("OK")

Check compressive stress in concrete

Tension is positive and compression is negative

Check top of precast slab unit:

$$f_{c_top_gir} := \frac{-P_{pe}}{A_{nc}} + \frac{P_{pe} \cdot e_{nc} - M_g - M_{pc}}{S_{t_nc}} - \frac{M_c}{S_{top_girder_c}} - \frac{M_{LL_FL.Legal}}{S_{top_girder_c}} = (-1.964) \cdot \text{ksi}$$

Stress at top of precast
girder

Check_top_girder_stress := for $i \in g$

$$\left| \begin{array}{l} \text{Check_top_girder_stress}_i \leftarrow \text{"OK"} \quad \text{if } \left| f_{c_top_gir_i} \right| \leq 0.45 \cdot f_{c_bm} \\ \text{Check_top_girder_stress}_i \leftarrow \text{"NOT OK"} \quad \text{otherwise} \end{array} \right.$$

Check_top_girder_stress = ("OK")

Check top of deck: - **[NO DECK PRESENT; CHECK NOT APPLICABLE]**

$$f_{c_top_deck} := \text{if} \left(t_{slab} = 0 \text{ in}, 0 \text{ ksi}, \frac{M_c}{S_t} \cdot n - \frac{M_{LL_FL.Legal}}{S_t} \cdot n \right) = 0 \cdot \text{ksi}$$

Stress at top of deck

Check_top_deck_stress := if $(t_{slab} = 0 \text{ in}, \text{"NOT APPLICABLE"}, \text{for } i \in g$

$$\left| \begin{array}{l} \text{Check_top_deck_stress}_i \leftarrow \text{"OK"} \quad \text{if } \left| f_{c_top_deck_i} \right| \leq 0.45 \cdot f_{cslab} \\ \text{Check_top_deck_stress}_i \leftarrow \text{"NOT OK"} \quad \text{otherwise} \end{array} \right.$$

Check_top_deck_stress = "NOT APPLICABLE"

Check stress in CFRP

Tension is positive and compression is negative

$$f_{f_s} := \frac{E_f}{E_{c_bm}} \cdot \left(f_D + \frac{M_{LL_FL.Legal}}{S_b} \right) - \epsilon_{bi} \cdot E_f = (4.115) \cdot \text{ksi}$$

Stress in CFRP

Check_FRP_stress := for i ∈ g

$$\begin{cases} \text{Check_FRP_stress}_i \leftarrow \text{"OK"} & \text{if } |f_{f_s_i}| \leq 0.55 \cdot f_{fu} \\ \text{Check_FRP_stress}_i \leftarrow \text{"Not OK"} & \text{otherwise} \end{cases}$$

Check that stress in CFRP satisfies
[ACI 440.2R-08 Table 10.1](#)

Check_FRP_stress = ("OK")

▲ Service I

▼ FRP Fatigue Check

FRP Reinforcement - Fatigue

[SDG Vol. 4.2](#) states that the standard fatigue truck from LRFD should be used to check fatigue stresses in CFRP composite. By inspection, the standard fatigue truck will produce lower stresses within the section when compared to the truck used for the Service I stress check. If Service I is satisfied, no further analysis is required.
(Refer to [ACI 440.2R-08 10.2.9](#))

▲ FRP Fatigue Check

Summary:

The Flexural Loading Rating (LR) controlled by SU4 Legal Strength loading which produced a LR of 0.931 was increased by CFRP strengthening along the bottom face of the slab unit length. The CFRP strengthening design consisted of U-wrap method plies which are 36" wide (C200HM) along the controlling sections. The strengthened section resulted in a flexural load rating shown below:

Number of Plies
for U-Wrap Shear

n = 2

Width of Plies

w_f = 36·in

FRP Development Length

l_{df} = 7.174·in

FRP Stress Check

Check_FRP_stress = ("OK")

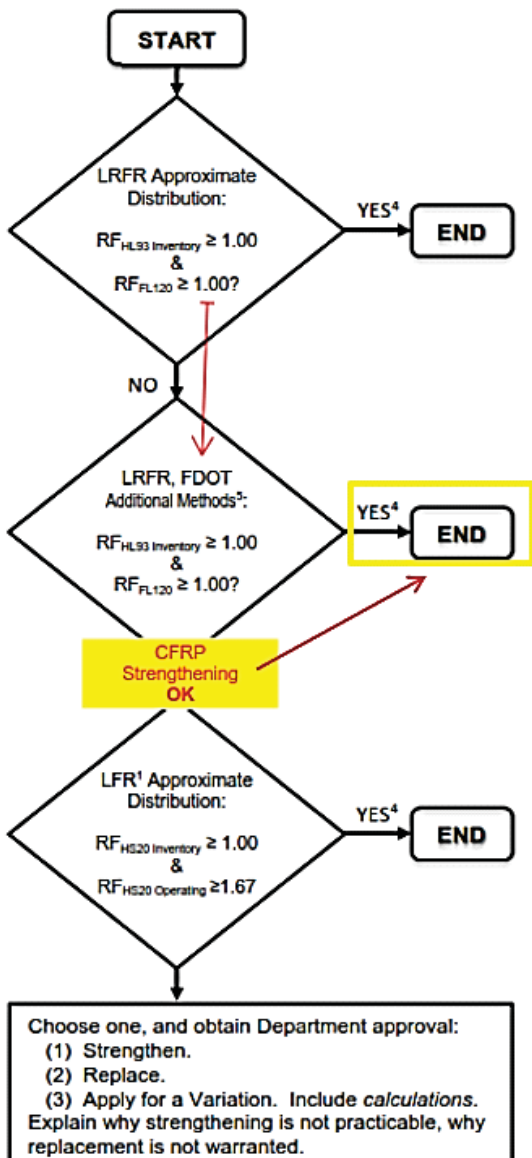
Rating Factor (Moment)

RATING FACTOR FOR CONTROLLING LEGAL LOAD (SU4) OPERATING LOADING MOMENT

$$RF_{OPT.moment_rehab} := \frac{\phi M_n - \gamma_{DC} \cdot M_{DC}}{\gamma_{OPT} \cdot M_{LL_FL.Legal}} = 1$$

Rating Factor (Moment)

FDOT Fig.2-2—Widening & Rehab.



3.0 POST-TENSIONING ALTERNATIVES FOR REPLACEMENT OF EXISTING POST-TENSIONING WIRE

Specifications: AASHTO LRFD Specifications for Highway Bridges, 9th edition 2020;
AASHTO ASD Specifications for Highway Bridges, 11th edition 1973
FDOT Load Rating Manual 2021

References 1) "Transverse post tensioning design and detailing of precast, prestressed adjacent box girder bridges", Kromel E. Hanna, George Morcoux, and Maher K. Tadros, PCI Journal, 2009.

Units: U.S customary units

Existing Sonovoid Slab Post-Tensioning:

INPUT DATA

Bridge Data:

$\text{Depth}_{\text{sonovoid}} := 17\text{in}$	Depth of Sonovoid Slab Unit (in.)
$\text{Width}_{\text{sonovoid}} := 36\text{in}$	Width of Sonovoid Slab Unit (in.)
$y_{\text{c_bot}} := 8.1667\text{in}$	Distance Y from bottom face to Cg of section (in.)
$y_{\text{c_top}} := \text{Depth}_{\text{sonovoid}} - y_{\text{c_bot}} = 0.736\text{ft}$	Distance Y from top face to Cg of section (in.)
$L_{\text{Span_1}} := 29.042\text{ft}$	Length of Span 1 or 3 (Brg-to-Brg.) (ft.)
$L_{\text{Span_2}} := 38.50\text{ft}$	Length of Span 2 (Brg-to-Brg.) (ft.)
$\text{Skew} := 0\text{deg}$	Bridge Skew Angle (degrees)
$\text{Width}_{\text{bridge}} := 34\text{ft}$	Width of Bridge (ft.) - (Assumed width of bridge ignoring the 6" sidewalk overhang for analysis).
$\text{Width}_{\text{diaphragm}} := 12\text{in}$	Diaphragm Width of Sonovoid Slab Unit (in.)

Post-Tensioning Strand Data:

$n := 2$	Specified Number of Post-Tensioning Bar per duct
$d_{\text{strand}} := 0.50\text{in}$	Specified Diameter of Post-Tensioning Strand (in) (See Appendix E)
$\text{Area}_{\text{PT_strand}} := 0.153\text{in}^2$	Minimum net Area of 0.50" diameter Strand (in ²) (See Appendix E)
$f_{\text{pu}} := 270\text{ksi}$	Ultimate Strength of Post-Tensioning Strand (ksi) (See Appendix E)
$f_y := 245\text{ksi}$	Yield Strength of Post-Tensioning Strand (ksi) (See Appendix E)
$P_{\text{ult}} := f_{\text{pu}} \cdot \text{Area}_{\text{PT_strand}} = 41.31\text{kip}$	Minimum Ultimate Strength of Post-Tensioning Strand (kip) (See Appendix E)

Calculate Minimum Required Transverse Post-Tensioning Force per Diaphragm after Anchorage Setting:
(AASHTO LRFD 5.12.2.3.3c)

$$F_{\min_trans_PT} := 0.25 \text{ksi} \cdot (\text{Width}_{\text{diaphragm}} \cdot \text{Depth}_{\text{sonovoid}}) = 51 \cdot \text{kip} \quad \text{Estimated Minimum Required Transverse Post-Tensioning Force per Diaphragm (AASHTO LRFD 5.12.2.3.3c)}$$

Check Minimum Required Prestressing Strands:

$$\text{Area}_{\text{Min_PT_strand}} := \frac{F_{\min_trans_PT}}{0.70 \cdot f_{pu}} = 0.27 \cdot \text{in}^2 \quad \text{Minimum Area of Post-Tensioning Bar required to satisfy the minimum Transverse Post-Tensioning Force (in}^2\text{) (AASHTO LRFD Table 5.9.2.2-1)}$$

$$\text{Area}_{\text{PT_strand_provided}} := n \cdot \text{Area}_{\text{PT_strand}} = 0.306 \cdot \text{in}^2 \quad \text{Area of Post-Tensioning Strands provided (in}^2\text{)}$$

Check Minimum Area of Post-Tensioning Strand to satisfy minimum transverse Post-Tensioning Force per AASHTO:

$$\text{Check}_{\min_Area_PT} := \text{if}(\text{Area}_{\text{PT_strand_provided}} < \text{Area}_{\text{Min_PT_strand}}, \text{"N.G., Increase Bar Size"}, \text{"OK, Min. Req. Area Satisfied"})$$

Check_{min_Area_PT} = "OK, Min. Req. Area Satisfied"

$$\text{Check}_{\min_Area_PT_ratio} := \frac{\text{Area}_{\text{PT_strand_provided}}}{\text{Area}_{\text{Min_PT_strand}}} = 1.134$$

Specifications: AASHTO LRFD Specifications for Highway Bridges, 9th edition 2020;
AASHTO ASD Specifications for Highway Bridges, 11th edition 1973
FDOT Load Rating Manual 2021

References 1) "Analysis of Bolt Torquing", PDHonline Course S149
2) "Transverse post tensioning design and detailing of precast, prestressed adjacent box girder bridges", Kromel E. Hanna, George Morcoux, and Maher K. Tadros, PCI Journal, 2009.
3) Williams Form Engineering Corp., "Post-Tensioning System and Prestressing Steel Bars".

Units: U.S customary units

Determine Force in Transverse Post-Tensioning:

INPUT DATA

Bridge Data:

Depth _{sonovoid} := 17in	Depth of Sonovoid Slab Unit (in.)
Width _{sonovoid} := 36in	Width of Sonovoid Slab Unit (in.)
L _{Span_1} := 29.042ft	Length of Span 1 or 3 (Brg-to-Brg.) (ft.)
L _{Span_2} := 38.50ft	Length of Span 2 (Brg-to-Brg.) (ft.)
Skew := 0deg	Bridge Skew Angle (degrees)
Width _{bridge} := 34ft	Width of Bridge (ft.) - (Assumed width of bridge ignoring the 6" sidewalk overhang for analysis).
Width _{diaphragm} := 12in	Diaphragm Width of Solenoid Slab Unit (in.) -

Post-Tensioning Bar Data:

n := 1	Specified Number of Post-Tensioning Bar per duct
d _{bar} := 1.0in	Specified Diameter of All-Threated Post-Tentioning Bar (in) (See Appendix E)
pitch _{bar} := 4.0in	Specified Pitch of All Threated Post-Tensioning Bar (in) (See Appendix E)
Area _{PT_bar} := 0.85in ²	Minimum net Area of 1" diameter All-threatened bar (in ²) (See Appendix E)
f _{pu} := 150ksi	Ultimate Strength of Post-Tensioning Bar (ksi) (See Appendix E)
f _y := 120ksi	Yield Strength of Post-Tensioning Bar (ksi) (See Appendix E)
P _{ult} := 128kip	Minimum Ultimate Strength of Post-Tensioning Bar (kip) (See Appendix E)

$$P_{0.6P_u_PT_Force} := 76.5 \text{ kip}$$

Ultimate Prestressing Force at release, $0.60P_u$ (kip)
(See Appendix E)

$$\text{major_diameter} := 1.125 \text{ in}$$

Major Bar/Bolt Diameter (in.)
(See Appendix E)

$$\text{minor_diameter} := n \cdot d_{\text{bar}} = 1 \cdot \text{in}$$

Minor Bar/Bolt Diameter (in)

Compute the Minimum Required Transverse Post-Tensioning Force per Diaphragm after Anchorage Setting:
(AASHTO LRFD 5.12.2.3.3c)

$$F_{\text{min_trans_PT}} := 0.25 \text{ ksi} \cdot (\text{Width}_{\text{diaphragm}} \cdot \text{Depth}_{\text{sonovoid}}) = 51 \cdot \text{kip}$$

Estimated Minimum Required Transverse Post-Tensioning Force per Diaphragm (AASHTO LRFD 5.12.2.3.3c)

Check Minimum Required Prestressing Bar:

$$\text{Area}_{\text{Min_Req_PT_Bar}} := \frac{F_{\text{min_trans_PT}}}{0.70 \cdot f_{pu}} = 0.486 \cdot \text{in}^2$$

Minimum Area of Post-Tensioning Bar required to satisfy the minimum Transverse Post-Tensioning Force (in^2) (AASHTO LRFD Table 5.9.2.2-1)

$$\text{Area}_{\text{PT_Bar_provided}} := n \cdot \text{Area}_{\text{PT_bar}} = 0.85 \cdot \text{in}^2$$

Area of Post-Tensioning Bar provided (in^2)

$$\text{Check}_{\text{min_Area_PT}} := \text{if}(\text{Area}_{\text{PT_Bar_provided}} < \text{Area}_{\text{Min_Req_PT_Bar}}, \text{"N.G., Increase Bar Size"}, \text{"OK, Min. Req. Area Satisfied"})$$

$$\text{Check}_{\text{min_Area_PT}} = \text{"OK, Min. Req. Area Satisfied"}$$

$$\text{Check}_{\text{min_Area_PT_ratio}} := \frac{\text{Area}_{\text{PT_Bar_provided}}}{\text{Area}_{\text{Min_Req_PT_Bar}}} = 1.75$$

Determine Preload Force in Post-Tensioning Bar From Applied Torque:

Determine force in 1" bar due to 1000 lb-ft torque

Loads and Load Factors:

$$\text{Torque} := 1000 \cdot \text{lb-ft}$$

Assumed Torque applied to Post-Tensioning bars to achieve the minimum required Post-Tensioning force
(See Appendix E)

$$d_m := \frac{\text{major_diameter} + \text{minor_diameter}}{2} = 1.063 \cdot \text{in}$$

Effective contact diameter for the threads

$$\text{TPI} := \frac{8}{\text{in}}$$

Threads per inch

$$\text{Nut_OD} := 1.625 \text{ in}$$

Distance between nut flats for hex nuts
(See Appendix E)

$$l := \frac{1}{\text{TPI}}$$

Lead

$$d_c := \frac{\text{major_diameter} + \text{Nut_OD}}{2} = 1.375 \cdot \text{in}$$

$$\alpha := 30 \text{deg}$$

Angle of thread

$$\mu := 0.15$$

Coefficient of friction assuming non-lubricated steel bolt

$$\text{Factor} := \frac{1}{2 \cdot \pi} + \frac{\mu \cdot d_m}{2 \cdot \cos(\alpha)} + \frac{\mu \cdot d_c}{2} = 0.018 \text{ ft}$$

Factor used to convert force to Torque

$$P_{\text{Torque}} := \frac{\text{Torque}}{\text{Factor}} = 55.805 \cdot \text{kip}$$

Prestressing force in Post-Tensioning Bar

Check Minimum Required Transverse Post-Tensioning Force per Diaphragm after Anchorage Setting:
(AASHTO LRFD 5.12.2.3.3c)

$$F_{\text{min_trans_PT}} = 51 \cdot \text{kip}$$

Estimated Minimum Required Transverse Post-Tensioning
Force per Diaphragm (AASHTO LRFD 5.12.2.3.3c)

$$F_{\text{PT_perBar}} := \frac{P_{\text{Torque}}}{n} = 55.805 \cdot \text{kip}$$

Estimated Force in each Transverse Post-Tensioning Bar (kip)

$$\text{Check}_{\text{min_trans_PT_Force}} := \text{if}(F_{\text{PT_perBar}} < F_{\text{min_trans_PT}}, \text{"N.G., Increase Force"}, \text{"OK, Min. Required Force Satisfied"})$$

$$\text{Check}_{\text{min_trans_PT_Force}} = \text{"OK, Min. Required Force Satisfied"}$$

$$\text{Check}_{\text{min_trans_PT_Force_ratio}} := \frac{F_{\text{PT_perBar}}}{F_{\text{min_trans_PT}}} = 1.094$$

4.0 COLUMN LOADS FOR TEMPORARY SHORING

Pier 2 Column Loads & LBC (RCPIer) Input - Matheson Hmk Park Bridge

A. General Criteria

(Note: On Project Tab in RCPier use Structure Type as "Pier". Use "US_LRFD" and State Specifications "None" with "U.S. Units".)

A1. General Variables

Depth of Interior Pier Cap:	$h_{cap} := 3.0\text{ft}$
Width of Interior Bent Cap:	$b_{cap} := 3.0\text{ft}$
Length of Interior Bent Cap:	$L_{cap} := 34\text{ft}$
Pile Embedment Depth:	$Pile_{embed} := 1.0\text{ft}$
Pile Size:	$Pile_{size} := 14\text{in}$
Unit Weight of Concrete:	$w_c := 150\text{pcf}$
Length of Span 1 or 3:	$L_{span1} := 30\text{ft}$
Length of Span 1 or 3:	$L_{span2} := 40\text{ft}$
Width of Bridge:	$W_{br} := 34\text{ft}$
Bridge Deck Depth:	$d_{slab} := 1.292\text{in}$
Bridge Skew Angle:	$\theta_{skew} := 0\text{deg}$
Length of Bridge:	$L_{br} := 100\text{ft}$
Height of Bearing Pad:	$h_{bp} := \left(\frac{1}{4}\right) \cdot \text{in}$
Width of Bearing Pad	$w_{bp} := 2\text{ft} + 0\text{in}$
Length of Bearing Pad:	$L_{bp} := 6\text{in}$

(Average Depth of Asphalt overlay used since no deck slab is present)

(See Appendix A, sheetno. 7 of 12 of Asbuilt Plans)

(Assumed per Asbuilt plans details)

B. Geometry Tab (RCPier)

B1. Pier Config.

Pier Type:	$PierType := \text{"Multi Columns"}$	(Use "Multi Columns" from the Pier Configuration)
Cap Shape:	$CapShape := \text{"Straight"}$	(Use Cap as straight since height of pedestal will determine cross slope of bridge)
Column Shape:	$ColumnShape := \text{"Round"}$	(Use "Round" Column Shape)

Pier View:

PierView := "Upstation"

(Use "Upstation" to coincide with load directions calculated herein. Either "Upstation" or "Downstation" can be used, but load directions will need to coincide with Pier View chosen.)

Strut and Tie Model Not Used for Bent Cap Design - box not checked in RCPier

► Expand for Upstation, Downstation and Skew Explanation

B2. Superstr.

Bridge Type:

BridgeType := "Pretensioned Girders"

(Use "Pretensioned Girders" from "Pretensioned Girders" or "CIP PT Bridges".)

Number of Lanes:

N_{lanes} := 1

Beam Height:

H_{beam} := 17in

[Appendix A, sheet no. 8 of 12]

Beam Width:

b_{slab.unit} := 36in

[Appendix A, sheet no. 8 of 12]

Beam Section Area:

A_{beam} := 438.82in²

[From AASHTOWare BrR Model]

Beam Inertia (I_{xx}):

I_{bm_xx} := 13330.10in⁴

[From AASHTOWare BrR Model]

Beam C.G (Y_{cg}):

Y_{bm_cg} := 8.17in

[From AASHTOWare BrR Model]

Barrier/Railing Height:

H_{barr} := 3ft + 0in = 36in

[Appendix A, sheet no. 8 of 12.
(Includes Railing)]

Depth of Deck

d_{slab} = 1.292in

Span Number Rear to
Current Pier:

SpanNumRear := 1

(Use Span 1 & Bent 2 to design the interior bent since the bridge is symmetric about the midway point of Span 2 and Bent 2 & 3 have the same EL from the bulkhead cap.)

Curb to Curb Distance:

Dist_{BtoB} := 14ft

(Use Clear Roadway width per Phase 1 of the Construction Sequence. See sheet 7 of 12 of Repair Plans)

Deck Offset:

Offset_{deck} := -8.0ft

(Offset between center of the deck and center of the Pier cap; (+) if on the right of center of Pier cap, (-) otherwise)

Span:

Span 1 L_{span1} = 30ft W_{br} = 34ft

Span 2 L_{span2} = 40ft W_{br} = 34ft

Span 3 L_{span1} = 30ft W_{br} = 34ft

End Bridge W_{br} = 34ft

B3. Cap

Straight Cap Parameters

Cap Length (X):	$L_{\text{cap}} = 34 \text{ ft}$	
Cap Height (Y):	$h_{\text{cap}} = 36 \text{ in}$	
Cap Depth (Z):	$b_{\text{cap}} = 36 \text{ in}$	
Skew Angle (deg.):	$\theta_{\text{skew}} = 0 \text{ deg}$	
Factor for Reduced Moment of Inertia:	$I_{\text{reduce}} := 1$	(No reduction in moment of inertia)
Start Elevation:	$\text{Elev}_{\text{top_cap_start}} := 15.93 \text{ ft}$	(Use Pier 2 top of cap elevation from Asbuilt Plans, sheet no. 6 of 12. Refer to Appendix A)
End Elevation:	$\text{Elev}_{\text{top_cap_end}} := 15.86 \text{ ft}$	(Use Pier 2 top of cap elevation from Asbuilt Plans, sheet no. 6 of 12. Refer to Appendix A)

Square ends of the Bent Cap are used so "Top Offset", "Fillet Radius" and "Chamfer" are not used.



B4. Brng/Grdr

Configuration:	$\text{NumBearings} := \text{"Double"}$	(Select double for simply supported intermediate bent.)
Bearing Line 1 Eccentricity from CL Cap:	$\text{BearingLine} := 0.75 \text{ ft}$	(See Asbuilt Plans, sheet no. 7 of 12; Appendix A)

Bearing Line 1

Choose the "Dimension" button and input the following bearing dimensions

Length of Bearing:	$L_{\text{bearing}} := w_{\text{bp}} = 2 \text{ ft}$
Width of Bearing:	$W_{\text{bearing}} := L_{\text{bp}} = 0.5 \text{ ft}$
Thickness of Bearing:	$t_{\text{bearing}} := h_{\text{bp}} = 0.021 \text{ ft}$
Distance Between Edge of Cap and Centerline of Slab Unit:	$\text{Dist}_{\text{cap_beam}} := 1.50 \text{ ft}$
Spacing of Beams:	$\text{Beam}_{\text{spacing}} := 3.0 \text{ ft}$

Cross Slope of Bridge:

CS := 0.016

Distance From:

DistanceFrom := "Cap Left End"

Bearing Point Input
for Bearing Line 1:

Bearing Points			
Line	Point	From	Dist.
1	1	Left	1.50
	2	Left	4.50
	3	Left	7.50
	4	Left	10.50
	5	Left	13.50
	6	Left	16.50
	7	Left	19.50
	8	Left	22.50
	9	Left	25.50
	10	Left	28.50
	11	Left	32.50

Bearing Line 2

Bearing Line 2
Eccentricity from CL Cap:

BearingLine := -0.75ft

(See Asbuilt Plans, sheet no. 7 of 12; Appendix A)

Choose the "Dimension" button and input the following bearing dimensions

Distance Between Edge
of Cap and Centerline of
Beam

Dist_{cap_beam} := 1.50 · ft

Spacing of Beams:

Beam_{spacing} := 3.0 · ft

Distance From:

DistanceFrom := "Cap Left End"

Bearing Point Input:

Bearing Points			
Line	Point	From	Dist.
2	1	Left	1.50
	2	Left	4.50
	3	Left	7.50
	4	Left	10.50
	5	Left	13.50
	6	Left	16.50
	7	Left	19.50
	8	Left	22.50
	9	Left	25.50
	10	Left	28.50
	11	Left	32.50

B5. Material

Concrete Strength

[From As-Built Plans, sheet no. 5 of 12]

Cap: $f_{c_cap} := 5000 \text{ psi}$

Pile: $f_{c_pile} := 5000 \text{ psi}$

Footing: $f_{c_footing} := 5000 \text{ psi}$

Concrete Density

Cap: (Use for All)

Pile: $w_c = 150 \text{ pcf}$

[SDG Table 2.2-1]

Footing:

Concrete Modulus of Elasticity

[AASHTO LRFD 5.4.2.4 & SDG 1.4.1.A]

Cap: $E_{c_cap} := 120000 \cdot 1.0 \cdot 0.145^2 \cdot \left(\frac{f_{c_cap}}{\text{ksi}} \right)^{0.33} \cdot \text{ksi} = 4291 \cdot \text{ksi}$

Pile: $E_{c_pile} := 120000 \cdot 1.0 \cdot 0.145^2 \cdot \left(\frac{f_{c_pile}}{\text{ksi}} \right)^{0.33} \cdot \text{ksi} = 4291 \cdot \text{ksi}$

Footing: $E_{c_footing} := 120000 \cdot 1.0 \cdot 0.145^2 \cdot \left(\frac{f_{c_footing}}{\text{ksi}} \right)^{0.33} \cdot \text{ksi} = 4291 \cdot \text{ksi}$

Steel Yield Strength

[SDG 1.4.1.B]

Cap (flex):

Cap (shear): $f_y := 60 \text{ ksi}$ (Use for all elements)

Pile:

Footing:

Concrete Type

Cap: $\text{ConcreteType} := \text{"Normal"}$ (Use for all elements from "Normal",
"Sand-lightweight", "All-lightweight".)

Pile:

Footing:

B6. Str. Model**Additional Check Points**

Add any additional points needed for checking moment and shear.

Hinge

No hinges will be added to the cap to. Design as a continuous beam.

C. Loads Tab (RCPIer)**C1. DC Loads**

Since bridge is simply supported, intermediate Piers 2 & 3 will experience identical dead loads.

Dead Loads for all slab units were determined from the AASHTOWare Load Rating Analysis model, and reactions along each bearing line were inputted at each bearing point for Spans 1 and 2, respectively (similar for Pier 3). Refer to "Summary of Dead Load Shear Reactions" from AASHTOWare BrR software for the reaction values inputted at the bearing points.

Dead Load from Temporary Type K barrier is assumed to be transferred to the bent through the bearing point at slab units 1-6 and 2-6 and the support reactions computed below will be added to the Assume Weight

DC of a single Temporary
Type K Barrier unit:

$$W_{\text{typeK}} := 2.7 \text{ ton} = 5.952 \cdot \text{kip}$$

[FDOT Standard Plans Index no. 102-110]

Length of a single Temporary
Type K Barrier unit:

$$L_{\text{typeK}} := 12.5 \text{ ft}$$

[FDOT Standard Plans Index no. 102-110]

Distributed DL from Type K
Barrier:

$$w_{\text{typeK}} := \frac{W_{\text{typeK}}}{L_{\text{typeK}}} = 0.476 \cdot \frac{\text{kip}}{\text{ft}}$$

[FDOT Standard Plans Index no. 102-110]

Estimated DC reaction of
Type K Barrier from Span 1:

$$P_{\text{typeK_sp1}} := \frac{-w_{\text{typeK}} \cdot L_{\text{span1}}}{2} = -7.143 \cdot \text{kip}$$

Estimated DC reaction of
Type K Barrier from Span 2:

$$P_{\text{typeK_sp2}} := \frac{-w_{\text{typeK}} \cdot L_{\text{span2}}}{2} = -9.524 \cdot \text{kip}$$

DC Reactions Input
at Bearing Points
for Bearing Line 1:

DL Reactions at Bearing Points			
Line	Bearing Point #	Dir	Load (kips)
1	1	Y	-13.89
	2	Y	-7.21
	3	Y	-7.21
	4	Y	-7.21
	5	Y	-7.21
	6	Y	-14.35
	7	Y	-7.21
	8	Y	-7.21
	9	Y	-7.21
	10	Y	-11.25
	11	Y	-15.36
* Dead Load from Superstructure components and attachments (including temporary Type K Barrier)			

DC Reactions Input
at Bearing Points
for Bearing Line 2:

DL Reactions at Bearing Points			
Line	Bearing Point #	Dir	Load (kips)
2	1	Y	-18.71
	2	Y	-9.62
	3	Y	-9.62
	4	Y	-9.62
	5	Y	-9.62
	6	Y	-19.14
	7	Y	-9.62
	8	Y	-9.62
	9	Y	-9.62
	10	Y	-15.12
	11	Y	-20.72
* Dead Load from Superstructure components and attachments (including temporary Type K Barrier)			

C2. DW Loads

Per LBC reference content, "The Load from the slab, barriers and wearing surface is distributed among bearings based on each bearing/girder tributary width."

Dead Load from wearing surface is assuming an equivalent tributary load per foot of based on the average thickness of the asphalt overlay corresponding to each span as per sheet no. 7 of 12 of Asbuilt Plans (see Appendix A).

Density of Asphalt:

$w_{aws} := 145 \text{pcf}$

[FDOT Standard Plans Index no. 102-110]

Average Thickness of
Wearing Surface along
Span 1 or 3:

$$t_{avg_span1} := 1.167\text{in}$$

Average Thickness of
Wearing Surface along
Span 2:

$$t_{avg_span2} := 1.292\text{in}$$

Tributary width for
interior Slab Units:

$$b_{trib_int} := b_{slab.unit} = 3\text{ft}$$

Tributary width for
interior Slab Unit 10:

$$b_{trib_int.10} := 1\text{ft}$$

Tributary width for
exterior Slab Unit 1:

$$b_{trib_int.1} := 1\text{ft}$$

Distributed DW on typical
interior Slab Units along
Span 1 or 3:

$$w_{DW_span1_int} := t_{avg_span1} \cdot w_{aws} \cdot b_{trib_int} = 0.0423 \cdot \text{klf}$$

Distributed DW on typical
interior Slab Units along
Span 2:

$$w_{DW_span2_int} := t_{avg_span2} \cdot w_{aws} \cdot b_{trib_int} = 0.0468 \cdot \text{klf}$$

Distributed DW on interior
Slab Unit 10 along Span 1
or 3:

$$w_{DW_span1_int.10} := t_{avg_span1} \cdot w_{aws} \cdot b_{trib_int.10} = 0.0141 \cdot \text{klf}$$

Distributed DW on interior
Slab Unit 10 along Span 2:

$$w_{DW_span2_int.10} := t_{avg_span2} \cdot w_{aws} \cdot b_{trib_int.10} = 0.0156 \cdot \text{klf}$$

Distributed DW on exterior
Slab Unit 1 along Span 1
or 3:

$$w_{DW_span1_ext.1} := t_{avg_span1} \cdot w_{aws} \cdot b_{trib_int.1} = 0.0141 \cdot \text{klf}$$

Distributed DW on exterior
Slab Unit 1 along Span 2:

$$w_{DW_span2_ext.1} := t_{avg_span2} \cdot w_{aws} \cdot b_{trib_int.1} = 0.0156 \cdot \text{klf}$$

► DW Bearing Reactions

DW Reactions Input
at Bearing Points for
Bearing Line 1:

DL Reactions at Bearing Points			
Line	Bearing Point #	Dir	Load (kips)
1	1	Y	-0.21
	2	Y	-0.63
	3	Y	-0.63
	4	Y	-0.63
	5	Y	-0.63
	6	Y	-0.63
	7	Y	-0.63
	8	Y	-0.63
	9	Y	-0.63
	10	Y	-0.21
	11	Y	0.00
* Dead Load from Superstructure components and attachments (including temporary Type K Barrier)			

DW Reactions Input at
Bearing Points for
Bearing Line 2:

DL Reactions at Bearing Points			
Line	Bearing Point #	Dir	Load (kips)
2	1	Y	-0.31
	2	Y	-0.94
	3	Y	-0.94
	4	Y	-0.94
	5	Y	-0.94
	6	Y	-0.94
	7	Y	-0.94
	8	Y	-0.94
	9	Y	-0.94
	10	Y	-0.31
	11	Y	0.00
* Dead Load from Superstructure components and attachments (including temporary Type K Barrier)			

C3. EH Loads (End Bent Only)

No EH loads on Interior Bent.

C4. LL & BR Loads

Longitudinal Reaction

Use "Compute Simply Supported Beam Reaction" since the superstructure is simply supported.

Per AASHTO LRFD 3.6.1.3 (Use the following load truck combinations):

- Use "Design Truck"
- Use "Design Truck + Lane Load"
- Use "Design Tandem + Lane Load"
- Do not use "Two Design Trucks + Lane Load". These truck loads could control for longer continuous spans. This live load case is used for negative moment between points of contraflexure and reactions at interior piers only.
- Do not use "Two Design Tandem + Lane Load" per AASHTO C3.6.1.3.1 this case will only be investigated if multiple lanes of heavier versions of "low boy" type vehicles are considered probable.

Transverse Positioning

Loaded Lanes: Use "All combinations" to check all the different combinations of loaded lanes.

Live Load Positions: Use "Variable Spacing" with a 1ft minimum spacing between positions. This live load positioning places a wheel over each bearing point then adds additional trucks from that position. It will then repeat a similar process for each bearing.

Longitudinal Force or BR Loads

[AASHTO LRFD 3.6.4]

No Breaking (BR) Loads will be considered with the live loads.

C5. Centrifugal Force or CE Loads

[AASHTO LRFD 3.6.3]

Since the bridge is a straight structure, the centrifugal force effects are not necessary. Do not check "Generate Centrifugal Load Cases also".

C6. Water Loads or WA Loads

[AASHTO LRFD 3.7]

Since the Column axial loads are considered in this model, No Water Loads will be applied.

D. Analysis Tab - A/D Parameters Button - Analysis/Design Parameters LRFD

D1. Resistance Factors

- Use "Phi as per 2006 classification" per *AASHTO LRFD 5.5.4.2*.
- Use the program defaults for "Modulus of Rupture" see *AASHTO LRFD 5.4.2.6*.
- Use the program defaults for Strain T: 60ksi - Comp 0.002 and Tension 0.005. These ratios come from *AASHTO LRFD 5.7.2.1* and *AASHTO LRFD Figure C5.7.2.1-1*. They use a compression controlled strain limits of 0.002 and tension controlled strain limit of .005 and similar triangles as shown in the figure.

D2. Impact and Reduction

- Use the program defaults for Dynamic Load Allowance (IM) since the cap, columns, and footing will have Truck + IM for an intermediate bent. **(Note: Even though there is no footing, there must be impact on the footing to get impact on the piles for a bent.)** The lane will not have IM. *[AASHTO LRFD 3.6.2.1]*
- Use program defaults for Multiple Presence Factors *[AASHTO LRFD Table 3.6.1.1.2-1]*.

D3. Crack Control

- Use the the Crack Control Criteria "Current LRFD" per *AASHTO LRFD 5.7.3.4* with the following exposure factors:
 1. Cap - 0.75
 2. Column - 0.75
 3. Footing - 1.0Use a Class 2 exposure condition since the column (pile) and cap are exposed to water *[See AASHTO LRFD 5.7.3.4 commentary and SDG 3.10.E]*.
- Use the program default for Fatigue "ff term" = 24 per *AASHTO LRFD 5.5.3.2-1*.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 1

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 1-1									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	6.47	0.25	0.49	2.09	4.59	0	7.21	6.68	13.89
0.5	6.24	0.24	0.49	2.02	4.42	0	6.97	6.44	13.41
0.5	6.24	0.24	0.16	2.02	4.42	0	6.64	6.44	13.08
1.69	5.69	0.22	0.16	1.84	4.04	0	6.07	5.88	11.95
2.83	5.17	0.2	0.16	1.67	3.67	0	5.53	5.34	10.87
5.66	3.88	0.15	0.16	1.26	2.75	0	4.19	4.01	8.20
6.75	3.38	0.13	0.16	1.09	2.4	0	3.67	3.49	7.16
6.75	3.38	0.13	0	1.09	2.4	0	3.51	3.49	7.00
8.49	2.59	0.1	0	0.84	1.83	0	2.69	2.67	5.36
11.32	1.29	0.05	0	0.42	0.92	0	1.34	1.34	2.68
14.15	0	0	0	0	0	0	0	0	0.00
16.98	-1.29	-0.05	0	-0.42	-0.92	0	-1.34	-1.34	-2.68
19.8	-2.59	-0.1	0	-0.84	-1.83	0	-2.69	-2.67	-5.36
21.75	-3.48	-0.13	0	-1.13	-2.47	0	-3.61	-3.6	-7.21
21.75	-3.48	-0.13	-0.17	-1.13	-2.47	0	-3.78	-3.6	-7.38
22.63	-3.88	-0.15	-0.17	-1.26	-2.75	0	-4.2	-4.01	-8.21
25.46	-5.17	-0.2	-0.17	-1.67	-3.67	0	-5.54	-5.34	-10.88
26.81	-5.79	-0.22	-0.17	-1.87	-4.11	0	-6.18	-5.98	-12.16
28	-6.33	-0.24	-0.17	-2.05	-4.49	0	-6.74	-6.54	-13.28
28	-6.33	-0.24	-0.49	-2.05	-4.49	0	-7.06	-6.54	-13.60
28.29	-6.47	-0.25	-0.49	-2.09	-4.59	0	-7.21	-6.68	-13.89

* Dead Load (Support) Bearing Reactions



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 1

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 1-8 **									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	6.47	0.25	0.49	0	0	0	7.21	0	7.21
0.5	6.24	0.24	0.49	0	0	0	6.97	0	6.97
0.5	6.24	0.24	0.16	0	0	0	6.64	0	6.64
1.69	5.69	0.22	0.16	0	0	0	6.07	0	6.07
2.83	5.17	0.2	0.16	0	0	0	5.53	0	5.53
5.66	3.88	0.15	0.16	0	0	0	4.19	0	4.19
6.75	3.38	0.13	0.16	0	0	0	3.67	0	3.67
6.75	3.38	0.13	0	0	0	0	3.51	0	3.51
8.49	2.59	0.1	0	0	0	0	2.69	0	2.69
11.32	1.29	0.05	0	0	0	0	1.34	0	1.34
14.15	0	0	0	0	0	0	0	0	0.00
16.98	-1.29	-0.05	0	0	0	0	-1.34	0	-1.34
19.8	-2.59	-0.1	0	0	0	0	-2.69	0	-2.69
21.75	-3.48	-0.13	0	0	0	0	-3.61	0	-3.61
21.75	-3.48	-0.13	-0.17	0	0	0	-3.78	0	-3.78
22.63	-3.88	-0.15	-0.17	0	0	0	-4.20	0	-4.20
25.46	-5.17	-0.2	-0.17	0	0	0	-5.54	0	-5.54
26.81	-5.79	-0.22	-0.17	0	0	0	-6.18	0	-6.18
28	-6.33	-0.24	-0.17	0	0	0	-6.74	0	-6.74
28	-6.33	-0.24	-0.49	0	0	0	-7.06	0	-7.06
28.29	-6.47	-0.25	-0.49	0	0	0	-7.21	0	-7.21

* Dead Load (Support) Bearing Reactions

** Slab Units 1-2 to 1-7 and 1-9 are similar.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 1

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 1-10									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Total DC Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	6.47	0.25	0.49	0	4.04	0	7.21	4.04	11.25
0.5	6.24	0.24	0.49	0	3.9	0	6.97	3.9	10.87
0.5	6.24	0.24	0.16	0	3.9	0	6.64	3.9	10.54
1.69	5.69	0.22	0.16	0	3.56	0	6.07	3.56	9.63
2.83	5.17	0.2	0.16	0	3.23	0	5.53	3.23	8.76
5.66	3.88	0.15	0.16	0	2.42	0	4.19	2.42	6.61
6.75	3.38	0.13	0.16	0	2.11	0	3.67	2.11	5.78
6.75	3.38	0.13	0	0	2.11	0	3.51	2.11	5.62
8.49	2.59	0.1	0	0	1.62	0	2.69	1.62	4.31
11.32	1.29	0.05	0	0	0.81	0	1.34	0.81	2.15
14.15	0	0	0	0	0	0	0	0	0.00
16.98	-1.29	-0.05	0	0	-0.81	0	-1.34	-0.81	-2.15
19.8	-2.59	-0.1	0	0	-1.62	0	-2.69	-1.62	-4.31
21.75	-3.48	-0.13	0	0	-2.17	0	-3.61	-2.17	-5.78
21.75	-3.48	-0.13	-0.17	0	-2.17	0	-3.78	-2.17	-5.95
22.63	-3.88	-0.15	-0.17	0	-2.42	0	-4.2	-2.42	-6.62
25.46	-5.17	-0.2	-0.17	0	-3.23	0	-5.54	-3.23	-8.77
26.81	-5.79	-0.22	-0.17	0	-3.62	0	-6.18	-3.62	-9.80
28	-6.33	-0.24	-0.17	0	-3.96	0	-6.74	-3.96	-10.70
28	-6.33	-0.24	-0.49	0	-3.96	0	-7.06	-3.96	-11.02
28.29	-6.47	-0.25	-0.49	0	-4.04	0	-7.21	-4.04	-11.25

* Dead Load (Support) Bearing Reactions



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 1

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 1-11									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	6.47	0.25	0.49	2.09	6.06	0	7.21	8.15	15.36
0.5	6.24	0.24	0.49	2.02	5.85	0	6.97	7.87	14.84
0.5	6.24	0.24	0.16	2.02	5.85	0	6.64	7.87	14.51
1.69	5.69	0.22	0.16	1.84	5.34	0	6.07	7.18	13.25
2.83	5.17	0.2	0.16	1.67	4.85	0	5.53	6.52	12.05
5.66	3.88	0.15	0.16	1.26	3.64	0	4.19	4.9	9.09
6.75	3.38	0.13	0.16	1.09	3.17	0	3.67	4.26	7.93
6.75	3.38	0.13	0	1.09	3.17	0	3.51	4.26	7.77
8.49	2.59	0.1	0	0.84	2.42	0	2.69	3.26	5.95
11.32	1.29	0.05	0	0.42	1.21	0	1.34	1.63	2.97
14.15	0	0	0	0	0	0	0	0	0.00
16.98	-1.29	-0.05	0	-0.42	-1.21	0	-1.34	-1.63	-2.97
19.8	-2.59	-0.1	0	-0.84	-2.42	0	-2.69	-3.26	-5.95
21.75	-3.48	-0.13	0	-1.13	-3.26	0	-3.61	-4.39	-8.00
21.75	-3.48	-0.13	-0.17	-1.13	-3.26	0	-3.78	-4.39	-8.17
22.63	-3.88	-0.15	-0.17	-1.26	-3.64	0	-4.2	-4.9	-9.10
25.46	-5.17	-0.2	-0.17	-1.67	-4.85	0	-5.54	-6.52	-12.06
26.81	-5.79	-0.22	-0.17	-1.87	-5.43	0	-6.18	-7.3	-13.48
28	-6.33	-0.24	-0.17	-2.05	-5.94	0	-6.74	-7.99	-14.73
28	-6.33	-0.24	-0.49	-2.05	-5.94	0	-7.06	-7.99	-15.05
28.29	-6.47	-0.25	-0.49	-2.09	-6.06	0	-7.21	-8.15	-15.36

* Dead Load (Support) Bearing Reactions



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 2

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 2-1									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	8.8	0.33	0.49	2.85	6.24	0	9.62	9.09	18.71
0.29	8.67	0.33	0.49	2.81	6.15	0	9.49	8.96	18.45
0.29	8.67	0.33	0.16	2.81	6.15	0	9.16	8.96	18.12
1.48	8.12	0.31	0.16	2.63	5.76	0	8.59	8.39	16.98
3.85	7.04	0.27	0.16	2.28	4.99	0	7.47	7.27	14.74
7.7	5.28	0.2	0.16	1.71	3.74	0	5.64	5.45	11.09
9.25	4.57	0.17	0.16	1.48	3.24	0	4.9	4.72	9.62
9.25	4.57	0.17	0	1.48	3.24	0	4.74	4.72	9.46
11.55	3.52	0.13	0	1.14	2.5	0	3.65	3.64	7.29
15.4	1.76	0.07	0	0.57	1.25	0	1.83	1.82	3.65
19.25	0	0	0	0	0	0	0	0	0.00
23.1	-1.76	-0.07	0	-0.57	-1.25	0	-1.83	-1.82	-3.65
26.95	-3.52	-0.13	0	-1.14	-2.5	0	-3.65	-3.64	-7.29
29.25	-4.57	-0.17	0	-1.48	-3.24	0	-4.74	-4.72	-9.46
29.25	-4.57	-0.17	-0.16	-1.48	-3.24	0	-4.9	-4.72	-9.62
30.8	-5.28	-0.2	-0.16	-1.71	-3.74	0	-5.64	-5.45	-11.09
34.65	-7.04	-0.27	-0.16	-2.28	-4.99	0	-7.47	-7.27	-14.74
37.02	-8.12	-0.31	-0.16	-2.63	-5.76	0	-8.59	-8.39	-16.98
38.21	-8.67	-0.33	-0.16	-2.81	-6.15	0	-9.16	-8.96	-18.12
38.21	-8.67	-0.33	-0.49	-2.81	-6.15	0	-9.49	-8.96	-18.45
38.5	-8.8	-0.33	-0.49	-2.85	-6.24	0	-9.62	-9.09	-18.71

* Dead Load (Support) Bearing Reactions



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BRR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 2

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BRR - INT SLAB UNIT 2-8 ***									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Total DC Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	8.8	0.33	0.49	0	0	0	9.62	0	9.62
0.29	8.67	0.33	0.49	0	0	0	9.49	0	9.49
0.29	8.67	0.33	0.16	0	0	0	9.16	0	9.16
1.48	8.12	0.31	0.16	0	0	0	8.59	0	8.59
3.85	7.04	0.27	0.16	0	0	0	7.47	0	7.47
7.7	5.28	0.2	0.16	0	0	0	5.64	0	5.64
9.25	4.57	0.17	0.16	0	0	0	4.9	0	4.90
9.25	4.57	0.17	0	0	0	0	4.74	0	4.74
11.55	3.52	0.13	0	0	0	0	3.65	0	3.65
15.4	1.76	0.07	0	0	0	0	1.83	0	1.83
19.25	0	0	0	0	0	0	0	0	0.00
23.1	-1.76	-0.07	0	0	0	0	-1.83	0	-1.83
26.95	-3.52	-0.13	0	0	0	0	-3.65	0	-3.65
29.25	-4.57	-0.17	0	0	0	0	-4.74	0	-4.74
29.25	-4.57	-0.17	-0.16	0	0	0	-4.9	0	-4.90
30.8	-5.28	-0.2	-0.16	0	0	0	-5.64	0	-5.64
34.65	-7.04	-0.27	-0.16	0	0	0	-7.47	0	-7.47
37.02	-8.12	-0.31	-0.16	0	0	0	-8.59	0	-8.59
38.21	-8.67	-0.33	-0.16	0	0	0	-9.16	0	-9.16
38.21	-8.67	-0.33	-0.49	0	0	0	-9.49	0	-9.49
38.5	-8.8	-0.33	-0.49	0	0	0	-9.62	0	-9.62

* Dead Load (Support) Bearing Reactions

*** Slab Units 2-2 to 2-7 and 2-9 are similar.



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 2

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 2-10									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	8.8	0.33	0.49	0	5.5	0	9.62	5.5	15.12
0.29	8.67	0.33	0.49	0	5.41	0	9.49	5.41	14.90
0.29	8.67	0.33	0.16	0	5.41	0	9.16	5.41	14.57
1.48	8.12	0.31	0.16	0	5.08	0	8.59	5.08	13.67
3.85	7.04	0.27	0.16	0	4.4	0	7.47	4.4	11.87
7.7	5.28	0.2	0.16	0	3.3	0	5.64	3.3	8.94
9.25	4.57	0.17	0.16	0	2.86	0	4.9	2.86	7.76
9.25	4.57	0.17	0	0	2.86	0	4.74	2.86	7.60
11.55	3.52	0.13	0	0	2.2	0	3.65	2.2	5.85
15.4	1.76	0.07	0	0	1.1	0	1.83	1.1	2.93
19.25	0	0	0	0	0	0	0	0	0.00
23.1	-1.76	-0.07	0	0	-1.1	0	-1.83	-1.1	-2.93
26.95	-3.52	-0.13	0	0	-2.2	0	-3.65	-2.2	-5.85
29.25	-4.57	-0.17	0	0	-2.86	0	-4.74	-2.86	-7.60
29.25	-4.57	-0.17	-0.16	0	-2.86	0	-4.9	-2.86	-7.76
30.8	-5.28	-0.2	-0.16	0	-3.3	0	-5.64	-3.3	-8.94
34.65	-7.04	-0.27	-0.16	0	-4.4	0	-7.47	-4.4	-11.87
37.02	-8.12	-0.31	-0.16	0	-5.08	0	-8.59	-5.08	-13.67
38.21	-8.67	-0.33	-0.16	0	-5.41	0	-9.16	-5.41	-14.57
38.21	-8.67	-0.33	-0.49	0	-5.41	0	-9.49	-5.41	-14.90
38.5	-8.8	-0.33	-0.49	0	-5.5	0	-9.62	-5.5	-15.12

* Dead Load (Support) Bearing Reactions



Project #: D210107FL00.00
Designed By: YRA
Design Date: Jan-22
Checked By: MAP
Check Date: Jan-22

Matheson Hmk Road over Matheson Hammock Canal
SUMMARY OF DEAD LOAD SHEAR REACTIONS

Note: The following Dead Load Shear reactions were extracted from the AASHTOWare BrR Rating model. The Slab unit superstructure system is assumed to be simply supported, and the reactions at the begin and end locations along the span represent the support reactions at the bearing points for each slab unit.

SPAN 2

DEAD LOAD SHEAR REACTIONS FROM AASHTOWARE BrR - INT SLAB UNIT 2-11									
Location	Self Weight (Slab Unit) (KIP-FT)	% of DC Slab Unit (KIP-FT)	Self Weight (Interior diagrams) (KIP-FT)	DC - Railing (KIP-FT)	DC - Curb/ Sidewalk (KIP-FT)	PS Transfer Forces (KIP-FT)	Selfweight of Slab Unit alone (per Slab Unit) (KIP-FT)	Total DC (Railing + Sidewalk) per Slab Unit (KIP-FT)	Total DC per Slab Unit * (KIP-FT)
0	8.8	0.33	0.49	2.85	8.25	0	9.62	11.1	20.72
0.29	8.67	0.33	0.49	2.81	8.12	0	9.49	10.93	20.42
0.29	8.67	0.33	0.16	2.81	8.12	0	9.16	10.93	20.09
1.48	8.12	0.31	0.16	2.63	7.61	0	8.59	10.24	18.83
3.85	7.04	0.27	0.16	2.28	6.6	0	7.47	8.88	16.35
7.7	5.28	0.2	0.16	1.71	4.95	0	5.64	6.66	12.30
9.25	4.57	0.17	0.16	1.48	4.28	0	4.9	5.76	10.66
9.25	4.57	0.17	0	1.48	4.28	0	4.74	5.76	10.50
11.55	3.52	0.13	0	1.14	3.3	0	3.65	4.44	8.09
15.4	1.76	0.07	0	0.57	1.65	0	1.83	2.22	4.05
19.25	0	0	0	0	0	0	0	0	0.00
23.1	-1.76	-0.07	0	-0.57	-1.65	0	-1.83	-2.22	-4.05
26.95	-3.52	-0.13	0	-1.14	-3.3	0	-3.65	-4.44	-8.09
29.25	-4.57	-0.17	0	-1.48	-4.28	0	-4.74	-5.76	-10.50
29.25	-4.57	-0.17	-0.16	-1.48	-4.28	0	-4.9	-5.76	-10.66
30.8	-5.28	-0.2	-0.16	-1.71	-4.95	0	-5.64	-6.66	-12.30
34.65	-7.04	-0.27	-0.16	-2.28	-6.6	0	-7.47	-8.88	-16.35
37.02	-8.12	-0.31	-0.16	-2.63	-7.61	0	-8.59	-10.24	-18.83
38.21	-8.67	-0.33	-0.16	-2.81	-8.12	0	-9.16	-10.93	-20.09
38.21	-8.67	-0.33	-0.49	-2.81	-8.12	0	-9.49	-10.93	-20.42
38.5	-8.8	-0.33	-0.49	-2.85	-8.25	0	-9.62	-11.1	-20.72

* Dead Load (Support) Bearing Reactions



Project #: D210107FL.00
Designed By: YRA
Design Date: Nov-21
Checked By: MAP
Check Date: Dec-21

Matheson Hmk Road over Matheson Hammock Canal

Dead Load Reactions from LBC (RCPIER) Model

LBC (RCPIER) COLUMN TOP LOADS - DC1 Superstructure & Attachments (UNFACTORED)*							
Memb	Node	Fx	Fy	Fz	Mx	My	Mz
1	2	-2.8	-119.4	-0.004246	-13.26	0.04451	-24.5
2	4	2.8	-126.9	0.004246	-13.52	0.04467	23.15

* Includes DL from Temporary Type K barrier.

LBC (RCPIER) COLUMN TOP LOADS - DW1 (UNFACTORED)							
Memb	Node	Fx	Fy	Fz	Mx	My	Mz
1	2	-0.9183	-8.072	0.001265	-1.044	-0.01326	-7.59
2	4	0.9183	-5.528	-0.001265	-0.966	-0.01331	8.041

LBC (RCPIER) COLUMN TOP LOADS - Self (Substructure) (UNFACTORED)							
Memb	Node	Fx	Fy	Fz	Mx	My	Mz
1	2	-1.193	-22.95	0	0	0	-10.16
2	4	1.193	-22.95	0	0	0	10.15

LBC (RCPIER) COLUMN TOP LOADS - TOTAL FACTORED DL							
Memb	Node	Fx	Fy	Fz	Mx	My	Mz
1	2	-6.3687	-190.0455	-0.00341	-18.141	0.035748	-54.71
2	4	4.9113	-195.6045	0.002981	-14.486	0.03136	41.341

X is along the pier (transverse direction)
Z along direction opposite to stationing (longitudinal direction)
Y is vertical



Project #: D210107FL.00
Designed By: YRA
Design Date: Nov-21
Checked By: MAP
Check Date: Dec-21

Matheson Hmk Road over Matheson Hammock Canal

LBC (RCPIER) COLUMN TOP LOADS - FACTORED LOADS WITH IMPACT *

Memb	Node	Fx	Fy(Max/Min)	Fz	Mx	My	Mz
1	2	-4.191	-133.4	-0.00300	-12.62	0.0314	-36.13
		-7.455	-394.3	-0.09098	-3.037	0.9534	-58.06
2	4	4.191	-138.5	0.00300	-12.8	0.0316	35.20
		24.49	-239.9	0.06353	-7.769	0.6684	200.70

* Includes DL from Temporary Type K barrier.

LBC (RCPIER) COLUMN TOP LOADS - SERVICE LOADS WITH IMPACT *

Memb	Node	Fx	Fy(Max/Min)	Fz	Mx	My	Mz
1	2	-4.911	-150.5	-0.00298	-14.31	0.0312	-42.26
		-5.532	-267.2	-0.05302	-5.674	0.5556	-44.17
2	4	4.911	-155.4	0.00298	-14.49	0.0314	41.34
		15.27	-180.7	0.03734	-8.44	0.3928	125.4

* Includes DL from Temporary Type K barrier.

X is along the pier (transverse direction)
Z along direction opposite to stationing (longitudinal direction)
Y is vertical

COLUMN LOADS FOR TEMPORARY SHORING

NOTE: Below is a summary of the maximum reactions computed at the top of the columns at Pier no. 2. Temporary Shoring will be installed at Column no. 2 to accommodate the column repairs. Highlighted in green are the estimated factored and service loads that will be supported by the temporary shoring.

Maximum DL Reactions - Pier Column Loads from RCPier (kips)							
COLUMN TOP DEAD LOADS							
Column No.	Node	Fx (kips)	Fy (kips)	Fz (kips)	Mx (kip-ft)	My (kip-ft)	Mz (kip-ft)
1	2	-7.960875	-191.0	-0.0043	-22.67625	0.044684375	-68.3875
2	4	6.139125	-196.0	0.00373	-18.1075	0.0392	51.67625

Maximum LL Reactions - Pier Column Loads from RCPier (kips)							
COLUMN TOP LL LOADS WITH IMPACT							
Column No.	Node	Fx (kips)	Fy (kips)	Fz (kips)	Mx (kip-ft)	My (kip-ft)	Mz (kip-ft)
1	2	-0.871575	-204.0	-0.0848	18.07325	0.888825625	-1.0575
2	4	19.728325	-44.0	0.05791	8.8895	0.609235	161.08525

Maximum Strength Envelope - Pier Column Loads from RCPier (kips)							
COLUMN TOP LOADS WITH IMPACT							
Memb	Node	Fx (kips)	Fy (kips)	Fz (kips)	Mx (kip-ft)	My (kip-ft)	Mz (kip-ft)
1	2	-8.83245	-394.3	-0.0891	-4.603	0.93351	-69.445
2	4	25.86745	-239.9	0.06163	-9.218	0.648435	212.7615

[Max Fy]

Maximum Service Envelope - Pier Column Loads from RCPier (kips)							
COLUMN TOP LOADS WITH IMPACT							
Memb	Node	Fx (kips)	Fy (kips)	Fz (kips)	Mx (kip-ft)	My (kip-ft)	Mz (kip-ft)
1	2	-6.4503	-267.2	-0.0518	-6.718	0.54234	-51.76
2	4	16.1883	-180.7	0.03608	-9.406	0.37949	133.441

[Max Fy]

Pier 2 RC-Pier Model, looking upstation:



APPENDICES

APPENDIX A – AS-BUILT BRIDGE PLANS

MATHESON HAMMOCK PARK

DADE COUNTY , FLORIDA

BRIDGE AND APPROACH ROAD

As Built Plans

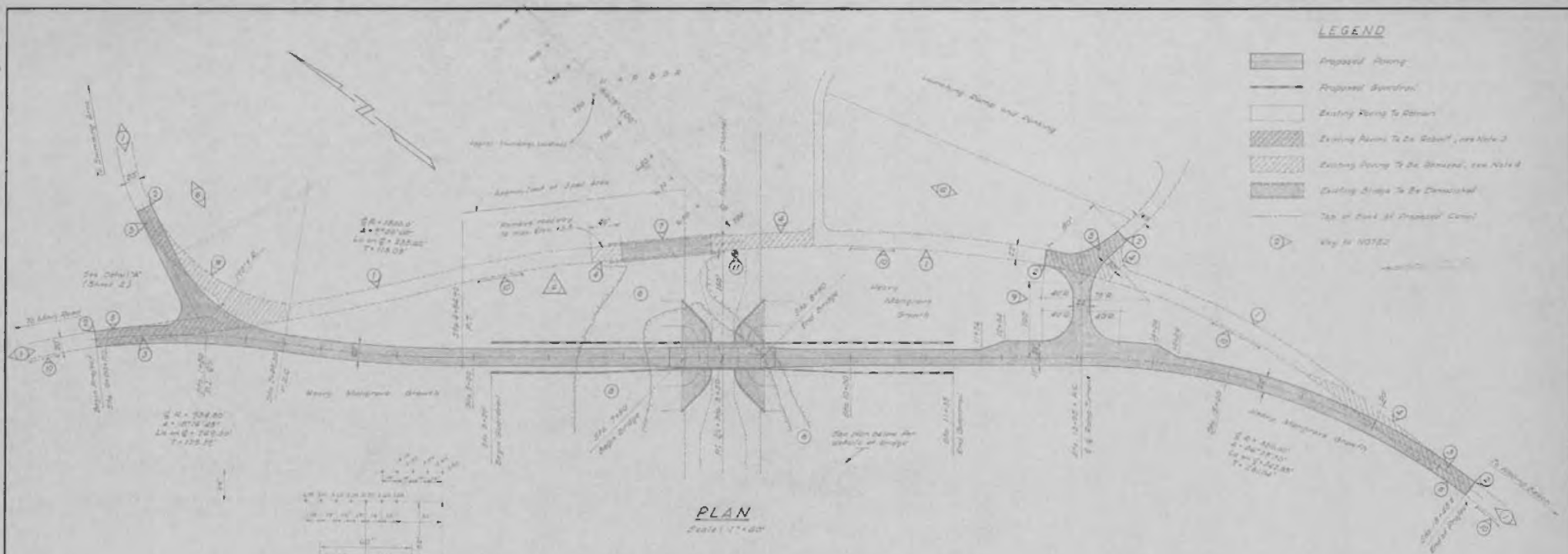


INDEX TO DRAWINGS

Sheet No.	Description
1	APPROACH ROAD PLAN
2	PROFILE
3	CROSS SECTIONS
4	" "
5	BRIDGE PLAN & ELEVATION
6	END & INTERMEDIATE BENTS
7	SUPERSTRUCTURE
8	PRESTRESSED SLAB UNIT
9	APPROACH SLAB - RILING
10	MISCELLANEOUS DETAILS
11	BULKHEAD PLAN
12	" " DETAILS

HART - REYNOLDS & ASSOCIATES, INC.
CONSULTING ENGINEERS
CORAL GABLES, FLORIDA

SITE NUMBER 294



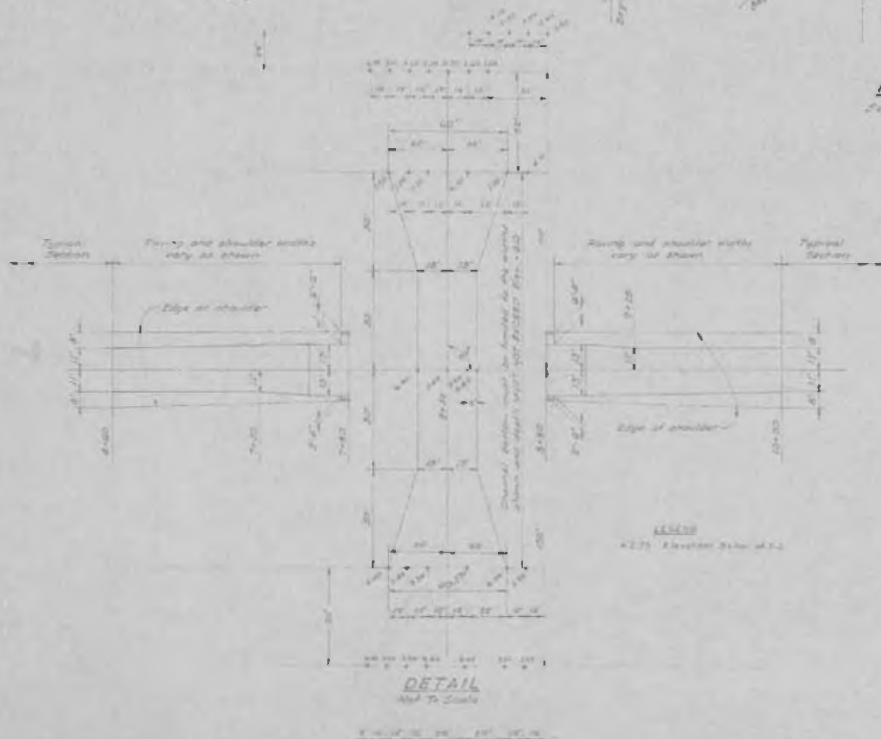
LEGEND

- Proposed Paving
- Proposed Shoulder
- Existing Paving To Remain
- Existing Paving To Be Rebuilt, see Note 3
- Existing Paving To Be Demolished, see Note 4
- Existing Bridge To Be Demolished
- Top of Bank at Proposed Canal
- Key to Notes

PLAN
Scale 1" = 40'

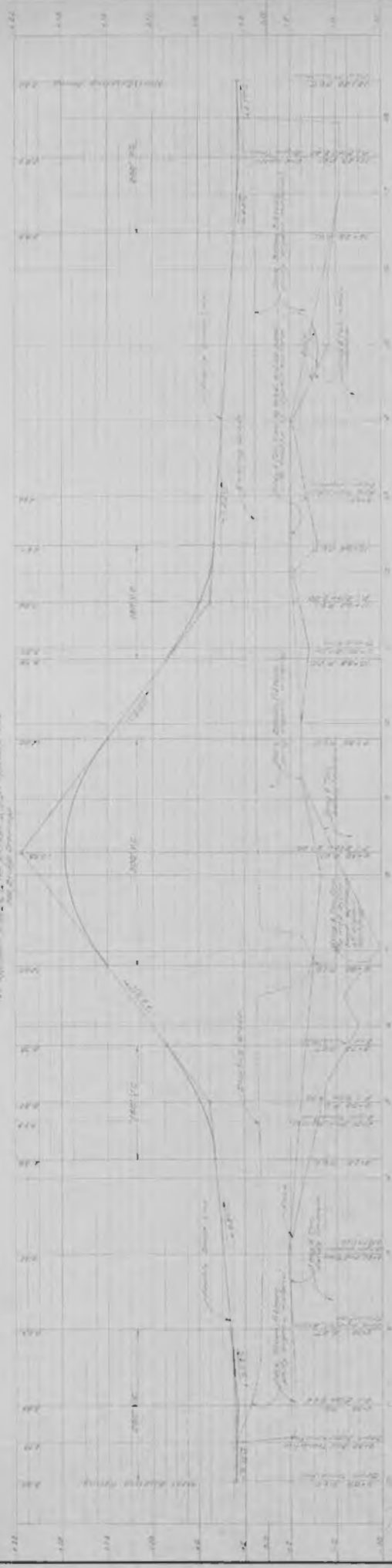
NOTES

- 1 Existing paving to remain.
- 2 Alter existing paving.
- 3 Remove existing base course under proposed paving. Construct new 8" base course with 1" asphalt concrete surface, in section only with typical bridge construction at existing sub-grade.
- 4 Remove existing roadways and embankment to elevation of adjacent ground. Where necessary, construct to project paving, where to road cross section.
- 5 Provide 40' long uniform transition of pavement and shoulder widths, as required to match existing cross section at limits of new construction.
- 6 Spill Area: To be cleared under existing Project. All work required from highway and all materials, except road, resulting from project construction and permanent removal shall be placed in these areas. See specifications.
- 7 Demolish existing bridge. See Specifications.
- 8 Existing drainage channel.
- 9 Turnout: To be graded to provide smooth connection between existing pavement and new road. Engineer will establish grades in field.
- 10 Existing 4" cement-asphalt pipe water main. See Specifications.
- 11 Test boring location. See boring log on sheet 2.

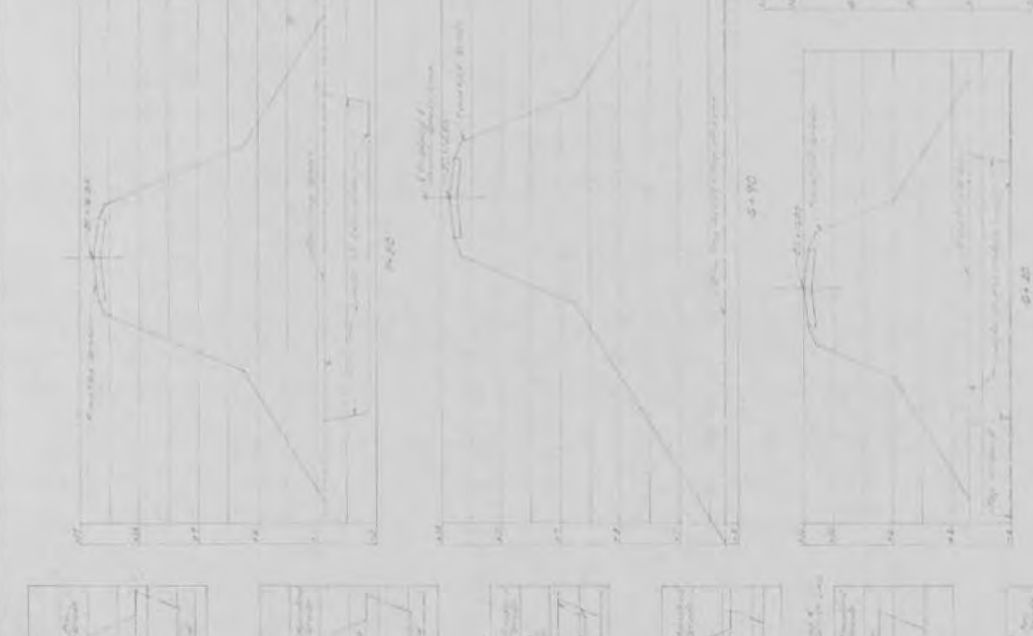
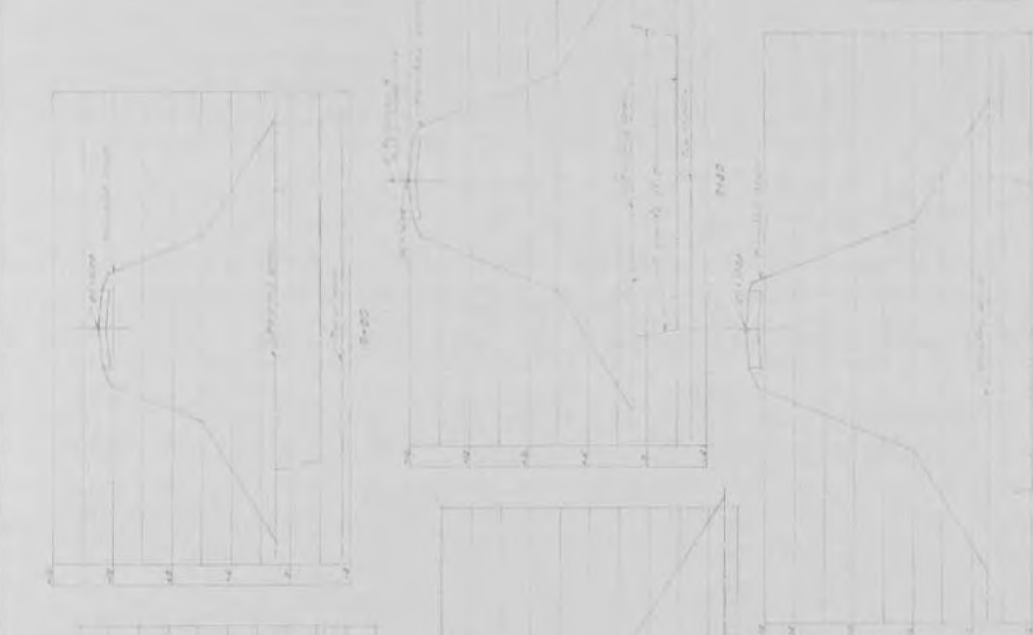
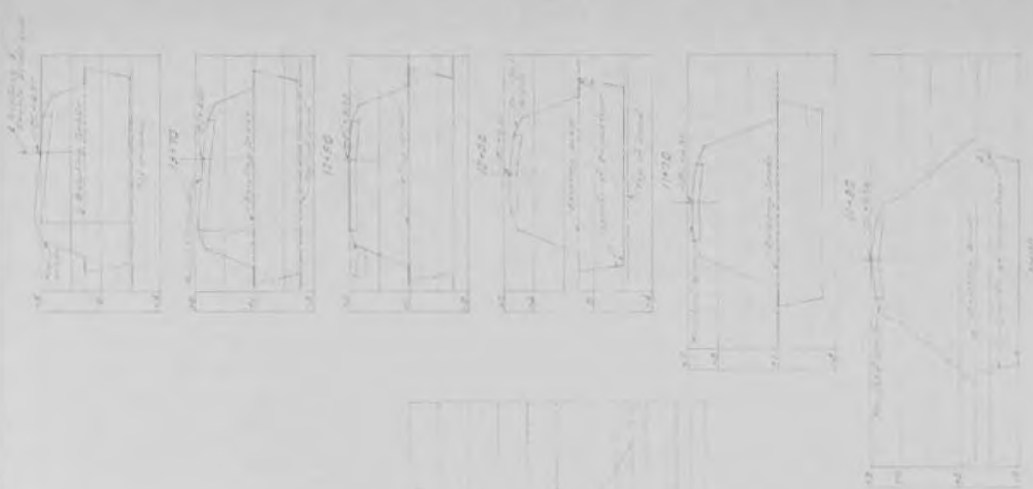


REVISIONS			
Date	By	For	Description
HART-REYNOLDS & ASSOCIATES, INC. CONSULTING ENGINEERS CORAL GABLES, FLORIDA			
MATHESON HAMMOCK PARK DADE COUNTY, FLORIDA BRIDGE AND APPROACH ROAD			
Design: C.L.R.	Drawn: C.L.R.	Checked: R.L.W.	No. 1
Approved: [Signature]	Date: JUNE 1961	Project No: 01-01	
Sheet: 1-40	APPROACH ROAD PLAN		of 2 Sheets

All Elevation refer to Mean Sea Level, U.S.C. & G.S. Datum

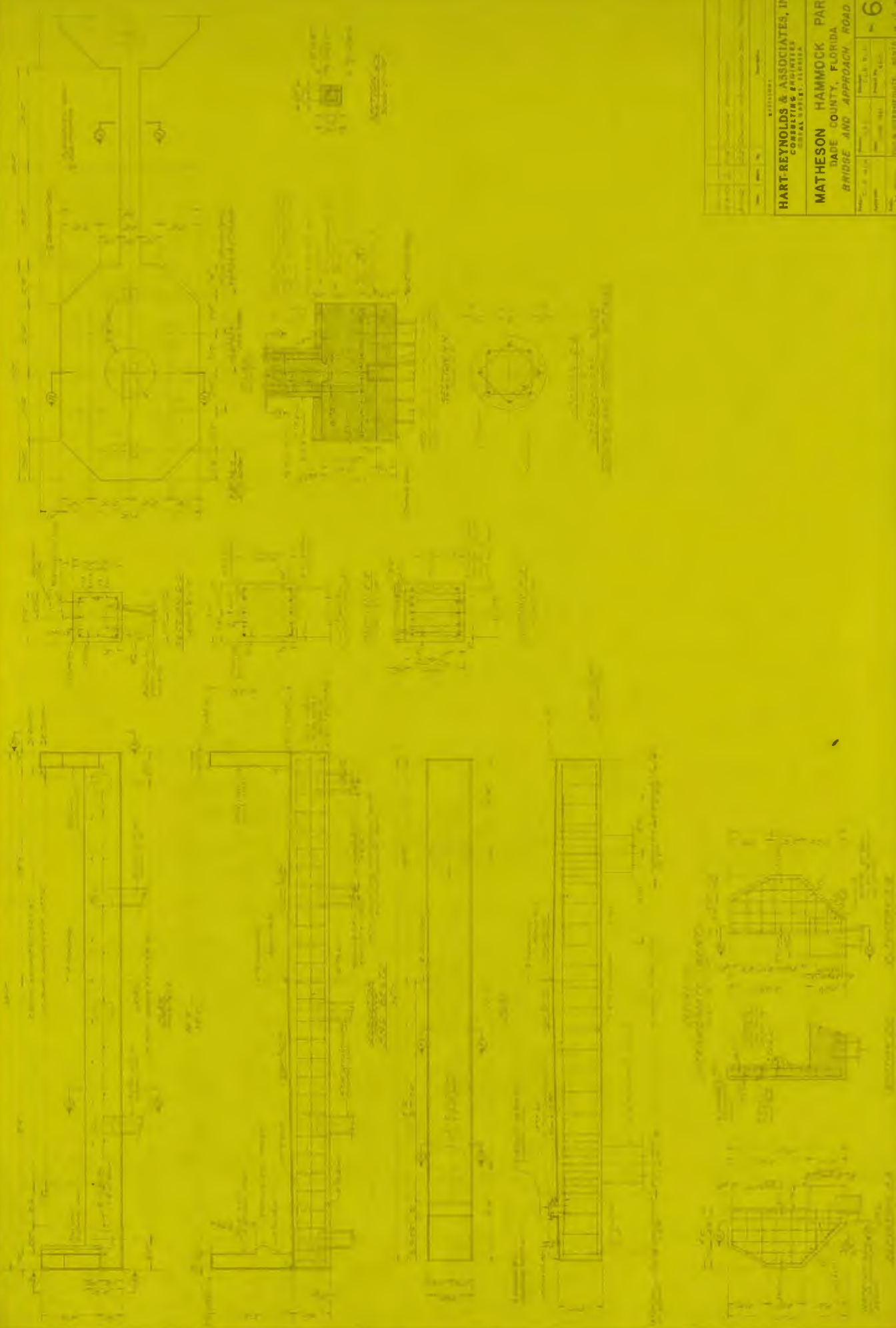


REVISIONS		DATE		BY		CHECKED		APPROVED	
HART-REYNOLDS & ASSOCIATES, INC. CONSULTING ENGINEERS CORAL GABLES, FLORIDA									
MATHESON HAMMOCK PARK DADE COUNTY, FLORIDA BRIDGE AND APPROACH ROAD									
Project No.	100-1000	Sheet No.	2	Date: 10/10/58 Scale: 1" = 10'-0" Profile: 1" = 10'-0"					

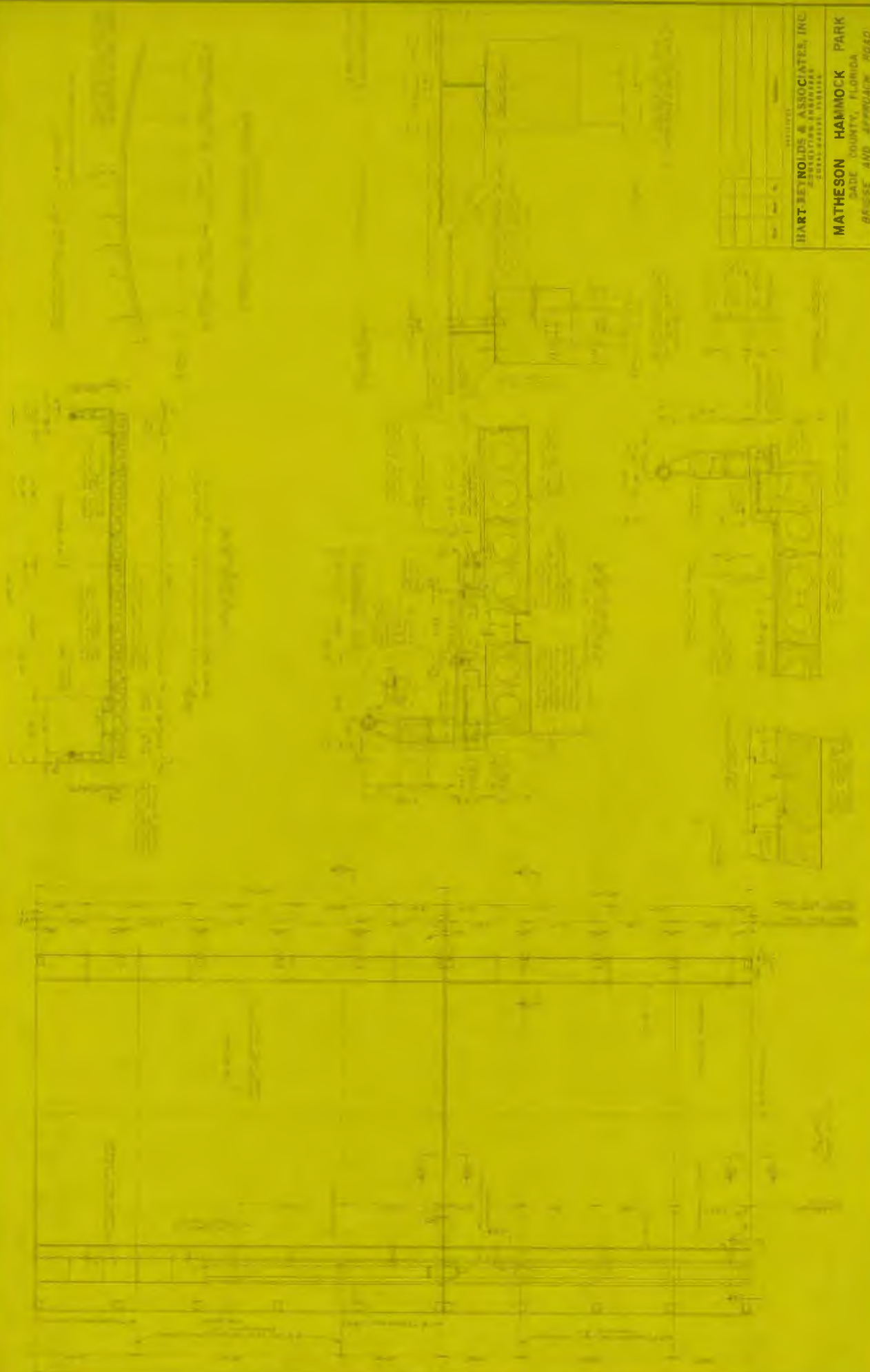


Station	Section	Notes
1+00	1	
1+20	2	
1+40	3	
1+60	4	
1+80	5	
2+00	6	
2+20	7	
2+40	8	
2+60	9	
2+80	10	
3+00	11	
3+20	12	
3+40	13	
3+60	14	
3+80	15	
4+00	16	
4+20	17	
4+40	18	
4+60	19	
4+80	20	
5+00	21	
5+20	22	
5+40	23	
5+60	24	
5+80	25	
6+00	26	
6+20	27	
6+40	28	
6+60	29	
6+80	30	
7+00	31	
7+20	32	
7+40	33	
7+60	34	
7+80	35	
8+00	36	
8+20	37	
8+40	38	
8+60	39	
8+80	40	
9+00	41	
9+20	42	
9+40	43	
9+60	44	
9+80	45	
10+00	46	
10+20	47	
10+40	48	
10+60	49	
10+80	50	

HART-REYNOLDS & ASSOCIATES, INC.
 CIVIL ENGINEERS
 CORAL GABLES, FLORIDA
 MATHESON HAMMOCK PARK
 DADE COUNTY, FLORIDA
 BRIDGE AND APPROACH ROAD
 Station 1+00 to 10+80
 Date: JUNE 1961
 Project No. 61-05
 Sheet 3 of 12
 CROSS SECTIONS
 10+80



REVISIONS		DATE	BY	APP'D
1	AS SHOWN			
HART-REYNOLDS & ASSOCIATES, INC.				
CONSULTING ENGINEERS				
1001 N. W. 10th St., Miami, Florida				
MATHESON HAMMOCK PARK				
DADE COUNTY, FLORIDA				
BRIDGE AND APPROACH ROAD				
Project No.	11	Sheet No.	6	of 6
Scale	1" = 10'	Section Scale	1" = 10'	
Drawn by	J. L. Smith	Checked by	J. L. Smith	
Engineer	J. L. Smith	Approved by	J. L. Smith	



HART REYNOLDS & ASSOCIATES, INC.
 REGISTERED ENGINEERS
 CIVIL ENGINEERS

MATHESON HAMMOCK PARK
 BADE COUNTY, FLORIDA
 BRIDGE AND APPROACH ROAD

DATE	10-1-60	BY	J. H. H.
CHECKED		DATE	
APPROVED		DATE	
SCALE	1" = 40'	NO. OF SHEETS	7



HART REYNOLDS & ASSOCIATES, INC. CIVIL ENGINEERS 1000 N. W. 10th Ave., Suite 1000 Fort Lauderdale, Florida 33304	
PROJECT: MATHESON HAMMOCK PARK LOCATION: DADE COUNTY, FLORIDA ADDRESS: BRIDGE AND APPROACH ROAD	
SHEET NO. 8	TOTAL SHEETS 8



A



REMARKS: SEE SHEET 8

DATE	NO.	REVISION
HART-REYNOLDS & ASSOCIATES INC. CONSULTING ENGINEERS CORAL GABLES, FLORIDA		
MATHESON HAMMOCK PARK DADE COUNTY, FLORIDA BRIDGE AND APPROACH ROAD		
DESIGNED BY	CHECKED BY	APPROVED BY
SHEET NO. 9		TOTAL SHEETS 10

[illegible]



PLAN OF BRIDGE AND APPROACH ROAD

Station	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
Station	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
Station	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100

1. ALL DIMENSIONS ARE IN FEET
2. ALL DIMENSIONS ARE TO CENTER LINE OF ROAD

HART-REYNOLDS & ASSOCIATES, INC.
ENGINEERS
CORPORATION, FLORIDA

MATHESON HAMMOCK PARK
DADE COUNTY, FLORIDA
BRIDGE AND APPROACH ROAD

Sheet No.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
-----------	---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----

APPENDIX B – FDOT BRIDGE INSPECTION REPORT AND SUBSEQUENT INTERIM REPORTS



BRIDGE INSPECTION REPORT

PREPARED FOR: FDOT District 6
 BRIDGE OWNER: MIAMI-DADE COUNTY
 INSPECTION TYPE: Regular NBI
 CONTRACT No. CA611

Inspected by:
Marlin Engineering, Inc.

Bridge No. 874294

REPORT CONTAINS

Inspection Date: 4-06-2020

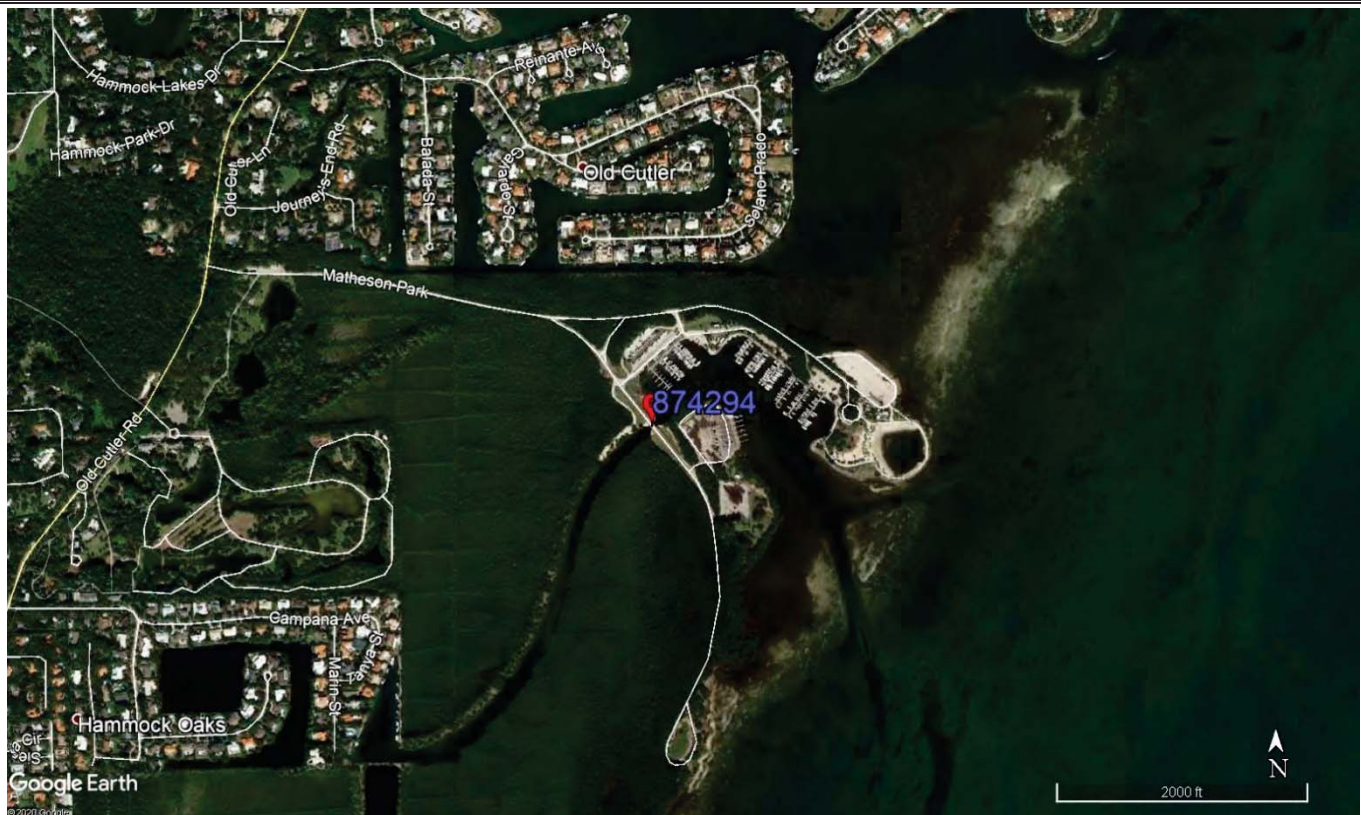
- | | | | |
|---|--|---|---|
| <input checked="" type="checkbox"/> BrM Inspection Report | <input checked="" type="checkbox"/> Bridge Profile | <input type="checkbox"/> Fracture Critical Data | <input type="checkbox"/> Addendum |
| <input checked="" type="checkbox"/> CIDR Information | <input checked="" type="checkbox"/> UW Inspection Report | <input checked="" type="checkbox"/> Load Rating Summary Sheet | <input type="checkbox"/> Mechanical and Electrical Data |



**Matheson Hammock Road over
 Matheson Hammock Canal**

Facility Carried & Location

Matheson Hammock Park



Location Map

Detour Length = N/A

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294**DISTRICT: D6 - Miami****INSPECTION DATE: 4/6/2020 GZJW**

BY:	Marlin Engineering, Inc.	STRUCTURE NAME:	Not recorded
OWNER:	2 County Hwy Agency	YEAR BUILT:	1967
MAINTAINED BY:	2 County Hwy Agency	SECTION NO.:	87 000 757
STRUCTURE TYPE:	5 Prestressed Concrete - 01 Slab	MP:	0.080
LOCATION:	Matheson Hammock Park	ROUTE:	00000
SERV. TYPE ON:	5 Highway-pedestrian	FACILITY CARRIED:	Matheson Hmk Road
SERV. TYPE UNDER:	5 Waterway	FEATURE INTERSECTED:	Matheson Hammock Canal

☐ FUNCTIONALLY OBSOLETE ☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Regular NBI

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 4/6/2020 UNDERWATER: 4/6/2020

SUFFICIENCY RATING: 15.5
HEALTH INDEX: 86.68

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

BY: Marlin Engineering, Inc.	STRUCTURE NAME: Not recorded
OWNER: 2 County Hwy Agency	YEAR BUILT: 1967
MAINTAINED BY: 2 County Hwy Agency	SECTION NO.: 87 000 757
STRUCTURE TYPE: 5 Prestressed Concrete - 01 Slab	MP: 0.080
LOCATION: Matheson Hammock Park	ROUTE: 00000
SERV. TYPE ON: 5 Highway-pedestrian	FACILITY CARRIED: Matheson Hmk Road
SERV. TYPE UNDER: 5 Waterway	FEATURE INTERSECTED: Matheson Hammock Canal

- ☐ THIS BRIDGE CONTAINS FRACTURE CRITICAL COMPONENTS
- ☐ THIS BRIDGE IS SCOUR CRITICAL
- ☒ THIS REPORT IDENTIFIES DEFICIENCIES WHICH REQUIRE PROMPT CORRECTIVE ACTION
- ☐ FUNCTIONALLY OBSOLETE ☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Regular NBI

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 4/6/2020 UNDERWATER: 4/6/2020

OVERALL NBI RATINGS:

DECK: 3 Serious	CHANNEL: 6 Bank Slumping
SUPERSTRUCTURE: 3 Serious	CULVERT: N N/A (NBI)
SUBSTRUCTURE: 4 Poor	SUFF. RATING: 15.5
PERF. RATING: Poor	HEALTH INDEX: 86.68

FIELD PERSONNEL / TITLE / NUMBER:**INITIALS**

Porras, Omar - Senior Diver Bridge Inspector (CBI#0368) (lead)

Gomez, Hiram - Bridge Inspector Assistance

Jacob Popp - Bridge Inspector Assistance, Diver

Burgos, Daniel - Bridge Inspector Assistance, Diver

Campo, Luis - Bridge Inspector Assistant

REVIEWING BRIDGE INSPECTION SUPERVISOR:

Rego, Alexis - Bridge Inspector (CBI#00409)

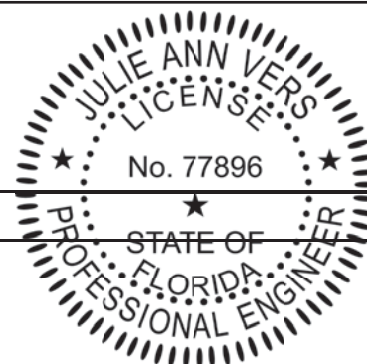
CONFIRMING REGISTERED PROFESSIONAL ENGINEER:

Vers, Julie - Structural Design Manager (P.E. # 77896) Marlin Engineering
 1700 NW 66 Avenue
 Suite 106
 Plantation Florida 33313

SIGNATURE: _____

DATE: _____

The official record of this package has been electronically signed and sealed by Julie A. Vers, P.E. on the date adjacent to the seal as required by Rule 61G15-23.004, F.A.C.. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.



This report contains information relating to the physical security of a structure and depictions of the structure. This information is confidential and exempt from public inspection pursuant to sections 119.071(3)(a) and 119.071(3)(b), Florida Statutes. Only the cover page of this report may be inspected and copied.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

All Elements

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3178	89.88	114	3.22	244	6.9	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	114	59.07	79	40.93	0	.	193 (SF)
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	20	100	0	.	20 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	144	100	0	.	144 (SF)
0	510 / 3	Wearing Surfaces	1929	73.23	0	.	705	26.77	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	705	100	0	.	705 sq.ft

Element Inspection Notes:

8099/3 Notes: The top of the slab units is not visible due to an asphalt overlay. The width of the sonovoid slab units was field verified to be 3ft. wide.

SECONDARY:

_Object markers and centerline raised pavement markers are missing on the structure. Refer to Photo 01. NO CHANGE.
 _Sidewalk panels are loose and moves under pedestrian load. Refer to Photo 02. NO CHANGE.
 _The slab unit joints show evidence of water seepage. NO CHANGE. NCAR.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Replace the southern utility access panel of Span 1.
 _Shim all sidewalk panels throughout the structure.
 _Rehab/replace slab units 1-7, 1-8, 2-7, 2-8, 3-7 and 3-8.
 _Clean efflorescence on slab units 1-6 and 1-7 to monitor the cracks.
 _Repair cracks on slab units 1-6, 1-9, 2-6, 2-9, 3-6.
 _Repair spalled/delaminated areas on slab units 1-6, 1-9, 2-6, 2-9, and 3-6 as needed.

CORRECTIVE ACTION EVALUATION:

_The recommendation noted above was completed.
 _The recommendation noted above was not completed. Recommendation will be repeated.
 _The recommendation noted above was not completed. Recommendation will be repeated.
 _The recommendation noted above was not completed. Recommendation will be repeated.
 _The recommendation noted above was not completed. Recommendation will be repeated

Refer to Defects 1080, 1090, 1100, and 1110 for additional deficiencies.

1080/3

CS-3:

_Slab Unit 1-8 east edge has a spall/delamination 4ft. L x 15in. W x 2in. D and associated cracks with corrosion bleed-out near mid-span. Previously noted a delamination with associated cracks. (Total 8 SF) Refer to Photo 03. INCREASE.
 _Slab Unit 1-9, center line has a spall/delamination up to 36in. L x 24in. W x 2in. D over Abutment 1. (Total 6 SF) Refer to Photo 04. NO CHANGE.
 _Slab Unit 3-7 has an unsound repaired area 11ft. L x 2ft. W starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out. (Total 22 SF) Refer to Photo 05. NO CHANGE.
 _Slab Unit 3-8 has a spall/delamination up to 7ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3. (Total 21 SF) Refer to Photo 06. NO CHANGE.
 _Slab Unit 3-8 west edge has an unsound repaired area 11ft. L x 18in. W starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence. (Total 22 SF) NO CHANGE.

CS-2:

This report contains information relating to the physical security of a structure and depictions of the structure. This information is confidential and exempt from public inspection pursuant to sections 119.071(3)(a) and 119.071(3)(b), Florida Statutes. Only the cover page of this report may be inspected and copied.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

_Slab Unit 1-6, east edge has a delamination up to full length x 12in. W starting at Pier 2 cap. Previously noted as 3in. W. (Total 30 SF) INCREASE.

_Slab Unit 1-7, east edge has a delamination 7ft. L x 4in. W, starting at Pier 2 cap. (Total 7 SF) NEW.

_Slab Unit 1-9, west edge has a delamination up to 10ft. L x 14in. W, starting at Pier 2 cap. (Total 10 SF) NO CHANGE.

_Slab Unit 2-6, east edge has a delamination 30in. L x 4in. W starting at Pier 2 cap. (Total 3 SF). Refer to Photo 07. NO CHANGE.

_Slab Unit 2-7, west edge has a delamination up to 24in. L x 4in. W starting at Pier 2 cap. (Total 2 SF) Refer to Photo 07. NO CHANGE.

_Slab Unit 2-8 west half has two delaminated areas up to 15ft. L x 18in. W (average width) at south and north ends. (Total 60 SF). Refer to Photo 08. NO CHANGE.

_Slab Unit 3-6 has a delamination up to 24in. L x 6in. W on the east edge over Pier 3. (Total 2 SF) NO CHANGE.

1090/3

CS-3:

_Slab Unit 1-6 exhibits a spall with exposed rebar up to 15in. L x 6in. W x 1/2in. D with evidence of previous failed repair, at 9ft. from Abutment 1. (Total 1 SF) Refer to Photo 09. NO CHANGE.

1100/3

CS-3:

_Slab Unit 2-8 has a spall 10ft. L x 24in. W x up to 4in. D at mid-span with 6 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (2 broken threads). (Total 20 SF) Refer to Photos 08 and 10. NO CHANGE.

1110/3

CS-3:

_Slab Unit 1-6 east edge has a delamination area full length x 12in. W with associated cracks up to 1/16in. W with efflorescence throughout. Previously noted as a delamination full length x 3in. W. (Total 30 SF) INCREASE.

_Slab Unit 1-7 east edge has a spall/delamination 24in. L x 12in. W with associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out over Abutment 1. No corrosion bleed out was previously noted. (Total 2 SF) Refer to Photo 11. INCREASE.

_Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W with associated cracks up to 1/8in. W with efflorescence and corrosion bleed-out, starting at Abutment 1. (Total 15 SF) Refer to Photo 11. NO CHANGE.

_Slab Unit 1-8 has a delaminated area up to 7ft. L x 3ft. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out. (Total 21 SF) NO CHANGE.

_Slab Unit 1-9 west edge has a delaminated area 8ft. L x 10in. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out, starting near the 3/4 point and extending to Pier 2 cap. (Total 8 SF) NO CHANGE.

_Slab Unit 2-7 east edge is intermittently cracked/delaminated up to span length x 16in. W (average width). (Total 38 SF) NO CHANGE.

_Slab Unit 2-9 west edge has a delaminated area up to 5ft. L x 5in. W with associated cracking up to 1/4in. wide, starting at the Pier 2 cap. (Total 5 SF). NO CHANGE.

_Slabs Unit 3-7 has two delaminated areas, one starting at Pier 3 up to 8ft. L x 15in. W (average width) with associated cracks, and the second, near mid-span up to 3ft. L x 30in. W. (Total 25 SF) NO CHANGE.

510/3

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Repair the asphalt overlay over the expansion joints and slab unit joints as needed.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defect 3220 for deficiencies.

3220/3

CS-3:

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

_The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated rutting over the slab unit joints with upheaving up to 1in. H at the shoulders, possibly indicating independent slab units movement. (Total 600 SF) Refer to Photo 12. NO CHANGE.

_The asphalt overlay has transverse cracks up to roadway width x 1/4in. W with rutting and upheaving up to 3in. H and vegetation growth over the expansion joints. (Total 105 SF) Refer to Photo 13. NO CHANGE.

DECKS : Joints

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	301 / 3	Pourable Joint Seal	0	.	0	.	104	74.29	36	25.71	140 ft
0	2310 / 3	Leakage	0	.	0	.	104	100	0	.	104 ft
0	2330 / 3	Seal Damage	0	.	0	.	0	.	36	100	36 ft

Element Inspection Notes:

301/3 Note: The roadway joints are not visible due to an asphalt overlay.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Clean and seal the expansion joints.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defects 2310 and 2330 for deficiencies.

2310/3 CS-3:
_There is evidence of moderate to heavy water seepage through the expansion joints on bents and abutment caps. (Total 104 LF) Refer to Photo 14. NO CHANGE. NCAR.

2330/3 CS-4:
_The sealant along the sidewalk expansion joints has deteriorated. (Total 36 LF) Refer to Photo 15. NO CHANGE.

MISCELLANEOUS : Channel

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8290 / 3	Channel	0	.	0	.	1	100	0	.	1 (EA)
0	9150 / 3	Bank Erosion	0	.	0	.	1	100	0	.	1 (EA)

Element Inspection Notes:

8290/3 FROM THE 2020 UNDERWATER INSPECTION:

Divers conducting the Underwater Inspection. Refer to Photo 16.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Repair undermining areas at the north seawall.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defect 9150 for deficiencies.

9150/3 CS-3:
_There are two areas of undermining up to 22ft. L x 3in. H x 21in. of penetration with backfill migration under the north seawall, below Slab Units 2-2 and 2-5. Previously noted

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

undermining up to 22ft. L x 9in. H x 21in. of penetration. (Total 1 ea.) Refer to Photo 17. NO CHANGE.

MISCELLANEOUS : Other Elements

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	321 / 3	Re Conc Approach Slab	1410	100	0	.	0	.	0	.	1410 sq.ft
0	510 / 3	Wearing Surfaces	957	91.14	0	.	93	8.86	0	.	1050 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	93	100	0	.	93 sq.ft

Element Inspection Notes:

321/3 Note: The approach slabs are not visible due to an asphalt overlay.

SECONDARY:

_There are several approach roadway guardrails posts spalled/delaminated up to 14in. H x 3.5in. W x 1-1/4in D with exposed and corroded rebars at the following locations: NW guardrail, Posts 1, 2, 3, and 4, SW guardrail, Posts 2 and 4 from the bridge, SE guardrail, Post 1 from the bridge. Post 4 in NW guardrail was not previously noted. Refer to Photo 18. INCREASE.

_The approach guardrail panels exhibit moderate to heavy corrosion with numerous corrosion holes throughout. Refer to Photo 19. NO CHANGE.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Replace the approach guardrail panels and posts.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

510/3 Refer to Defect 3220 for deficiencies.

3220/3 CS-3:

_The asphalt over the north approach slab has two longitudinal ravel cracks up to slab length x 1/8in. W in Lanes 1 and Lane 2. Previously noted cracks up to 1/16in. W (Total 40 SF) INCREASE. NCAR.

_The asphalt in both approach slab to approach roadway transitions has a transverse crack up to roadway width x 1/4in. W. (Total 53 SF) NO CHANGE. NCAR.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	205 / 3	Re Conc Column	0	.	0	.	4	100	0	.	4 each
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 each
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	3	100	0	.	3 each

Element Inspection Notes:

205/3 Note: At high tide, the seawater reaches the lower section of the columns.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Repair delaminated areas in columns.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defects 1090 and 1130 for deficiencies.

1090/3 CS-3:

_Column 2-2, south face has a spall/delamination up to 7ft. H x 3ft. W x 3in. D with one

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

exposed rebar and one stirrup, having areas of up to 80% section remaining. Additionally, there are areas of delamination around the column circumference covering the entire column height with associated cracks up to 1/4in. W. No exposed rebar was previously noted. (Total 1 ea.) Refer to Photo 20. INCREASE.

1130/3

CS-3:

_Columns 2-1, 3-1, and 3-2 have delaminated areas along their entire length with associated cracks up to full height x 1/16in. W, as a result of corrosion of the steel reinforcement. (Total 3 ea.) Refer to Photo 21. NO CHANGE.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	215 / 3	Re Conc Abutment	65	92.86	0	.	5	7.14	0	.	70 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	0	.	5	100	0	.	5 ft

Element Inspection Notes:

215/3

Refer to Defect 1080 for deficiencies.

1080/3

CS-3:

_Abutment 4 cap has a spall/delamination up to 5ft. L x full height x 2in. D with associated cracks up to 1/16in. W under Slab Units 3-10 and 3-11. (Total 5 LF) Refer to Photo 22. NEW.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	234 / 3	Re Conc Pier Cap	49	72.06	12	17.65	7	10.29	0	.	68 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	12	63.16	7	36.84	0	.	19 ft

Element Inspection Notes:

234/3

SECONDARY:

_Bents 2 and 3 caps have vegetation growth along the west end. Refer to Photo 23. NO CHANGE.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Remove vegetation from west end of caps.
 _Repair delaminations in Pier 2 and 3 caps.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.
 _The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defect 1080 for additional deficiencies.

1080/3

CS-3:

_Bent 2 cap has a spall/delamination up to 3ft. L x 16in. H x 1 in. D on the south face over Column 2-2, and on the same location, north face a delamination 20in. L x 12in. H. Previously noted only a delamination 3ft. L x 16in. H. (Total 3 LF) Refer to Photo 24. INCREASE.
 _Bent 3 cap, bottom and north faces has two unsound repaired areas with multidirectional cracks up to 1/64in. W. No unsound concrete with cracks was previously noted. (Total 4 LF) INCREASE.

CS-2:

_Pier 3 cap has intermittent delaminated areas up to 3ft. L x 16in. H between Columns 3-1 and 3-2, along the top and bottom north edges. Previously noted delaminations up to 3ft. L

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

x 16in. H totaling 5 LF. (Total 12 LF) INCREASE.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8393 / 3	Bulkhead Seawall Any Materia	0	.	0	.	354	100	0	.	354 ft
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	314	100	0	.	314 ft
0	6000 / 3	Scour	0	.	0	.	40	100	0	.	40 ft

Element Inspection Notes:

8393/3 Note: This element represents the concrete seawall that lines both sides of the channel. The seawall is underwater during high tide. The seawalls have a total of 44 piles; 22 piles at each seawall.

SECONDARY:

_The brackets and fasteners attaching the clearance gauges to the seawalls exhibit heavy to severe corrosion. Refer to Photo 25.

FROM THE 2020 UNDERWATER INSPECTION:**SECONDARY:**

_SE and NW clearance gauges have moderate decay at bottom 3ft. Refer to Photo 26. NO CHANGE.

_The south seawall has two open joints up to 4in. W with backfill leakage behind Piles 15 and 18 from west. Refer to Photo 27. NO CHANGE.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Clean & seal cracks & repair delaminations/spalls in seawall caps.

_Seal open joints at the south seawall behind Piles 15 and 18.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defects 1130 and 6000 for additional deficiencies.

1130/3

CS-3:

_The seawall caps on the north and south walls have up to 1/4in W cracks, with associated delaminations/spalls throughout their entire lengths. (Total 314 LF) Refer to Photo 28. NO CHANGE.

_The south seawall at Pile 13, SE corner has a spall 14in. H x 3-1/2in. W x 1in. D, 3ft. 9in. below cap. NO CHANGE. NCAR.

_South seawall piles have vertical cracks up to 31in. L x 1/8in. W, some with corrosion bleed out as follows: NO CHANGE. NCAR.

-Pile 3, NE corner has a crack, and west, north and east faces have cracks with corrosion bleed out.

-Pile 4, north face has a crack with corrosion bleed out.

-Pile 16, east face has a crack with corrosion bleed out.

-Pile 17, west, north and east faces have cracks with corrosion bleed out.

-Piles 19, 20 and 21, SW and SE corners have cracks.

_North seawall piles have vertical cracks intermittently throughout, up to 34in. L x 1/16in. W, some with corrosion bleed out as follows: NO CHANGE. NCAR.

-Piles 5 and 6, SW and SE corners have cracks with corrosion bleed out.

-Pile 3, SW corner has a crack.

-Pile 4, NW corner has a crack.

-Piles 7, 8, 10, 12, 13, 14, 15, 16, 17, 18, 19, 20, 23 have cracks in the SW and SE corners.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

-Pile 11, SE corner has a crack.

6000/3 From the 2020 Underwater Inspection:

CS-3:

_There are two areas of undermining up to 22ft. L x 9in. H x 21in. of penetration with backfill migration under the north seawall, below Slab Units 2 and 5. Refer to Element 8290 for related comments and recommended corrective actions. (Total 40 LF) NO CHANGE.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8394 / 3	R/Conc Abut Slope Protection	3968	73.81	0	.	1408	26.19	0	.	5376 (SF)
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	320	100	0	.	320 (SF)
0	4000 / 3	Settlement	0	.	0	.	1088	100	0	.	1088 (SF)

Element Inspection Notes:

8394/3 Note: At high tide, the seawater reaches the lower section of the concrete slope pavement.

SECONDARY:

_There is vegetation growth in the joints between the panels of slope protection in several locations. NO CHANGE. NCAR.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Repair settled & fractured sections of slope pavement.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defects 1130 and 4000 for additional deficiencies.

1130/3 CS-3:
_The slope pavement has multidirectional cracks up to 5ft. L x 1/8in. W along the NE corner near the toe. (Total 320 SF) NO CHANGE. NCAR.

4000/3 CS-3:
_The top slope pavement section along the SW and NW corners has settled up to 4in. H. (Total 933 SF) NO CHANGE.
_The slope protection toe has a fractured and settled area of 15ft. x 7ft. x 2ft deep at the NW corner behind the seawall cap. Possibly due to water reaching this area at high tide, no undermining or backfill migration are noted in the channel adjacent area. (Total 105 SF) Refer to Photo 29. NO CHANGE.
_The SW slope protection toe has 5 fractured panels that have settled up to 3in. H. Possibly due to water reaching this area at high tide, no undermining or backfill migration are noted in the channel adjacent area. (Total 50 SF) Refer to Photo 30. NO CHANGE.

SUPERSTRUCTURE : Superstructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	333 / 3	Other Bridge Railing	167	83.5	33	16.5	0	.	0	.	200 ft
0	1000 / 3	Corrosion	0	.	30	100	0	.	0	.	30 ft
0	1020 / 3	Connection	0	.	3	100	0	.	0	.	3 ft

Element Inspection Notes:

333/3 Note: This element represents the concrete post and beam bridge rail with

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

aluminum handrail on top across both sides of the structure.

CS-1:

_The concrete bridge rail beams have 1/64in W cracks at the junctures with the posts in several locations. NO CHANGE. NCAR.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Replace the approach guardrail panels and posts.

_Replace the missing railing nuts on left side of Bent 3.

_Clean & coat the corroded nuts of railing.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

Refer to Defects 1000 and 1020 for additional deficiencies.

1000/3

CS-2:

_The rail anchor bolt nuts and washers have moderate corrosion at random locations: 25 nuts at west railing, and 5 nuts at east railing. (Total 30 LF) Refer to Photo 31. NO CHANGE.

1020/3

CS-2:

_There are several missing anchor bolt nuts at the aluminium rail posts at the following locations: (Total 3 ea.) Refer to Photo 32. INCREASE.

_West rail, Post 1-1 is missing 1 of 4 nuts. NEW.

_West rail, Post 2-6 is missing 2 of 4 nuts. NO CHANGE.

_East rail, Post 1-5 is missing 1 of 4 nuts. NEW.

Total Number of Elements*: 10

*excluding defects/protective systems

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

Inspector Recommendations

UNIT: 0 DECKS**ELEMENT/ENV: 301:2330 / 3 Seal Damage****ELEM CATEGORY: Joints**

CONDITION STATE	PRIORITY
4 MMS Quantity: 36 lf Element Estimated Quantity: 36 ft	3
WORK ORDER RECOMMENDATION: Install new sealant along the sidewalk expansion joints. Photo 15	

ELEMENT/ENV: 8099 / 3 PS Conc Slab (Sonovoid)**ELEM CATEGORY: Decks/Slabs**

CONDITION STATE	PRIORITY
1 , 2 , 3 MMS Quantity: 4 sf Element Estimated Quantity: 4 (SF)	3
WORK ORDER RECOMMENDATION: Replace missing object markers at the four corners of the bridge. Photo 01	
1 , 2 , 3 MMS Quantity: 300 sf Element Estimated Quantity: 300 (SF)	3
WORK ORDER RECOMMENDATION: Properly secure the sidewalk panels. Photo 02	

ELEMENT/ENV: 8099:510:3220 / 3 Crack (Wearing Surface)**ELEM CATEGORY: Decks/Slabs**

CONDITION STATE	PRIORITY
3 MMS Quantity: 600 sf Element Estimated Quantity: 600 sq.ft	0
WORK ORDER RECOMMENDATION: Monitor the slab units for independent movement. Photo 12	
3 MMS Quantity: 600 sf Element Estimated Quantity: 600 sq.ft	3
WORK ORDER RECOMMENDATION: Repair cracks on the asphalt along the slab unit joints. Photo 12	
3 MMS Quantity: 105 sf Element Estimated Quantity: 105 sq.ft	3
WORK ORDER RECOMMENDATION: Clean and repair cracks and rutting along the expansion joints. Photo 13	

ELEMENT/ENV: 8099:1080 / 3 Delamination/Spall/Patched Area**ELEM CATEGORY: Decks/Slabs**

CONDITION STATE	PRIORITY
2 , 3 MMS Quantity: 338 sf Element Estimated Quantity: 338 (SF)	3
WORK ORDER RECOMMENDATION: Repair spalls delaminations and cracks along the underside of the slabs units. Photos 03 to 11	

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

Inspector Recommendations

UNIT: 0 DECKS**ELEMENT/ENV: 8099:1100 / 3 Exposed Prestressing****ELEM CATEGORY: Decks/Slabs**

CONDITION STATE	PRIORITY
3 MMS Quantity: 20 sf Element Estimated Quantity: 20 (SF)	3
WORK ORDER RECOMMENDATION: Clean and coat exposed prestressing and reinforce Slab Unit 2-8. Photos 08 and 10	

UNIT: 0 MISCELLANEOUS**ELEMENT/ENV: 321 / 3 Re Conc Approach Slab****ELEM CATEGORY: Other Elements**

CONDITION STATE	PRIORITY
1 MMS Quantity: 80 sf Element Estimated Quantity: 80 sq.ft	3
WORK ORDER RECOMMENDATION: Replace all the approach guardrail panels. Photo 19	
1 MMS Quantity: 7 sf Element Estimated Quantity: 7 sq.ft	3
WORK ORDER RECOMMENDATION: Replace spalled and delaminated posts along the roadway approach guardrails. Photo 18	

ELEMENT/ENV: 8290:9150 / 3 Bank Erosion**ELEM CATEGORY: Channel**

CONDITION STATE	PRIORITY
3 MMS Quantity: 8 mh Element Estimated Quantity: 1 (EA)	3
WORK ORDER RECOMMENDATION: Repair undermining areas at the north seawall. Photo 17	

UNIT: 0 SUBSTRUCTURE**ELEMENT/ENV: 205:1090 / 3 Exposed Rebar****ELEM CATEGORY: Substructure**

CONDITION STATE	PRIORITY
3 MMS Quantity: 16 mh Element Estimated Quantity: 1 each	3
WORK ORDER RECOMMENDATION: Remove any loose concrete and repair delaminations and spalls along the Column 2-2. Photo 20	

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

Inspector Recommendations

UNIT: 0 SUBSTRUCTURE**ELEMENT/ENV: 205:1130 / 3 Cracking (RC and Other)****ELEM CATEGORY: Substructure**

CONDITION STATE			PRIORITY
3	MMS Quantity: 8 mh	Element Estimated Quantity: 4 each	3
WORK ORDER RECOMMENDATION: Install cathodic protection to Bents 2 and 3 columns. Photos 20 and 21			
3	MMS Quantity: 80 mh	Element Estimated Quantity: 4 each	3
WORK ORDER RECOMMENDATION: Repair delaminations and seal cracks along Bents 2 and 3 columns. Photo 21			

ELEMENT/ENV: 215:1080 / 3 Delamination/Spall/Patched Area**ELEM CATEGORY: Substructure**

CONDITION STATE			PRIORITY
3	MMS Quantity: 8 mh	Element Estimated Quantity: 5 ft	3
WORK ORDER RECOMMENDATION: Repair spall/delamination on Abutment 4 cap under Slab Units 3-10 and 3-11. Photo 22			

ELEMENT/ENV: 234 / 3 Re Conc Pier Cap**ELEM CATEGORY: Substructure**

CONDITION STATE			PRIORITY
1 , 2 , 3	MMS Quantity: 2 mh	Element Estimated Quantity: 2 ft	3
WORK ORDER RECOMMENDATION: Remove vegetation growing on west end of Bents 2 and 3 caps. Photo 23			

ELEMENT/ENV: 234:1080 / 3 Delamination/Spall/Patched Area**ELEM CATEGORY: Substructure**

CONDITION STATE			PRIORITY
2 , 3	MMS Quantity: 16 mh	Element Estimated Quantity: 19 ft	3
WORK ORDER RECOMMENDATION: Repair spalls and delaminations along Bents 2 and 3 caps. Photo 24			

ELEMENT/ENV: 8393 / 3 Bulkhead Seawall Any Material**ELEM CATEGORY: Substructure**

CONDITION STATE			PRIORITY
3	MMS Quantity: 8 mh	Element Estimated Quantity: 4 ft	3
WORK ORDER RECOMMENDATION: Replace the clearance gauges and hardware on the seawall at both sides of the channel. Photos 25 and 26			

This report contains information relating to the physical security of a structure and depictions of the structure. This information is confidential and exempt from public inspection pursuant to sections 119.071(3)(a) and 119.071(3)(b), Florida Statutes. Only the cover page of this report may be inspected and copied.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
 Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
 Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

Inspector Recommendations

UNIT: 0 SUBSTRUCTURE

ELEMENT/ENV: 8393 / 3 Bulkhead Seawall Any Material**ELEM CATEGORY: Substructure**CONDITION
STATE

PRIORITY

3 MMS Quantity: 8 mh Element Estimated Quantity: 2 ft

3

WORK ORDER RECOMMENDATION:

Seal open joints at the south seawall behind Piles 15 and 18. Photo 27

ELEMENT/ENV: 8393:1130 / 3 Cracking (RC and Other)**ELEM CATEGORY: Substructure**CONDITION
STATE

PRIORITY

3 MMS Quantity: 40 mh Element Estimated Quantity: 314 ft

3

WORK ORDER RECOMMENDATION:

Repair delaminations and spalls along the seawall caps. Photo 28

ELEMENT/ENV: 8394:4000 / 3 Settlement**ELEM CATEGORY: Substructure**CONDITION
STATE

PRIORITY

3 MMS Quantity: 160 mh Element Estimated Quantity: 1088 (SF)

3

WORK ORDER RECOMMENDATION:

Repair settled and fractured areas along the slope protections. Photos 29 and 30

UNIT: 0 SUPERSTRUCTURE

ELEMENT/ENV: 333:1000 / 3 Corrosion**ELEM CATEGORY: Superstructure**CONDITION
STATE

PRIORITY

2 MMS Quantity: 30 lf Element Estimated Quantity: 30 ft

3

WORK ORDER RECOMMENDATION:

Clean and paint or replace corroded hardware along the bridge aluminium rail. Photo 31

ELEMENT/ENV: 333:1020 / 3 Connection**ELEM CATEGORY: Superstructure**CONDITION
STATE

PRIORITY

2 MMS Quantity: 3 lf Element Estimated Quantity: 3 ft

3

WORK ORDER RECOMMENDATION:

Replace missing nuts at the aluminium rail post connections. Photo 32

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north.

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

Element 227/3 Re Conc Pile notes have been replaced by Element 205/3 Re Conc Column on 10/29/2019.

TRAFFIC RESTRICTIONS:

Based on the current load rating analysis dated 1/13/2020, it is recommended that this bridge be posted for the SU, C and ST5 type vehicles as follows: SU = 11 tons, C = 16 tons, ST5 = 18 tons. The bridge is currently posted for SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 33 and 34.

REVIEWED BY:

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

INSPECTION NOTES: **GZJW** **4/6/2020**

Sufficiency Rating Calculation Accepted by knmeira at 5/13/2020 9:36:35 AM

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/06/2020)

The Substructure NBI Rating is coded 4 (Poor) due to the significant deterioration of Column 2-2. (04/06/2020)

The Channel NBI Rating was lowered from 7 to 6 due to areas of undermining on the channel below the North seawall. (04/06/2020)

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 04/06/2020 per Julie A. Vers, P.E.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure.

Element 8475 R/Conc Walls was replaced by 8393 Bulkhead Seawall Any Material during this inspection cycle. All previous notes were transferred accordingly. (04/06/2020)

The following elements were inspected underwater by the divers:

8290 Channel

8393 Bulkhead Seawall Any Material

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED.

RT: Right

LT: Left

NC: No Change

INC: Increase

CAT: Corrective Action Taken

L: Long

W: Wide

H: High

D: Deep

UW: Underwater

S.L.: Section Loss

in.: Inches

ft.: Feet

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 01 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Object markers and centerline raised pavement markers are missing on the structure.

WORK ORDER RECOMMENDATION:

Replace missing object markers at the four corners of the bridge.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 02 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Sidewalk panels are loose and moves under pedestrian load.

WORK ORDER RECOMMENDATION:
Properly secure the sidewalk panels.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 03 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-8 east edge has a spall/delamination 4ft. L x 15in. W x 2in. D and associated cracks with corrosion bleed-out near mid-span.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 04 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-9, center line has a spall/delamination up to 36in. L x 24in. W x 2in. D over Abutment 1.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 05 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 3-7 has an unsound repaired area 11ft. L x 2ft. W starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 06 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 3-8 has a spall/delamination up to 7ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 07 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Units 2-6 and 2-7, east and west edges have delaminations up to 30in. L x 4in. W, starting at Pier 2 cap.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 08 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 2-8 west half has two delaminated areas up to 15ft. L x 18in. W (average width) at south and north ends, and at midspan has a spall 10ft. L x 24in. W x up to 4in. D with exposed strands. Refer to Photo 10 for additional information.

WORK ORDER RECOMMENDATION:

Clean and coat exposed prestressing and reinforce Slab Unit 2-8.

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 09 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-6 exhibits a spall with exposed rebar up to 15in. L x 6in. W x 1/2in. D with evidence of previous failed repair, at 9ft. from Abutment 1.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 10 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 2-8 has a spall 10ft. L x 24in. W x up to 4in. D at mid-span with 6 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (2 broken threads).

WORK ORDER RECOMMENDATION:

Clean and coat exposed prestressing and reinforce Slab Unit 2-8.

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 11 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-7 east edge has a spall/delamination 24in. L x 12in. W with associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out over Abutment 1. Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W with associated cracks up to 1/8in. W with efflorescence and corrosion bleed-out, starting at Abutment 1.

WORK ORDER RECOMMENDATION:

Repair spalls delaminations and cracks along the underside of the slabs units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 12 Element/Env 8099/ 510/3: PS Conc Slab (Sonovoid)/ Wearing Surfaces

The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated rutting over the slab unit joints with upheaving up to 1in. H at the shoulders, possibly indicating independent slab units movement.

WORK ORDER RECOMMENDATION:

Repair cracks on the asphalt along the slab unit joints.
Monitor the slab units for independent movement.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 13 Element/Env 8099/ 510/3: PS Conc Slab (Sonovoid)/ Wearing Surfaces

The asphalt overlay has transverse cracks up to roadway width x 1/4in. W with rutting and upheaving up to 3in. H and vegetation growth over the expansion joints.

WORK ORDER RECOMMENDATION:

Clean and repair cracks and rutting along the expansion joints.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 14 Element/Env 301/3: Pourable Joint Seal

There is evidence of moderate to heavy water seepage through the expansion joints on bents and abutment caps.

WORK ORDER RECOMMENDATION:

None.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 15 Element/Env 301/3: Pourable Joint Seal

The sealant along the sidewalk expansion joints has deteriorated.

WORK ORDER RECOMMENDATION:

Install new sealant along the sidewalk expansion joints.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 16 Element/Env 8290/3: Channel

Divers conducting the Underwater Inspection.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

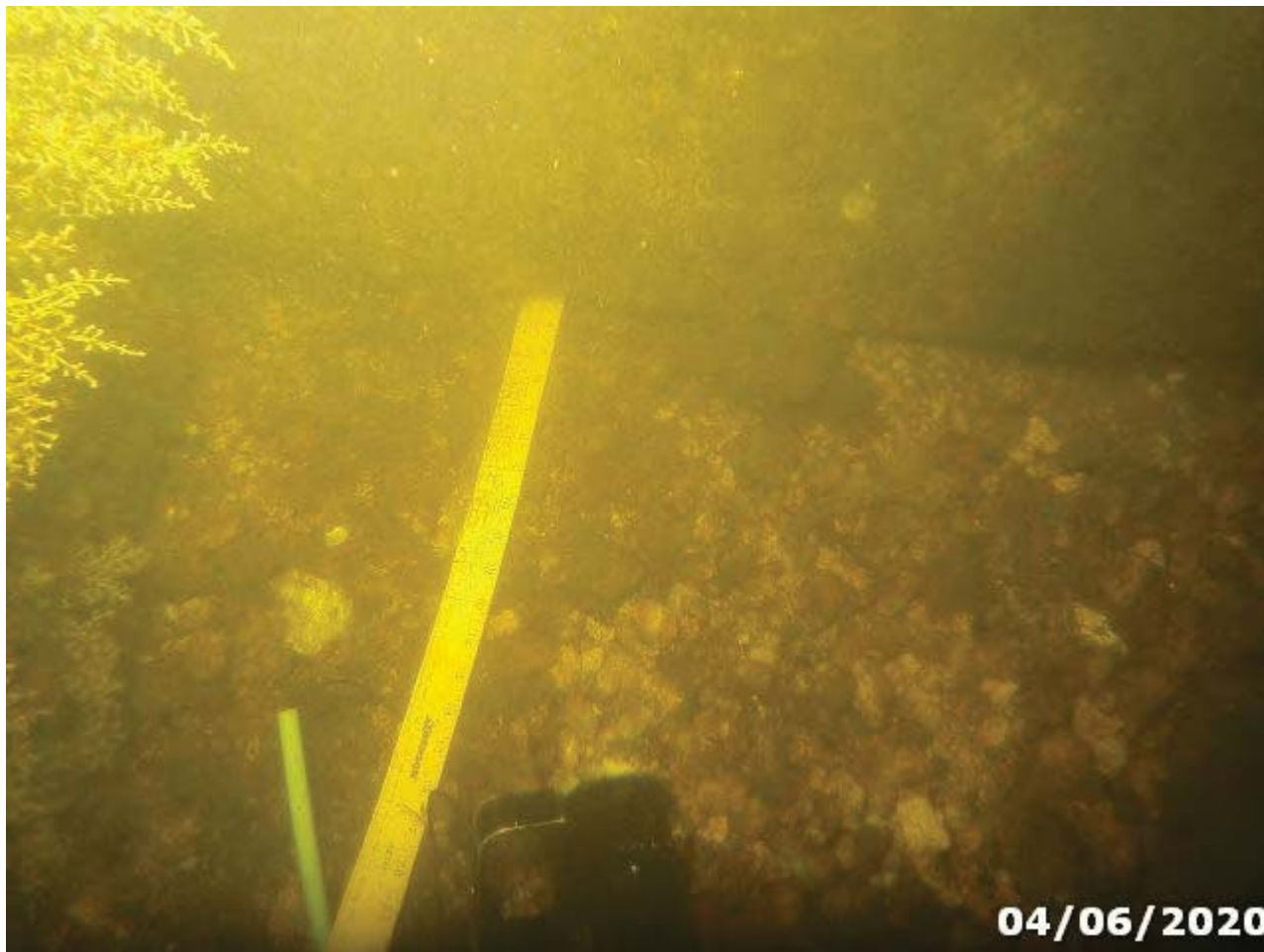


Photo 17 Element/Env 8290/3: Channel

There are two areas of undermining up to 22ft. L x 3in. H x 21in. of penetration with backfill migration under the north seawall, below Slab Units 2-2 and 2-5.

WORK ORDER RECOMMENDATION:

Repair undermining areas at the north seawall.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 18 Element/Env 321/3: R/Conc Approach Slab

There are several approach roadway guardrails posts spalled/delaminated up to 14in. H x 3.5in. W x 1-1/4in D with exposed and corroded rebars. Shown Post 1 at NW approach guardrail.

WORK ORDER RECOMMENDATION:

Replace spalled and delaminated posts along the roadway approach guardrails.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 19 Element/Env 321/3: R/Conc Approach Slab

The approach guardrail panels exhibit moderate to heavy corrosion with numerous corrosion holes throughout.

WORK ORDER RECOMMENDATION:

Replace all the approach guardrail panels.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 20 Element/Env 205/3: Re Conc Column

Column 2-2, south face has a spall/delamination up to 7ft. H x 3ft. W x 3in. D with one exposed rebar and one stirrup, having areas of up to 80% section remaining. Additionally, there are areas of delamination around the column circumference covering the entire column height with associated cracks up to 1/4in. W.

WORK ORDER RECOMMENDATION:

Remove any loose concrete and repair delaminations and spalls along the Column 2-2.
Install cathodic protection to Bents 2 and 3 columns.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 21 Element/Env 205/3: Re Conc Column

Columns 2-1, 3-1, and 3-2 have delaminated areas along their entire length with associated cracks up to full height x 1/16in. W, as a result of corrosion of the steel reinforcement.

WORK ORDER RECOMMENDATION:

Install cathodic protection to Bents 2 and 3 columns.

Repair delaminations and seal cracks along Bents 2 and 3 columns.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 22 Element/Env 215/3: Re Conc Abutment

Abutment 4 cap has a spall/delamination up to 5ft. L x full height x 2in. D with associated cracks up to 1/16in. W under Slab Units 3-10 and 3-11.

WORK ORDER RECOMMENDATION:

Repair spall/delamination on Abutment 4 cap under Slab Units 3-10 and 3-11.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 23 Element/Env 234/3: Re. Concrete Pier Cap

Bents 2 and 3 caps have vegetation growth along the west end.

WORK ORDER RECOMMENDATION:

Remove vegetation growing on west end of Bents 2 and 3 caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection**

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 24 Element/Env 234/3: Re. Concrete Pier Cap

Bent 2 cap has a spall/delamination up to 3ft. L x 16in. H x 1 in. D on the south face over Column 2-2, and on the same location, north face a delamination 20in. L x 12in. H.

WORK ORDER RECOMMENDATION:

Repair spalls and delaminations along Bents 2 and 3 caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 25 Element/Env 8393/3: Bulkhead Seawall Any Material

The brackets and fasteners attaching the clearance gauges to the seawalls exhibit heavy to severe corrosion.

WORK ORDER RECOMMENDATION:

Replace the clearance gauges and hardware on the seawall at both sides of the channel.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 26 Element/Env 8393/3: Bulkhead Seawall Any Material

SE and NW clearance gauges have moderate decay at bottom 3ft.

WORK ORDER RECOMMENDATION:

Replace the clearance gauges and hardware on the seawall at both sides of the channel.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW

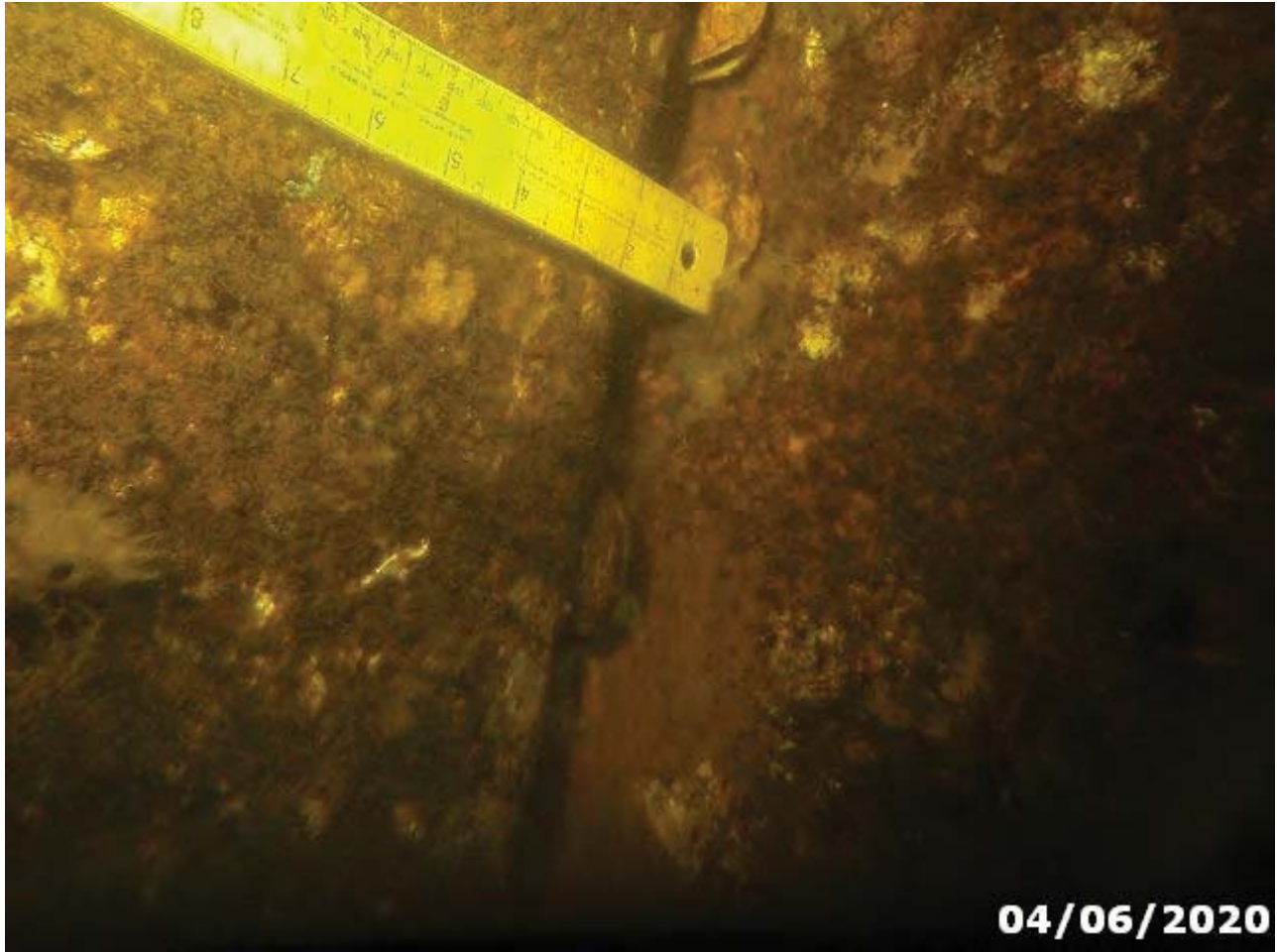


Photo 27 Element/Env 8393/3: Bulkhead Seawall Any Material

The south seawall has two open joints up to 4in. W with backfill leakage behind Piles 15 and 18 from west.

WORK ORDER RECOMMENDATION:

Seal open joints at the south seawall behind Piles 15 and 18.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 28 Element/Env 8393/3: Bulkhead Seawall Any Material

The seawall caps on the north and south walls have up to 1/4in W cracks, with associated delaminations/spalls throughout their entire lengths.

WORK ORDER RECOMMENDATION:

Repair delaminations and spalls along the seawall caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 29 Element/Env 8394/3: R/Conc Abut Slope Protection

The slope protection toe has a fractured and settled area of 15ft. x 7ft. x 2ft deep at the NW corner behind the seawall cap. The channel water reach this area at high tide.

WORK ORDER RECOMMENDATION:

Repair settled and fractured areas along the slope protections.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 30 Element/Env 8394/3: R/Conc Abut Slope Protection

The SW slope protection toe has 5 fractured panels that have settled up to 3in. H. The channel water reach this area at high tide.

WORK ORDER RECOMMENDATION:

Repair settled and fractured areas along the slope protections.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 31 Element/Env 333/3: Other Bridge Railing

The rail anchor bolt nuts and washers have moderate corrosion at random locations: 25 nuts at west railing, and 5 nuts at east railing.

WORK ORDER RECOMMENDATION:

Clean and paint or replace corroded hardware along the bridge aluminium rail.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 32 Element/Env 333/3: Other Bridge Railing

There are several missing anchor bolt nuts at the aluminium rail posts: west rail, Posts 1-1 and 2-6; and east rail, Post 1-5.

WORK ORDER RECOMMENDATION:

Replace missing nuts at the aluminium rail post connections.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 33 STRUCTURE NOTES: South Approach Posting Sign

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



Photo 34 STRUCTURE NOTES: North Approach Posting Sign

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



SCOUR EVALUATION

Channel looking West

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**
Inspection/CIDR/Bridge Profile Report with PDF attachment(s)
Inspection

Structure ID: 874294

DISTRICT: D6 - Miami

INSPECTION DATE: 4/6/2020 GZJW



SCOUR EVALUATION

Channel looking East

F. FIELD PREPARATION and CHECKLIST

Structure ID: 874294Inspection Date: 04/06/2020Underwater: 04/06/2020

A. Tools and Equipment

Full Size Cargo Van:	Yes: <input checked="" type="checkbox"/>	No:	Pick-up Truck:	Yes: <input checked="" type="checkbox"/>	No:
Automobile:	Yes:	No: <input checked="" type="checkbox"/>	Video:	Yes: <input type="checkbox"/>	No: <input checked="" type="checkbox"/>
Camera:	Yes: <input checked="" type="checkbox"/>	No:			
NDT Equipment:	Yes:	No: <input checked="" type="checkbox"/>			
NDT Type:	<u>N/A</u>				
Binoculars:	Yes:	No: <input checked="" type="checkbox"/>			
Diving Performed:	Yes: <input checked="" type="checkbox"/>	No:	Max Depth: <u>10.6 ft.</u>	Current: <u>Moderate</u>	
Dive Mode:	<u>SCUBA</u>				
Hand Tools:					
1. Standard Inspection Tools	2. Chipping Hammer				
3. Inspection Hand Tools	4. Flashlight				
5. Folding Rulers					

Other:

B. Services

Flag Crew: <u>N/A</u>	Snooper: <u>N/A</u>
Electrician: <u>N/A</u>	Other: _____

C. Scheduling (Brief Explanation)

Routine Inspection, no special scheduling needed.

Man Hours: 0 hrs. Dive Time: 2 hrs. Travel Time: 1 hr. Office Time: 1 hr.

D. Site Conditions


Boat Needed: NO Type of Boat: N/ALocation of Boat Ramp: N/ALengthy Travel Required: N/ADifficult Access: NOWater Obviously Polluted: NOWater quality is fair: YesStrong Water Current: YesOther: N/A

E. UNDERWATER ELEMENTS INSPECTED:

- 8290 Channel – 1ea.
- 8393 Bulkhead Seawall Any Material – 354 ft.

Bridge No.	874294	Analysis Method:	LRFR-LRFD	FDOT Bridge Load Rating Summary Form (Page 1 of 1)
Location	Matheson hammock Road over matheson Hammock Canal			
Description	3 Spans, 2-30'&1-40', Prestressed voided slab beams 36"x17"			

Rating Type	Rating Type	Gross Axle Weight (tons)	Moment/Shear/Service		Dead Load Factor	Live Load Factor	Live Load Distrib. Factor (axles)	Rating Factor	Span No. - Girder No., Interior/Exterior, %Span Length	RF-Weight (tons)
Level	Vehicle	Weight	Member Type	Limit	DC	LL	LLDF	RF	Governing Location	RATING
Inventory	HL93	36	Prestressed	Service	1.00	0.80	0.600	0.210	Central span, midspan	7.6
Operating	HL93	36	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.330	Central span, midspan	11.9
Permit	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Permit Max Span	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Legal	SU2	17	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.690	Central span, midspan	11.7
	SU3	33	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.370	Central span, midspan	12.2
	SU4	35	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.340	Central span, midspan	11.9
	C3	28	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.650	Central span, midspan	18.2
	C4	36.7	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	16.9
	C5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.440	Central span, midspan	17.6
	ST5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	18.4
Emergency Vehicle (EV)	EV2	28.75	Prestressed	NA	NA	NA	0.600			-1
	EV3	43	Prestressed	NA	NA	NA	0.600			-1

Original Design Load	HS20 or HS20-S16-44	Performed by:	Mengyuan Chen	Date:	01/13/20
Rating Type, Analysis	LRFR-LRFD	Checked by:	Juan A. Sobrino	Date:	01/13/20
Distribution Method	Others	Sealed By:	Juan A. Sobrino	Date:	01/13/20
Impact Factor	33.0% (axle loading)	FL P.E. No.:	73121		
FL120 Gov. Span Length	38.3 (feet)	Cert. Auth. No.:	27244		
Minimum Span Length	28.3 (feet)	Phone & email:	(+1) 305 648 00 10, miami@pedelta.om		
Recommended Posting	> 39.9% below (0.000-0.600) (Required)	Company:	Pedelta Inc.		
Recommended SU Posting*	11 (tons)	Address:	2000 Ponce de Leon Blvd., Suite 624, Coral Gables, Florida 33134, USA		
Recommended C Posting	16 (tons)	<div> <div>  <div> Juan A. Sobrino P.E. State of Florida, Professional Engineer </div> </div> <div> Digitally signed by Juan Sobrino Date: 2020.01.13 15:58:25 -05'00' </div> </div> <p>Juan A. Sobrino, State of Florida, Professional Engineer, License No 73121.</p> <p>This document has been electronically signed and sealed by Juan A. Sobrino on January 13th, 2020 using a SHA authentication code. Printed copies of this document are not considered signed and sealed and the SHA authentication code must be verified on any electronic copies.</p>			
Recommended ST5 Posting	18 (tons)				
Owner	02 County Highway Agency				
Location	Neither Interstate traffic nor within 1 mile reasonable access to an Interstate				
EV Posting	No. EV posting is not recommended. The FAST Act does not apply				
Floor Beam Present?	No				
Segmental Bridge?	No				
Project No. & Reason	432907-1-72-02 Deterioration				
Plans Status	Built				

This 10-11-2019 summary follows the FDOT Bridge Load Rating Manual (BLRM), and the FDOT BMS Coding Guide.

*Recommended SU Posting levels for Florida SU trucks adequately restricts AASHTO SU trucks; see BLRM Chapter 7.

fdot.gov/maintenance/LoadRating.shtm

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 5/18/2020

Description

Structure Unit Identification

Bridge/Unit Key: 874294 0
 Structure Name:
 Description: SPANS 1 THRU 3
 Type: M - Main

Roadway Identification

NBI Structure No (8): 874294
 Position/Prefix (5): 1 - Route On Structure
 Kind Hwy (Rte Prefix): 4 County Hwy
 Design Level of Service: 8 Service Road
 Route Number/Suffix: 00000 / 0 N/A (NBI)
 Feature Intersect (6): Matheson Hammock Canal
 Critical Facility: Not Defense-crit
 Facility Carried (7): Matheson Hmk Road
 Mile Point (11): 0.08
 Latitude (16): 025d40'44.2" Long (17): 080d15'43.8"

Roadway Traffic and Accidents

Lanes (28): 2 Medians: 0 Speed: 15 mph
 ADT Class: 2 ADT Class 2
 Recent ADT (29): 736 Year (30): 2014
 Future ADT (114): 1168 Year (115): 2036
 Truck % ADT (109): 1
 Detour Length (19): 99 mi
 Detour Speed:
 Accident Count: -1 Rate:

Roadway Classification

Nat. Hwy Sys (104): 0 Not on NHS
 National base Net (12): 0 - Not on Base Network
 LRS Inventory Rte (13a): 87 000 757 Sub Rte (13b): 00
 Functional Class (26): 09 Rural Local
 Federal Aid System: OFF
 Defense Hwy (100): 0 Not a STRAHNET hwy
 Direction of Traffic (102): 2 2-way traffic
 Emergency: ☒

Roadway Clearances

Vertical (10): 99.99 ft Appr. Road (32): 26.25 ft
 Horiz. (47): 26.25 ft Roadway (51): 26.25 ft
 Truck Network (110): 0 Not part of natl netwo
 Toll Facility (20): 3 On free road
 Fed. Lands Hwy (105): 0 N/A (NBI)
 School Bus Route: ☐
 Transit Route: ☐

NBI Project Data

Proposed Work (075A): Not Applicable (P)
 Work To Be Done By (075B): Not Applicable (P)
 Improvement Length (076): 0 ft

Improvement Cost (094): \$ 0.00
 Roadway Improvement Cost (095): \$ 0.00
 Total Cost (096): \$ 0.00
 Year of Estimate (097):

NBI Rating

Channel (61): 6 Bank Slumping
 Deck (58): 3 Serious
 Superstructure (59): 3 Serious
 Substructure (60): 4 Poor

Culvert (62): N N/A (NBI)
 Waterway (71): 8 Equal Desirable
 Unrepaired Spalls: -1 sq.ft.
 Review Required: ☒

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 5/18/2020

Structure Identification

Admin Area: Miami-Dade
 District (2): D6 - Miami
 County (3): (87)Miami-Dade
 Place Code (4): South Miami Heights
 Location (9): Matheson Hammock Park
 Border Br St/Reg (98): Not Applicable (P) Share: 0 %
 Border Struct No (99):
 FIPS State/Region (1): 12 Florida Region 4-Atlanta
 NBIS Bridge Len (112): Y - Meets NBI Length
 Parallel Structure (101): No || bridge exists
 Temp. Structure (103): Not Applicable (P)
 Maint. Resp. (21): 2 County Hwy Agency
 Owner (22): 2 County Hwy Agency
 Historic Signif. (37): 5 Not eligible for NRHP

Structure Type and Material

Curb/Sidewalk (50): Left: 1.5 ft Right: 5.5 ft
 Bridge Median (33): 0 No median
 Main Span Material (43A): 5 Prestressed Concrete
 Appr Span Material (44A): Not Applicable (P)
 Main Span Design (43B): 01 Slab
 Appr Span Design (44B): 00 Other (NBI)

Appraisal**Structure Appraisal**

Open/Posted/Closed (41): P Posted for load
 Deck Geometry (68): 5 Above Tolerable
 Underclearances (69): N Not applicable (NBI)
 Approach Alignment (72): 8-No Speed Red thru Curv
 Bridge Railings (36a): 0 Substandard
 Transitions (36b): 0 Substandard
 Approach Guardrail (36c): 0 Substandard
 Approach Guardrail Ends (36d): 0 Substandard
 Scour Critical (113): U Unknown Foundation

Minimum Vertical Clearance

Over Structure (53): 99.99 ft
 Under (reference) (54a): N Feature not hwy or RR
 Under (54b): 0 ft

Schedule**Current Inspection**

Inspection Date: 04/06/2020
 Inspector: KNMEIOP - Omar Porras
 Bridge Group: CA611
 Alt. Bridge Group:
 Primary Type: Regular NBI
 Review Required: ☒

Geometrics

Spans in Main Unit (45): 3
 Approach Spans (46): 0
 Length of Max Span (48): 38.3 ft
 Structure Length (49): 100.33 ft
 Total Length: 140.33 ft
 Deck Area: 3536 sqft
 Structure Flared (35): 0 No flare

Age and Service

Year Built (27): 1967
 Year Reconstructed (106): 0
 Type of Service On (42a): 5 Highway-pedestrian
 Under (42b): 5 Waterway
 Fracture Critical Details: Not Applicable

Deck Type and Material

Deck Width (52): 35.25 ft
 Skew (34): 0 deg
 Deck Type (107): 2 Concrete Precast Panel
 Surface (108): 6 Bituminous
 Membrane: 0 None
 Deck Protection: None

Navigation Data

Navigation Control (38): Permit Not Required
 Nav Vertical Clr (39): 0 ft
 Nav Horizontal Clr (40): 0 ft
 Min Vert Lift Clr (116): 0 ft
 Pier Protection (111): 1 Not Required

NBI Condition Rating

Sufficiency Rating: 15.5
 Health Index: 86.68
 Structural Eval (67): 3 Intolerable - Correct
 Deficiency: Structurally Deficient

Minimum Lateral Underclearance

Reference (55a): N Feature not hwy or RR
 Right Side (55b): 0 ft
 Left Side (56): 0 ft

Next Inspection Date Scheduled

NBI: 04/06/2022
 Element: 10/06/2020
 Fracture Critical:
 Underwater: 04/06/2022
 Other/Special: 10/06/2020
 Inventory Photo Update Due: 04/06/2024

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 5/18/2020

Schedule Cont.**Inspection Types
Performed**NBI ☒Element ☒Fracture Critical ☐Underwater ☒Other Special ☒**Inspection Intervals****Required (92)****Frequency (92)****Last Date (93)****Inspection Resources**Fracture Critical ☐

mos

Crew Hours: 4

Underwater ☒

24 mos

04/06/2020

Flagger Hours: 0

Other Special ☒

6 mos

04/06/2020

Helper Hours: 0

NBI

24 mos

(91) 04/06/2020 (90)

Snooper Hours: 0

Special Crew Hours: 3

Special Equip Hours: 0

Bridge Related**General Bridge Information**

Parallel Bridge Seq:

Channel Depth: 10.6 ft

Radio Frequency: -1

Phone Number:

Exception Date:

Exception Type: Unknown

Accepted By Maint: 01/01/1967

Warranty Expiration: 00/00/0000

Performance Rating: Poor

Bridge Rail 1: Conc parapet-alum-rail

Bridge Rail 2: Not applicable-No rail

Electrical Devices: No electric service

Culvert Type: Not applicable

Maintenance Yard: Not FDOT Maintained

FIHS ON / OFF: No Routes on FIHS

Previous Structure:

2nd Previous Structure:

Replacement Structure:

Permitted Utilities: Power ☐Water ☒Gas ☐Fiber Optic ☐Sewage ☒Other ☐**Bridge Load Rating Information**

Inventory Type (065): 3 LRFR Load & Res. Fact

Operating Type (063): 3 LRFR Load & Res. Fact

Original Design Load (031): HL 93

Date: 01/13/2020

Initials: JA

Load Rating Rev. Recom.: No

Load Rating Plans Status: Field Measurements

Inventory Rating (066): 7.6 tons

Operating Rating (064): 11.9 tons

FL120 Permit Rating: 16.2 tons

HS20/FL120 Max Span Rating: 16.2 tons

Dynamic Impact in Percent: 33 %

Governing Span Length: 38.3 ft

Minimum Span Length: 28.3 ft

Distribution Method: Others

Load Rating Notes:

LEGAL LOADS

SU2: 11.7 tons

SU3: 12.2 tons

SU4: 11.9 tons

C3: 18.2 tons

C4: 16.9 tons

C5: 17.6 tons

ST5: 18.4 tons

Posting (070): 2 20.0-29.9%below

Open/Posted/Closed (041): P Posted for load

POSTING

Recom. SU Posting: 11 tons

Recom. C Posting: 16 tons

Recom. ST5 Posting: 18 tons

Actual SU Posting: 11 tons

Actual C Posting: 16 tons

Actual ST5 Posting: 18 tons

Actual Blanket Posting: 99 tons

Emergency Vehicle: 1 EV inapplicable

FLOOR BEAM (FB)

FB Present: No

FB Span Length, Gov: 0.0 ft

FB Spacing, Gov: 0.0 ft

FB OPR Rating: 0.0 tons

FB SU4 OPR Rating: 0.0 tons

FB FL120 Rating: 0.0 tons

SEGMENTAL (SEG)

SEG Wing-Span: -1.0 ft

SEG Web-to-Web Span: -1.0 ft

SEG Transverse HL93 Operating: -1.00 RF

Bridge Scour and Storm Information

Pile Driving Record: No pile driving records

Foundation Type: Unknown

Mode of Flow: Tidal

Rating Scour Eval: Unknown

Highest Scour Eval: Unknown

Scour Evaluation Method:

Scour Recommended I: Unknown

Scour Recommended II: Unknown

Scour Recommended III: Unknown

Scour Elevation: -1 ft

Action Elevation: -1 ft

Storm Frequency: -1

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 5/18/2020

Elements

Inspection Date: 04/06/2020 GZJW

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3178	89.88	114	3.22	244	6.9	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	114	59.07	79	40.93	0	.	193 (SF)
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	20	100	0	.	20 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	144	100	0	.	144 (SF)
0	510 / 3	Wearing Surfaces	1929	73.23	0	.	705	26.77	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	705	100	0	.	705 sq.ft

DECKS : Joints

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	301 / 3	Pourable Joint Seal	0	.	0	.	104	74.29	36	25.71	140 ft
0	2310 / 3	Leakage	0	.	0	.	104	100	0	.	104 ft
0	2330 / 3	Seal Damage	0	.	0	.	0	.	36	100	36 ft

MISCELLANEOUS : Channel

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8290 / 3	Channel	0	.	0	.	1	100	0	.	1 (EA)
0	9150 / 3	Bank Erosion	0	.	0	.	1	100	0	.	1 (EA)

MISCELLANEOUS : Other Elements

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	321 / 3	Re Conc Approach Slab	1410	100	0	.	0	.	0	.	1410 sq.ft
0	510 / 3	Wearing Surfaces	957	91.14	0	.	93	8.86	0	.	1050 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	93	100	0	.	93 sq.ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	205 / 3	Re Conc Column	0	.	0	.	4	100	0	.	4 each
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 each
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	3	100	0	.	3 each

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	215 / 3	Re Conc Abutment	65	92.86	0	.	5	7.14	0	.	70 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	0	.	5	100	0	.	5 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	234 / 3	Re Conc Pier Cap	49	72.06	12	17.65	7	10.29	0	.	68 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	12	63.16	7	36.84	0	.	19 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8393 / 3	Bulkhead Seawall Any Material	0	.	0	.	354	100	0	.	354 ft
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	314	100	0	.	314 ft

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 5/18/2020

0	6000 / 3	Scour	0	.	0	.	40	100	0	.	40 ft
---	----------	-------	---	---	---	---	----	-----	---	---	-------

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8394 / 3	R/Conc Abut Slope Protection	3968	73.81	0	.	1408	26.19	0	.	5376 (SF)
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	320	100	0	.	320 (SF)
0	4000 / 3	Settlement	0	.	0	.	1088	100	0	.	1088 (SF)

SUPERSTRUCTURE : Superstructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	333 / 3	Other Bridge Railing	167	83.5	33	16.5	0	.	0	.	200 ft
0	1000 / 3	Corrosion	0	.	30	100	0	.	0	.	30 ft
0	1020 / 3	Connection	0	.	3	100	0	.	0	.	3 ft

Total Number of Elements*: 10

*excluding defects/protective systems

Inspection Information**Inspection Date:** 04/06/2020**Type:** Regular NBI**Inspector:** KNMEIOP - Omar Porras**Inspection Notes:** Sufficiency Rating Calculation Accepted by knmeira at 5/13/2020 9:36:35 AM

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/06/2020)

The Substructure NBI Rating is coded 4 (Poor) due to the significant deterioration of Column 2-2. (04/06/2020)

The Channel NBI Rating was lowered from 7 to 6 due to areas of undermining on the channel below the North seawall. (04/06/2020)

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 04/06/2020 per Julie A.Vers, P.E.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure.

Element 8475 R/Conc Walls was replaced by 8393 Bulkhead Seawall Any Material during this inspection cycle. All previous notes were transferred accordingly. (04/06/2020)

The following elements were inspected underwater by the divers:

8290 Channel

8393 Bulkhead Seawall Any Material

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED.

RT: Right

LT: Left

NC: No Change

INC: Increase

CAT: Corrective Action Taken

L: Long

W: Wide

H: High

D: Deep

UW: Underwater

S.L.: Section Loss

in.: Inches

ft.: Feet

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

REPORT ID: INSP005

Inspection/CIDR/Bridge Profile Report with PDF attachment(s)

Structure ID: 874294

CIDRDATE PRINTED: 5/18/2020

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north.

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

Element 227/3 Re Conc Pile notes have been replaced by Element 205/3 Re Conc Column on 10/29/2019.

TRAFFIC RESTRICTIONS:

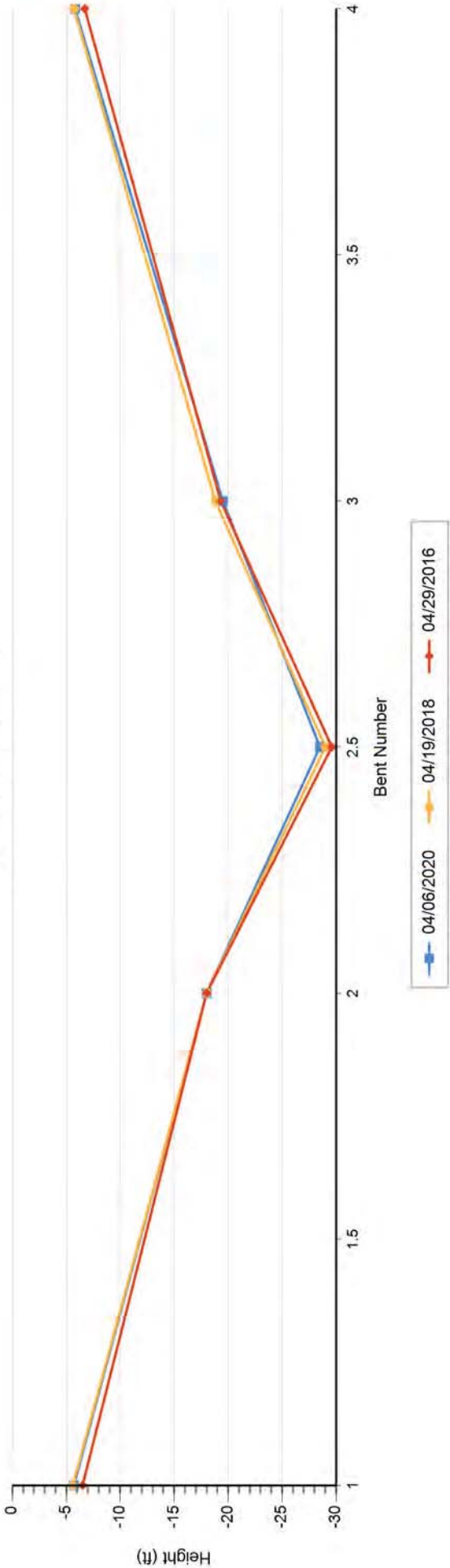
Based on the current load rating analysis dated 1/13/2020, it is recommended that this bridge be posted for the SU, C and ST5 type vehicles as follows: SU = 11 tons, C = 16 tons, ST5 = 18 tons. The bridge is currently posted for SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 33 and 34.

REVIEWED BY:

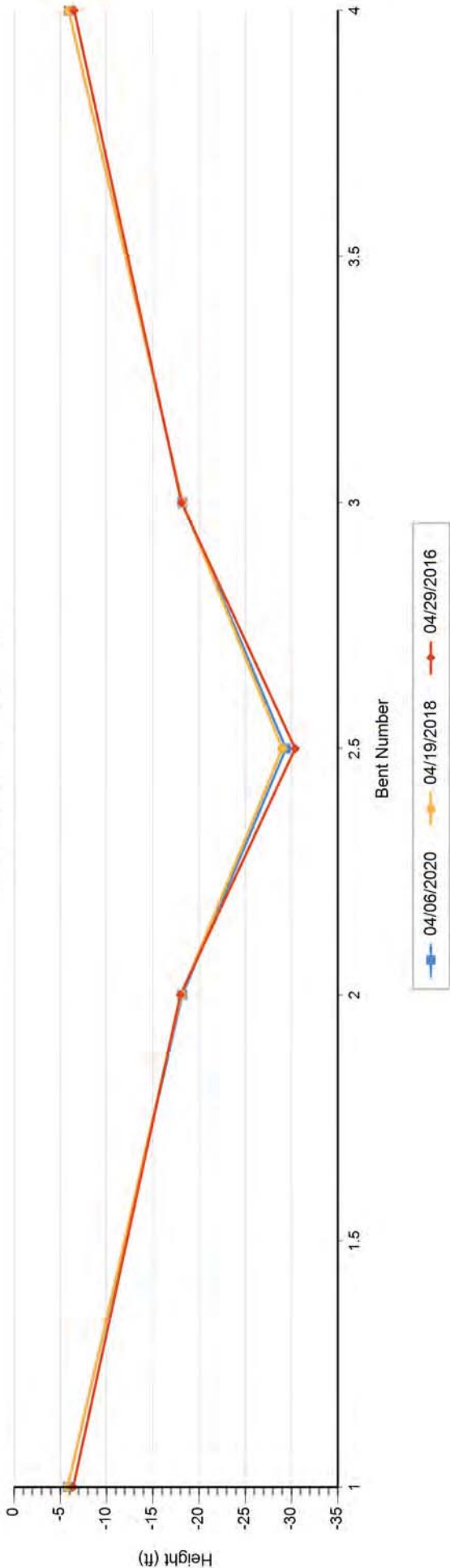
Schedule Notes

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure.

Left Profile by Inspection



Right Profile by Inspection



Profile Data - Numerical Summary

Inspection Date and Key: 4/6/2020	GZJW	Bent #	Left Height	Right Height	(All Heights are in Feet)
		1	5.70	5.80	
		2	18.00	18.20	
		2.5	28.50	29.40	
		3	19.50	18.20	
		4	5.80	5.90	

Air Temp: 82

Profile Notes:

Measurements were referenced from the top of the concrete barriers.
Waterline taken at mid channel: Left = 18.7 ft. and Right = 18.8 ft.
Maximum channel depth: 10.6 ft.

Inspection Date and Key: 4/19/2018

ODLG

1	5.60	5.80
2	18.00	18.10
2.5	29.00	29.00
3	18.80	18.20
4	5.70	5.90

Air Temp: 74

Profile Notes:

Measurements were referenced from the top of the concrete barriers.
Waterline taken at mid channel: Left = 18.3 ft. and Right = 18.4 ft.
Maximum channel depth: 10.7 ft.

Profile Data - Numerical Summary

Inspection Date and Key:	Bent #	Left Height	Right Height	(All Heights are in Feet)
4/29/2016 MOSY	1	6.50	6.40	
	2	18.00	18.00	
	2.5	29.60	30.40	
	3	19.30	18.10	
	4	6.70	6.50	

Air Temp: 1
Profile Notes:

Measurements referenced from the top of the concrete bridge rail.
Waterline at C/L of Channel = 19.2ft.
Water depth = 11.2ft.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 1 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Bridge Number - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 2 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Typical Bridge Rail - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 3 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Southeast Oncoming Transition - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 4 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Northwest Oncoming Transition - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 5 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Southwest Off-Going Transition - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 6 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Northeast Off-Going Transition - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 7 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



South Approach Looking North - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 8 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



South Approach Looking South - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 9 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



North Approach Looking South - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 10 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



North Approach Looking North - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 11 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



West Elevation - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 12 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



East Elevation - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 13 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Typical Underside - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 14 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Channel Looking West - 4/25/2014

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
STRUCTURE LEVEL INVENTORY REPORT

Page 15 of 15

BRIDGE ID : 874294

Structure Inventory Photo Due Date : 04/06/2024



Channel Looking East - 4/25/2014



BRIDGE INSPECTION REPORT

PREPARED FOR: FDOT District 6
 BRIDGE OWNER: Miami-Dade County
 INSPECTION TYPE: Interim CONTRACT No. CA611

Inspected by:
LARS Engineering, Inc.

Bridge No. 874294

REPORT CONTAINS

Inspection Date: 10-22-20

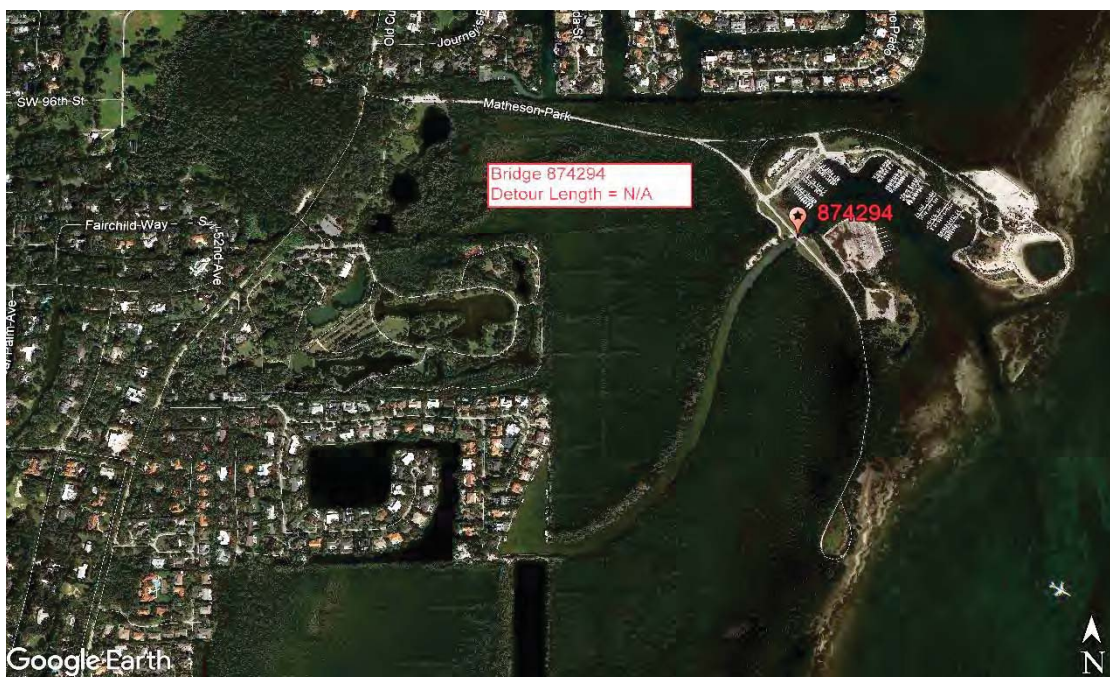
- | | | | |
|---|---|---|---|
| <input checked="" type="checkbox"/> BrM Inspection Report | <input type="checkbox"/> Bridge Profile | <input type="checkbox"/> Fracture Critical Data | <input type="checkbox"/> Addendum |
| <input checked="" type="checkbox"/> CIDR Information | <input type="checkbox"/> UW Inspection Report | <input checked="" type="checkbox"/> Load Rating Summary Sheet | <input type="checkbox"/> Mechanical and Electrical Data |



**Matheson Hammock Road over
 Matheson Hammock Canal**

Facility Carried & Location

Matheson Hammock Park



Location Map

Detour Length = 3.13 mi.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM****Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)****Structure ID: 874294****Inspection****DISTRICT: D6 - Miami****INSPECTION DATE: 10/22/2020 MIGV**

BY:	LARS Engineering, Inc.	STRUCTURE NAME:	Not recorded
OWNER:	2 County Hwy Agency	YEAR BUILT:	1967
MAINTAINED BY:	2 County Hwy Agency	SECTION NO.:	87 000 757
STRUCTURE TYPE:	5 Prestressed Concrete - 01 Slab	MP:	0.080
LOCATION:	Matheson Hammock Park	ROUTE:	00000
SERV. TYPE ON:	5 Highway-pedestrian	FACILITY CARRIED:	Matheson Hmk Road
SERV. TYPE UNDER:	5 Waterway	FEATURE INTERSECTED:	Matheson Hammock Canal

☐ FUNCTIONALLY OBSOLETE☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Interim

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 10/22/2020 UNDERWATER: 4/6/2020

SUFFICIENCY RATING:	15.5
HEALTH INDEX:	85.67

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

BY: LARS Engineering, Inc.
 OWNER: 2 County Hwy Agency
 MAINTAINED BY: 2 County Hwy Agency
 STRUCTURE TYPE: 5 Prestressed Concrete - 01 Slab
 LOCATION: Matheson Hammock Park
 SERV. TYPE ON: 5 Highway-pedestrian
 SERV. TYPE UNDER: 5 Waterway

STRUCTURE NAME: Not recorded
 YEAR BUILT: 1967
 SECTION NO.: 87 000 757
 MP: 0.080
 ROUTE: 00000
 FACILITY CARRIED: Matheson Hmk Road
 FEATURE INTERSECTED: Matheson Hammock Canal

- ☐ THIS BRIDGE CONTAINS FRACTURE CRITICAL COMPONENTS
- ☐ THIS BRIDGE IS SCOUR CRITICAL
- ☒ THIS REPORT IDENTIFIES DEFICIENCIES WHICH REQUIRE PROMPT CORRECTIVE ACTION
- ☐ FUNCTIONALLY OBSOLETE ☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Interim

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 10/22/2020 UNDERWATER: 4/6/2020

OVERALL NBI RATINGS:

DECK: 3 Serious	CHANNEL: 6 Bank Slumping
SUPERSTRUCTURE: 3 Serious	CULVERT: N N/A (NBI)
SUBSTRUCTURE: 4 Poor	SUFF. RATING: 15.5
PERF. RATING: Poor	HEALTH INDEX: 85.67

FIELD PERSONNEL / TITLE / NUMBER:**INITIALS**

Marquez, Loren - Professional Engineer (P.E. # 85631) (lead)

Lledias, Jorge - Bridge Inspector Assistant

REVIEWING BRIDGE INSPECTION SUPERVISOR:

Leon, Adrian - Professional Engineer (P.E. #83827)

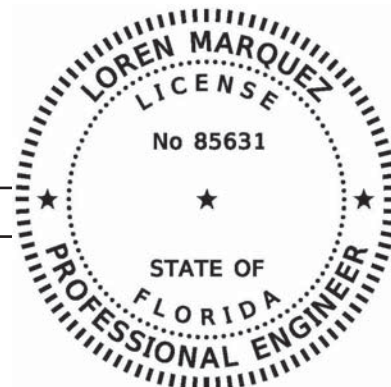
CONFIRMING REGISTERED PROFESSIONAL ENGINEER:

Marquez, Loren - Professional Engineer (P.E. # 85631) LARS Engineering, Inc.
 7225 NW 25th Street
 Suite 211
 Miami Florida 33122

SIGNATURE: _____

DATE: _____

The official record of this package has been electronically signed and sealed by Loren Marquez, P.E. on the date adjacent to the seal as required by Rule 61G15-23.004, F.A.C. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.



This report contains information relating to the physical security of a structure and depictions of the structure. This information is confidential and exempt from public inspection pursuant to sections 119.071(3)(a) and 119.071(3)(b), Florida Statutes. Only the cover page of this report may be inspected and copied.

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

All Elements

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3122	88.29	5	0.14	409	11.57	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	5	45.45	6	54.55	0	.	11 (SF)
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	20	100	0	.	20 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	292	100	0	.	292 (SF)
0	1900 / 3	Distortion	0	.	0	.	90	100	0	.	90 (SF)
0	510 / 3	Wearing Surfaces	1629	61.85	0	.	1005	38.15	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	1005	100	0	.	1005 sq.ft

Element Inspection Notes:

8099/3 Notes: The top of the slab units is not visible due to an asphalt overlay. The width of the sonovoid slab units was field verified to be 3ft. wide.

SECONDARY:

_Object markers and centerline raised pavement markers are missing on the structure. (14 SF). - NO CHANGE. Refer to Photo 01.

_Sidewalk panels are loose and move under pedestrian load. (300 SF). - NO CHANGE.

_The slab unit joints show evidence of water seepage. - NO CHANGE. NCAR.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

- 1_Replace missing object markers at the four corners of the bridge.
- 2_Properly secure the sidewalk panels.
- 3_Repair spalls, delaminations, and cracks along the underside of the slab units.
- 4_Clean and coat exposed prestressing and reinforce Slab Unit 2-8.

CORRECTIVE ACTION EVALUATION:

- 1_Work not completed. Recommendation will be repeated.
- 2_Work not completed. Recommendation will be repeated.
- 3_Work not completed. Recommendation will be repeated.
- 4_Work not completed. Recommendation will be repeated.

For additional deficiencies refer to Defects 1080, 1090, 1100, 1110, and 1900.

1080/3

CS-3:

_Slab Unit 1-9, center line has a spall/delamination up to 36in. L x 24in. W x 2.5in. D over Abutment 1, with an exposed stirrup. (6 SF). - INCREASE. Refer to Photo 02.

CS-2:

_Slab Unit 2-6, east edge has a delamination 30in. L x 4in. W starting at Pier 2 cap. (3 SF). - NO CHANGE.

_Slab Unit 2-7, west edge has a delamination up to 24in. L x 4in. W starting at Pier 2 cap. (2 SF). - NO CHANGE.

1090/3

CS-3:

_Slab Unit 1-6 exhibits a spall with exposed rebar up to 11in. L x 5in. W x 1/8in. D with minor section loss and evidence of previous failed repair, at 9ft. from Abutment 1. (1

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

SF). - NO CHANGE. Refer to Photo 03.

1100/3

CS-3:

_Slab Unit 2-8 has a spall 10ft. L x 24in. W x up to 4in. D at mid-span with 6 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (2 broken threads). (20 SF). - NO CHANGE. Refer to Photo 04.

1110/3

CS-3:

_Slab Unit 1-6 east edge has two delamination areas, one up to 5ft. L x 6in. W starting at Abutment 1 and the other starting at Pier Cap 2 up to 9ft. L x 12in. W with associated cracks up to 1/16in. W with efflorescence throughout. (Previously noted as a delamination full length x 12in. W.) (14 SF). - DECREASE. Refer to Photos 05 and 06.

_Slab Unit 1-7 east edge has a spall/delamination 24in. L x 12in. W with associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out over Abutment 1. (2 SF). - NO CHANGE. Refer to Photo 07.

_Slab Unit 1-7, east edge has a delamination 7ft. L x 4in. W, with an associated crack of up to 1/16in. starting at Pier 2 cap. (7 SF). - INCREASE. Refer to Photo 08.

_Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W starting at Abutment 1 with associated cracks up to 1/4in. W with efflorescence and corrosion bleed-out and associated spalling up to 4ft. L x 6in. W x 2in. D approximately 10ft from Abutment 1. (Spalling was previously noted as spall/delamination on the east edge) (19 SF). - INCREASE. Refer to Photos 09 and 10.

_Slab Unit 1-8 east edge has a delamination 4ft. L x 15in. W and associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out, 9ft. from Pier Cap 2. (Previously noted as spall/delamination near mid-span). (5 SF). - DECREASE. Refer to Photo 11.

_Slab Unit 1-8 has a delaminated area up to 8ft. L x 3ft. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out starting at Pier Cap 2. (24 SF). - INCREASE. Refer to Photo 12.

_Slab Unit 1-9 west edge has a delaminated area 9ft. L x 10in. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out, starting near the 3/4 point and extending to Pier 2 cap. (9 SF). - NO CHANGE. Refer to Photo 13.

_Slab Unit 2-7 east edge is intermittently cracked/delaminated up to span length x 16in. W (average width) with up to 1/4in. W cracks. (38 SF). - NO CHANGE. Refer to Photo 14.

_Slab Unit 2-8 west half has two delaminated areas up to 15ft. L x 18in. W (average width) at south and north ends, with associated cracks of up to 1/4in. W. (60 SF). - NO CHANGE. Refer to Photo 15.

_Slab Unit 2-9 west edge has a delaminated area up to 5ft. L x 5in. W with associated cracking up to 1/4in. wide, starting at the Pier 2 cap. (5 SF). - NO CHANGE.

_Slab Unit 3-6 has a delamination up to 24in. L x 6in. W on the east edge over Pier 3, with an associated crack of up to 1/16in. W. (2 SF). - INCREASE. Refer to Photo 16.

_Slab Unit 3-6 east edge has a delaminated area up to 42in. L x 8in. W with associated cracks up to 1/16in. W. (4 SF). - NEW. Refer to Photo 17.

_Slabs Unit 3-7 has two delaminated areas, one starting at Pier 3 up to 8ft. L x 15in. W (average width) with associated cracks, and the second, near mid-span up to 3ft. L x 30in. W. (25 SF). - NO CHANGE. Refer to Photos 18 and 19.

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

_Slab Unit 3-7 has an unsound repaired area 12ft. L x up to slab width (3ft.) starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out. (30 SF). - INCREASE. Refer to Photo 20.

_Slab Unit 3-8 has a spall/delamination up to 8ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3. (24 SF). - INCREASE. Refer to Photo 21.

_Slab Unit 3-8 has an unsound repair/delamination up to 42in. L x 30in. W with associated cracks up to 1/16in. W with efflorescence starting at Abutment 4. (9 SF). - INCREASE. Refer to Photo 22.

_Slab Unit 3-8 has an unsound repair/delamination up to 74in. L x up to slab width (3ft.) with associated cracks up to 1/16in. W with efflorescence starting 5.5ft. from Abutment 4. (15 SF). - INCREASE. Refer to Photo 23.

1900/3

CS-3:

_Slab Unit 1-1 exhibits a slight outward rotation at Abutment 1 with up to 1/4in. height difference in reference to the top of the cap, potentially indicating shear key failure. (90 SF). - NO CHANGE. Refer to Photo 24.

510/3

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

- 1_Monitor the slab units for independent movement.
- 2_Repair cracks on the asphalt along the slab unit joints.
- 3_Clean and repair cracks and rutting along the expansion joints.

CORRECTIVE ACTION EVALUATION:

- 1_Work not completed. Recommendation will be repeated.
- 2_Work not completed. Recommendation will be repeated.
- 3_Work not completed. Recommendation will be repeated.

For deficiencies refer to Defect 3220.

3220/3

CS-3:

_The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated 1in. W rutting over the slab unit joints and upheaving up to 1in. H at the shoulders, possibly indicating independent slab unit movement. (600 SF). - NO CHANGE. Refer to Photos 25 and 26.

_The asphalt overlay at Spans 1 and 2 has multi-directional cracking up to 1/2in. W on Lane 2 (NB), worse condition is on Span 1 which has a 19.5ft L x 11ft. W area with hollow-sounding starting 1 ft. from the right sidewalk. (300 SF). - NEW. Refer to Photo 27.

_The asphalt overlay has transverse cracks up to roadway width x 1/4in. W with rutting and upheaving up to 3in. W and vegetation growth over the expansion joints. (105 SF). - NO CHANGE. Refer to Photo 28.

Total Number of Elements*: 1

*excluding defects/protective systems

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

Inspector Recommendations

UNIT: 0 DECKS
ELEMENT/ENV: 8099 / 3 PS Conc Slab (Sonovoid) ELEM CATEGORY: Decks/Slabs

CONDITION STATE			PRIORITY
1, 2, 3	MMS Quantity: 14 sf	Element Estimated Quantity: 14 (SF)	3
WORK ORDER RECOMMENDATION:			
_Replace missing object markers at the four corners of the bridge and provide missing RPMs throughout the bridge. Refer to Photo 01.			
1, 2, 3	MMS Quantity: 300 sf	Element Estimated Quantity: 300 (SF)	3
WORK ORDER RECOMMENDATION:			
_Properly secure the sidewalk panels.			

ELEMENT/ENV: 8099:510:3220 / 3 Crack (Wearing Surface) ELEM CATEGORY: Decks/Slabs

CONDITION STATE			PRIORITY
3	MMS Quantity: 900 sf	Element Estimated Quantity: 900 sq.ft	3
WORK ORDER RECOMMENDATION:			
_Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2. Refer to Photos 25, 26, and 27.			
3	MMS Quantity: 105 sf	Element Estimated Quantity: 105 sq.ft	3
WORK ORDER RECOMMENDATION:			
_Clean and seal cracks and rutting along the expansion joints. Refer to Photo 28.			
3	MMS Quantity: 600 sf	Element Estimated Quantity: 600 sq.ft	3
WORK ORDER RECOMMENDATION:			
_Monitor cracks along slab unit joints for independent movement of the slab units. Refer to Photos 25 and 26.			

ELEMENT/ENV: 8099:1080 / 3 Delamination/Spall/Patched Area ELEM CATEGORY: Decks/Slabs

CONDITION STATE			PRIORITY
2, 3	MMS Quantity: 303 sf	Element Estimated Quantity: 303 (SF)	3
WORK ORDER RECOMMENDATION:			
_Repair spalls, delaminations, and cracks along the underside of the slab units. Refer to Photos 02 and 05 through 23.			

ELEMENT/ENV: 8099:1090 / 3 Exposed Rebar ELEM CATEGORY: Decks/Slabs

CONDITION STATE			PRIORITY
3	MMS Quantity: 1 sf	Element Estimated Quantity: 1 (SF)	3
WORK ORDER RECOMMENDATION:			
_Clean and coat exposed rebar and repair spall along the underside of slab unit 1-6, 9ft. from Abutment 1. Refer to Photo 03.			

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

Inspector Recommendations

UNIT: 0 **DECKS**
ELEMENT/ENV: 8099:1100 / 3 Exposed Prestressing **ELEM CATEGORY: Decks/Slabs**

CONDITION STATE			PRIORITY
3	MMS Quantity: 20 sf	Element Estimated Quantity: 20 (SF)	3
WORK ORDER RECOMMENDATION:			
_Clean and coat exposed prestressing and reinforce Slab Unit 2-8. Refer to Photo 04.			

ELEMENT/ENV: 8099:1900 / 3 Distortion **ELEM CATEGORY: Decks/Slabs**

CONDITION STATE			PRIORITY
3	MMS Quantity: 90 sf	Element Estimated Quantity: 90 (SF)	3
WORK ORDER RECOMMENDATION:			
_Monitor slab unit 1-1 for possible independent movement on the slab unit. Refer to Photo 24.			

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north. (Entrance on North end, boat ramp on South end).

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

Element 227/3 Re Conc Pile notes have been replaced by Element 205/3 Re Conc Column on 10/29/2019.

Element 8475/3 R/Conc Walls notes have been replaced by Element 8393/3 Bulkhead Seawall Any Material on 04/06/2020.

The NBI Rating for Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/06/2020).

The Substructure NBI Rating is coded 4 (Poor) due to the significant deterioration of Column 2-2. (04/06/2020).

The Channel NBI Rating was lowered from 7 to 6 due to areas of undermining on the channel below the North seawall. (04/06/2020).

TRAFFIC RESTRICTIONS:

Based on the current load rating analysis dated 1/13/2020, it is recommended that this bridge be posted for the SU, C and ST5 type vehicles as follows: SU = 11 tons, C = 16 tons, ST5 = 18 tons. The bridge is currently posted for SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 29 and 30.

REVIEWED BY:

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

INSPECTION NOTES: **MIGV** **10/22/2020**

Sufficiency Rating Calculation Accepted by KNLREJP at 11/18/2020 2:56:35 PM

This Interim inspection (10/22/2020) was conducted to evaluate Element 8099 PS Conc Slab (Sonovoid), for the status of the entire structure refer to the last Regular NBI Inspection (04/06/2020).

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 10/22/2020 per Loren Marquez, P.E.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure.

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (10/22/2020).

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED

RT: Right

LT: Left

L: Long

W: Wide

H: High

D: Deep

in.: Inches

ft.: Feet

LF: Linear Feet

SF: Square Feet

NE: Northeast

NW: Northwest

SE: Southeast

SW: Southwest

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM****Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)****Structure ID: 874294****Inspection****DISTRICT: D6 - Miami****INSPECTION DATE: 10/22/2020 MIGV**

PHOTO 01: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Object markers and centerline raised pavement markers are missing on the structure.

REPAIR RECOMMENDATION:

Replace missing object markers at the four corners of the bridge and provide missing RPMs throughout the bridge.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 02: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-9, center line has a spall/delamination up to 36in. L x 24in. W x 2.5in. D over Abutment 1, with an exposed stirrup.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 03: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-6 exhibits a spall with exposed rebar up to 11in. L x 5in. W x 1/8in. D with minor section loss and evidence of previous failed repair, at 9ft. from Abutment 1.

REPAIR RECOMMENDATION:

Clean and coat exposed rebar and repair spall along the underside of slab unit 1-6, 9ft. from Abutment 1.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 04: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 2-8 has a spall 10ft. L x 24in. W x up to 4in. D at mid-span with 6 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (2 broken threads).

REPAIR RECOMMENDATION:

Clean and coat exposed prestressing and reinforce Slab Unit 2-8.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 05: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-6 east edge has two delamination areas, one up to 5ft. L x 6in. W starting at Abutment 1 and the other starting at Pier Cap 2 up to 9ft. L x 12in. W with associated cracks up to 1/16in. W with efflorescence throughout. (Abutment 1 shown).

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 06: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-6 east edge has two delamination areas, one up to 5ft. L x 6in. W starting at Abutment 1 and the other starting at Pier Cap 2 up to 9ft. L x 12in. W with associated cracks up to 1/16in. W with efflorescence throughout. (Pier Cap 2 shown).

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 07: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-7 east edge has a spall/delamination 24in. L x 12in. W with associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out over Abutment 1.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV

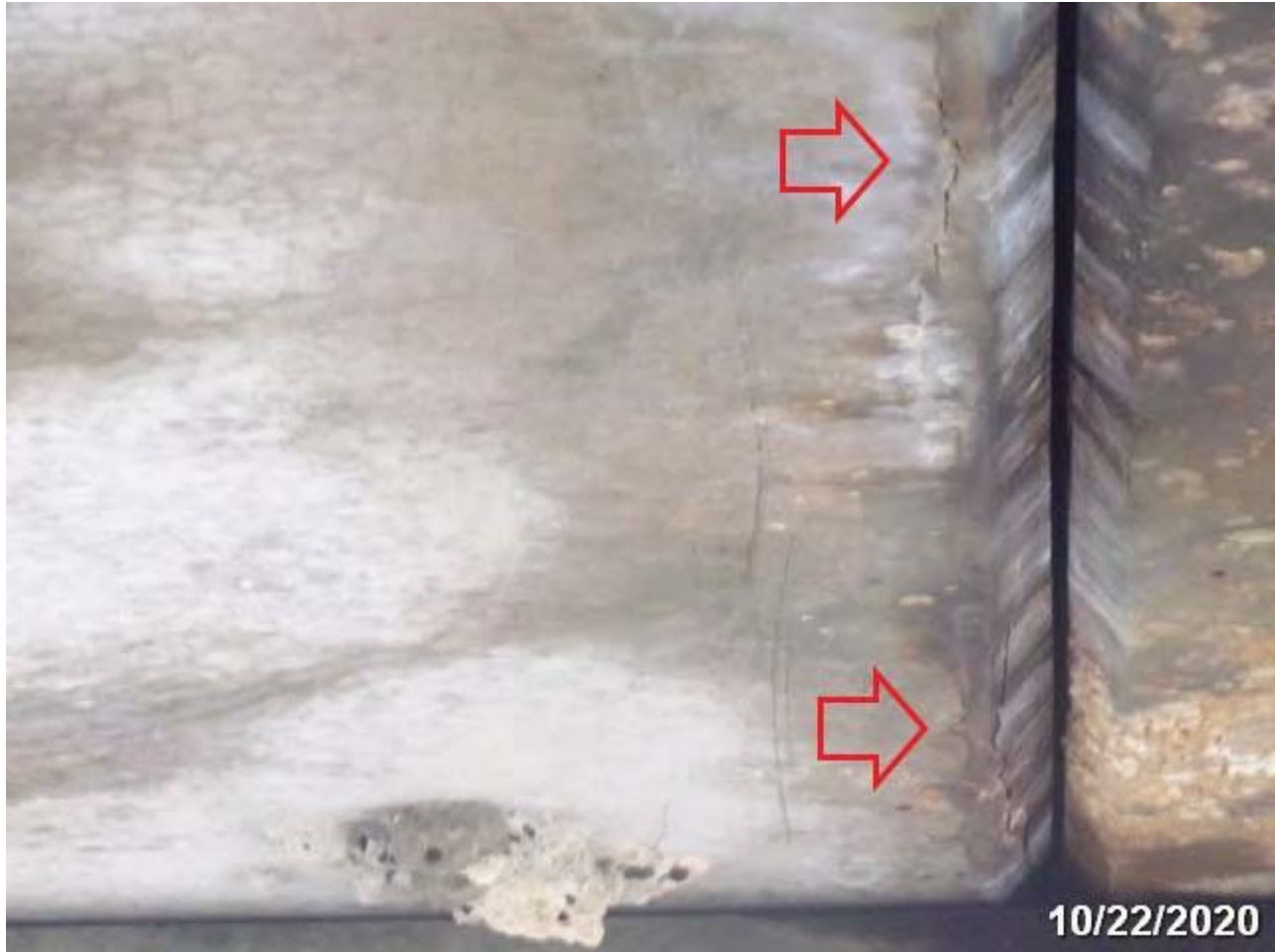


PHOTO 08: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-7, east edge has a delamination 7ft. L x 4in. W, with an associated crack of up to 1/16in. starting at Pier 2 cap.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 09: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W starting at Abutment 1 with associated cracks up to 1/4in. W with efflorescence and corrosion bleed-out and associated spalling up to 4ft. L x 6in. W x 2in. D approximately 10ft from Abutment 1.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 10: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W starting at Abutment 1 with associated cracks up to 1/4in. W with efflorescence and corrosion bleed-out and associated spalling up to 4ft. L x 6in. W x 2in. D approximately 10ft from Abutment 1.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 11: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-8 east edge has a delamination 4ft. L x 15in. W and associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out, 9ft. from Pier Cap 2.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 12: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-8 has a delaminated area up to 8ft. L x 3ft. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out starting at Pier Cap 2.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 13: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-9 west edge has a delaminated area 9ft. L x 10in. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out, starting near the 3/4 point and extending to Pier 2 cap.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 14: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 2-7 east edge is intermittently cracked/delaminated up to span length x 16in. W (average width) with up to 1/4in. W cracks.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 15: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 2-8 west half has two delaminated areas up to 15ft. L x 18in. W (average width) at south and north ends, with associated cracks of up to 1/4in. W.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 16: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-6 has a delamination up to 24in. L x 6in. W on the east edge over Pier 3, with an associated crack of up to 1/16in. W.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 17: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-6 east edge has a delaminated area up to 42in. L x 8in. W with associated cracks up to 1/16in. W.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 18: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slabs Unit 3-7 has two delaminated areas, one starting at Pier 3 up to 8ft. L x 15in. W (average width) with associated cracks, and the second, near mid-span up to 3ft. L x 30in. W. (Pier 3 shown).

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 19: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slabs Unit 3-7 has two delaminated areas, one starting at Pier 3 up to 8ft. L x 15in. W (average width) with associated cracks, and the second, near mid-span up to 3ft. L x 30in. W. (Mid-span shown).

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 20: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-7 has an unsound repaired area 12ft. L x up to slab width (3ft.) starting from Abutment 4 with hollow-sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 21: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-8 has a spall/delamination up to 8ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 22: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-8 has an unsound repair/delamination up to 42in. L x 30in. W with associated cracks up to 1/16in. W with efflorescence starting at Abutment 4.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 23: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 3-8 has an unsound repair/delamination up to 74in. L x up to slab width (3ft.) with associated cracks up to 1/16in. W with efflorescence starting 5.5ft. from Abutment 4.

REPAIR RECOMMENDATION:

Repair spalls, delaminations, and cracks along the underside of the slab units.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 24: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

Slab Unit 1-1 exhibits a slight outward rotation at Abutment 1 with up to 1/4in. height difference in reference to the top of the cap, potentially indicating shear key failure.

REPAIR RECOMMENDATION:

Monitor slab unit 1-1 for possible independent movement of the slab unit.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 25: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated 1in. W rutting over the slab unit joints and upheaving up to 1in. H at the shoulders, possibly indicating independent slab unit movement.

REPAIR RECOMMENDATION:

- 1) Monitor cracks along slab unit joints for independent movement of the slab units.
- 2) Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 26: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated 1in. W rutting over the slab unit joints and upheaving up to 1in. H at the shoulders, possibly indicating independent slab unit movement.

REPAIR RECOMMENDATION:

- 1) Monitor cracks along slab unit joints for independent movement of the slab units.
- 2) Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 27: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

The asphalt overlay at Spans 1 and 2 has multi-directional cracking up to 1/2in. W on Lane 2 (NB), worse condition is on Span 1 which has a 19.5ft L x 11ft. W area with hollow-sounding starting 1 ft. from the right sidewalk.

REPAIR RECOMMENDATION:

Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 28: ELEMENT/ENV: 8099/3 PS Conc Slab (Sonovoid)

The asphalt overlay has transverse cracks up to roadway width x 1/4in. W with rutting and upheaving up to 3in. W and vegetation growth over the expansion joints.

REPAIR RECOMMENDATION:

Clean and seal cracks and rutting along the expansion joints.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 29: STRUCTURE NOTES

South Approach Posting Sign.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 10/22/2020 MIGV



PHOTO 30: STRUCTURE NOTES

North Approach Posting Sign.

Bridge No.	874294	Analysis Method:	LRFR-LRFD	FDOT Bridge Load Rating Summary Form (Page 1 of 1)
Location	Matheson hammock Road over matheson Hammock Canal			
Description	3 Spans, 2-30'&1-40', Prestressed voided slab beams 36"x17"			

Rating Type	Rating Type	Gross Axle Weight (tons)	Moment/Shear/Service		Dead Load Factor	Live Load Factor	Live Load Distrib. Factor (axles)	Rating Factor	Span No. - Girder No., Interior/Exterior, %Span Length	RF-Weight (tons)
Level	Vehicle	Weight	Member Type	Limit	DC	LL	LLDF	RF	Governing Location	RATING
Inventory	HL93	36	Prestressed	Service	1.00	0.80	0.600	0.210	Central span, midspan	7.6
Operating	HL93	36	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.330	Central span, midspan	11.9
Permit	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Permit Max Span	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Legal	SU2	17	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.690	Central span, midspan	11.7
	SU3	33	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.370	Central span, midspan	12.2
	SU4	35	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.340	Central span, midspan	11.9
	C3	28	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.650	Central span, midspan	18.2
	C4	36.7	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	16.9
	C5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.440	Central span, midspan	17.6
	ST5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	18.4
Emergency Vehicle (EV)	EV2	28.75	Prestressed	NA	NA	NA	0.600			-1
	EV3	43	Prestressed	NA	NA	NA	0.600			-1

Original Design Load	HS20 or HS20-S16-44	Performed by:	Mengyuan Chen	Date:	01/13/20
Rating Type, Analysis	LRFR-LRFD	Checked by:	Juan A. Sobrino	Date:	01/13/20
Distribution Method	Others	Sealed By:	Juan A. Sobrino	Date:	01/13/20
Impact Factor	33.0% (axle loading)	FL P.E. No.:	73121		
FL120 Gov. Span Length	38.3 (feet)	Cert. Auth. No.:	27244		
Minimum Span Length	28.3 (feet)	Phone & email:	(+1) 305 648 00 10, miami@pedelta.om		
Recommended Posting	> 39.9% below (0.000-0.600) (Required)		Company:	Pedelta Inc.	
Recommended SU Posting*	11 (tons)	P.E. Seal/Comments by the Engineer	Address:	2000 Ponce de Leon Blvd., Suite 624, Coral Gables, Florida 33134, USA	
Recommended C Posting	16 (tons)		<div><div>Juan Sobrino</div><div>Digitally signed by Juan Sobrino</div><div>Date: 2020.01.13 15:58:25 -05'00'</div></div> <div>Juan A. Sobrino, State of Florida, Professional Engineer, License No 73121. This document has been electronically signed and sealed by Juan A. Sobrino on January 13th, 2020 using a SHA authentication code. Printed copies of this document are not considered signed and sealed and the SHA authentication code must be verified on any electronic copies.</div>		
Recommended ST5 Posting	18 (tons)				
Owner	02 County Highway Agency				
Location	Neither interstate traffic nor within 1 mile reasonable access to an interstate				
EV Posting	No. EV posting is not recommended. The FAST Act does not apply.				
Floor Beam Present?	No				
Segmental Bridge?	No				
Project No. & Reason	432907-1-72-02 Deterioration				
Plans Status	Built				

This 10-11-2019 summary follows the FDOT Bridge Load Rating Manual (BLRM), and the FDOT BMS Coding Guide.

*Recommended SU Posting levels for Florida SU trucks adequately restricts AASHTO SU trucks; see BLRM Chapter 7.

fdot.gov/maintenance/LoadRating.shtm

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 11/24/2020

Description

Structure Unit Identification

Bridge/Unit Key: 874294 0
 Structure Name:
 Description: SPANS 1 THRU 3
 Type: M - Main

Roadway Identification

NBI Structure No (8): 874294
 Position/Prefix (5): 1 - Route On Structure
 Kind Hwy (Rte Prefix): 4 County Hwy
 Design Level of Service: 8 Service Road
 Route Number/Suffix: 00000 / 0 N/A (NBI)
 Feature Intersect (6): Matheson Hammock Canal
 Critical Facility: Not Defense-crit
 Facility Carried (7): Matheson Hmk Road
 Mile Point (11): 0.08
 Latitude (16): 025d40'44.2" Long (17): 080d15'43.8"

Roadway Traffic and Accidents

Lanes (28): 2 Medians: 0 Speed: 15 mph
 ADT Class: 2 ADT Class 2
 Recent ADT (29): 736 Year (30): 2014
 Future ADT (114): 1168 Year (115): 2041
 Truck % ADT (109): 1
 Detour Length (19): 99 mi
 Detour Speed:
 Accident Count: -1 Rate:

Roadway Classification

Nat. Hwy Sys (104): 0 Not on NHS
 National base Net (12): 0 - Not on Base Network
 LRS Inventory Rte (13a): 87 000 757 Sub Rte (13b): 00
 Functional Class (26): 09 Rural Local
 Federal Aid System: OFF
 Defense Hwy (100): 0 Not a STRAHNET hwy
 Direction of Traffic (102): 2 2-way traffic
 Emergency: ☒

Roadway Clearances

Vertical (10): 99.99 ft Appr. Road (32): 26.25 ft
 Horiz. (47): 26.25 ft Roadway (51): 26.25 ft
 Truck Network (110): 0 Not part of natl netwo
 Toll Facility (20): 3 On free road
 Fed. Lands Hwy (105): 0 N/A (NBI)
 School Bus Route: ☐
 Transit Route: ☐

NBI Project Data

Proposed Work (075A): Not Applicable (P)
 Work To Be Done By (075B): Not Applicable (P)
 Improvement Length (076): 0 ft

Improvement Cost (094): \$ 0.00
 Roadway Improvement Cost (095): \$ 0.00
 Total Cost (096): \$ 0.00
 Year of Estimate (097):

NBI Rating

Channel (61): 6 Bank Slumping
 Deck (58): 3 Serious
 Superstructure (59): 3 Serious
 Substructure (60): 4 Poor

Culvert (62): N N/A (NBI)
 Waterway (71): 8 Equal Desirable
 Unrepaired Spalls: -1 sq.ft.
 Review Required: ☒

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 11/24/2020

Structure Identification

Admin Area: Miami-Dade
 District (2): D6 - Miami
 County (3): (87)Miami-Dade
 Place Code (4): South Miami Heights
 Location (9): Matheson Hammock Park
 Border Br St/Reg (98): Not Applicable (P) Share: 0 %
 Border Struct No (99):
 FIPS State/Region (1): 12 Florida Region 4-Atlanta
 NBIS Bridge Len (112): Y - Meets NBI Length
 Parallel Structure (101): No || bridge exists
 Temp. Structure (103): Not Applicable (P)
 Maint. Resp. (21): 2 County Hwy Agency
 Owner (22): 2 County Hwy Agency
 Historic Signif. (37): 5 Not eligible for NRHP

Structure Type and Material

Curb/Sidewalk (50): Left: 1.5 ft Right: 5.5 ft
 Bridge Median (33): 0 No median
 Main Span Material (43A): 5 Prestressed Concrete
 Appr Span Material (44A): Not Applicable (P)
 Main Span Design (43B): 01 Slab
 Appr Span Design (44B): 00 Other (NBI)

Appraisal**Structure Appraisal**

Open/Posted/Closed (41): P Posted for load
 Deck Geometry (68): 5 Above Tolerable
 Underclearances (69): N Not applicable (NBI)
 Approach Alignment (72): 8-No Speed Red thru Curv
 Bridge Railings (36a): 0 Substandard
 Transitions (36b): 0 Substandard
 Approach Guardrail (36c): 0 Substandard
 Approach Guardrail Ends (36d): 0 Substandard
 Scour Critical (113): U Unknown Foundation

Minimum Vertical Clearance

Over Structure (53): 99.99 ft
 Under (reference) (54a): N Feature not hwy or RR
 Under (54b): 0 ft

Schedule**Current Inspection**

Inspection Date: 10/22/2020
 Inspector: KNLRELM - Loren Marquez
 Bridge Group: CA611
 Alt. Bridge Group:
 Primary Type: Interim
 Review Required: ☒

Geometrics

Spans in Main Unit (45): 3
 Approach Spans (46): 0
 Length of Max Span (48): 38.3 ft
 Structure Length (49): 100.33 ft
 Total Length: 140.33 ft
 Deck Area: 3536 sqft
 Structure Flared (35): 0 No flare

Age and Service

Year Built (27): 1967
 Year Reconstructed (106): 0
 Type of Service On (42a): 5 Highway-pedestrian
 Under (42b): 5 Waterway
 Fracture Critical Details: Not Applicable

Deck Type and Material

Deck Width (52): 35.25 ft
 Skew (34): 0 deg
 Deck Type (107): 2 Concrete Precast Panel
 Surface (108): 6 Bituminous
 Membrane: 0 None
 Deck Protection: None

Navigation Data

Navigation Control (38): Permit Not Required
 Nav Vertical Clr (39): 0 ft
 Nav Horizontal Clr (40): 0 ft
 Min Vert Lift Clr (116): 0 ft
 Pier Protection (111): 1 Not Required

NBI Condition Rating

Sufficiency Rating: 15.5
 Health Index: 85.67
 Structural Eval (67): 3 Intolerable - Correct
 Deficiency: Structurally Deficient

Minimum Lateral Underclearance

Reference (55a): N Feature not hwy or RR
 Right Side (55b): 0 ft
 Left Side (56): 0 ft

Next Inspection Date Scheduled

NBI: 04/06/2022
 Element: 04/06/2021
 Fracture Critical:
 Underwater: 04/06/2022
 Other/Special: 04/06/2021
 Inventory Photo Update Due: 04/06/2024

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 11/24/2020

Schedule Cont.

Inspection Types Performed

NBI ☐Element ☒Fracture Critical ☐Underwater ☐Other Special ☒

Inspection Intervals

Required (92)

Frequency (92)

Last Date (93)

Inspection Resources

Fracture Critical

☐

mos

Crew Hours: 4

Underwater

☒

24 mos

04/06/2020

Flagger Hours: 0

Other Special

☒

6 mos

10/22/2020

Helper Hours: 0

NBI

24 mos (91) 04/06/2020 (90)

Snooper Hours: 0

Special Crew Hours: 3

Special Equip Hours: 0

Bridge Related

General Bridge Information

Parallel Bridge Seq:

Channel Depth: 10.6 ft

Radio Frequency: -1

Phone Number:

Exception Date:

Exception Type: Unknown

Accepted By Maint: 01/01/1967

Warranty Expiration: 00/00/0000

Performance Rating: Poor

Bridge Rail 1: Conc parapet-alum-rail

Bridge Rail 2: Not applicable-No rail

Electrical Devices: No electric service

Culvert Type: Not applicable

Maintenance Yard: Not FDOT Maintained

FIHS ON / OFF: No Routes on FIHS

Previous Structure:

2nd Previous Structure:

Replacement Structure:

Permitted Utilities: Power

☐

Water

☒

Gas

☐

Fiber Optic

☐

Sewage

☒

Other

☐

Bridge Load Rating Information

Inventory Type (065): 3 LRFR Load & Res. Fact

Operating Type (063): 3 LRFR Load & Res. Fact

Original Design Load (031): HL 93

Date: 01/13/2020

Initials: JS

Load Rating Rev. Recom.: No

Load Rating Plans Status: Field Measurements

Inventory Rating (066): 7.6 tons

Operating Rating (064): 11.9 tons

FL120 Permit Rating: 16.2 tons

HS20/FL120 Max Span Rating: 16.2 tons

Dynamic Impact in Percent: 33 %

Governing Span Length: 38.3 ft

Minimum Span Length: 28.3 ft

Distribution Method: Others

Load Rating Notes:

LEGAL LOADS

SU2: 11.7 tons

SU3: 12.2 tons

SU4: 11.9 tons

C3: 18.2 tons

C4: 16.9 tons

C5: 17.6 tons

ST5: 18.4 tons

Posting (070): 2 20.0-29.9%below

Open/Posted/Closed (041): P Posted for load

FLOOR BEAM (FB)

FB Present: No

FB Span Length, Gov: 0.0 ft

FB Spacing, Gov: 0.0 ft

FB OPR Rating: 0.0 tons

FB SU4 OPR Rating: 0.0 tons

FB FL120 Rating: 0.0 tons

POSTING

Recom. SU Posting: 11 tons

Recom. C Posting: 16 tons

Recom. ST5 Posting: 18 tons

Actual SU Posting: 11 tons

Actual C Posting: 16 tons

Actual ST5 Posting: 18 tons

Actual Blanket Posting: 99 tons

Emergency Vehicle: 1 EV inapplicable

SEGMENTAL (SEG)

SEG Wing-Span: -1.0 ft

SEG Web-to-Web Span: -1.0 ft

SEG Transverse HL93 Operating: -1.00 RF

Bridge Scour and Storm Information

Pile Driving Record: No pile driving records

Foundation Type: Unknown

Mode of Flow: Tidal

Rating Scour Eval: Minimal Risk

Highest Scour Eval: Unknown

Scour Evaluation Method:

Scour Recommended I: Unknown

Scour Recommended II: Unknown

Scour Recommended III: Unknown

Scour Elevation: -1 ft

Action Elevation: -1 ft

Storm Frequency: -1

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 11/24/2020

Elements

Inspection Date: 10/22/2020 MIGV

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3122	88.29	5	0.14	409	11.57	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	5	45.45	6	54.55	0	.	11 (SF)
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	20	100	0	.	20 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	292	100	0	.	292 (SF)
0	1900 / 3	Distortion	0	.	0	.	90	100	0	.	90 (SF)
0	510 / 3	Wearing Surfaces	1629	61.85	0	.	1005	38.15	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	1005	100	0	.	1005 sq.ft

DECKS : Joints

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	301 / 3	Pourable Joint Seal	0	.	0	.	104	74.29	36	25.71	140 ft
0	2310 / 3	Leakage	0	.	0	.	104	100	0	.	104 ft
0	2330 / 3	Seal Damage	0	.	0	.	0	.	36	100	36 ft

MISCELLANEOUS : Channel

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8290 / 3	Channel	0	.	0	.	1	100	0	.	1 (EA)
0	9150 / 3	Bank Erosion	0	.	0	.	1	100	0	.	1 (EA)

MISCELLANEOUS : Other Elements

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	321 / 3	Re Conc Approach Slab	1410	100	0	.	0	.	0	.	1410 sq.ft
0	510 / 3	Wearing Surfaces	957	91.14	0	.	93	8.86	0	.	1050 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	93	100	0	.	93 sq.ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	205 / 3	Re Conc Column	0	.	0	.	4	100	0	.	4 each
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 each
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	3	100	0	.	3 each

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	215 / 3	Re Conc Abutment	65	92.86	0	.	5	7.14	0	.	70 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	0	.	5	100	0	.	5 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	234 / 3	Re Conc Pier Cap	49	72.06	12	17.65	7	10.29	0	.	68 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	12	63.16	7	36.84	0	.	19 ft

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 11/24/2020

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8393 / 3	Bulkhead Seawall Any Material	0	.	0	.	354	100	0	.	354 ft
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	314	100	0	.	314 ft
0	6000 / 3	Scour	0	.	0	.	40	100	0	.	40 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8394 / 3	R/Conc Abut Slope Protection	3968	73.81	0	.	1408	26.19	0	.	5376 (SF)
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	320	100	0	.	320 (SF)
0	4000 / 3	Settlement	0	.	0	.	1088	100	0	.	1088 (SF)

SUPERSTRUCTURE : Superstructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	333 / 3	Other Bridge Railing	167	83.5	33	16.5	0	.	0	.	200 ft
0	1000 / 3	Corrosion	0	.	30	100	0	.	0	.	30 ft
0	1020 / 3	Connection	0	.	3	100	0	.	0	.	3 ft

Total Number of Elements*: 10

*excluding defects/protective systems

Inspection Information**Inspection Date:** 10/22/2020**Type:** Interim**Inspector:** KNLRELM - Loren Marquez**Inspection Notes:** Sufficiency Rating Calculation Accepted by KNLREJP at 11/18/2020 2:56:35 PM

This Interim inspection (10/22/2020) was conducted to evaluate Element 8099 PS Conc Slab (Sonovoid), for the status of the entire structure refer to the last Regular NBI Inspection (04/06/2020).

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 10/22/2020 per Loren Marquez, P.E.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure.

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (10/22/2020).

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED

RT: Right

LT: Left

L: Long

W: Wide

H: High

D: Deep

in.: Inches

ft.: Feet

LF: Linear Feet

SF: Square Feet

NE: Northeast

NW: Northwest

SE: Southeast

SW: Southwest

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDRDATE PRINTED: 11/24/2020

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north. (Entrance on North end, boat ramp on South end).

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

Element 227/3 Re Conc Pile notes have been replaced by Element 205/3 Re Conc Column on 10/29/2019.

Element 8475/3 R/Conc Walls notes have been replaced by Element 8393/3 Bulkhead Seawall Any Material on 04/06/2020.

The NBI Rating for Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/06/2020).

The Substructure NBI Rating is coded 4 (Poor) due to the significant deterioration of Column 2-2. (04/06/2020).

The Channel NBI Rating was lowered from 7 to 6 due to areas of undermining on the channel below the North seawall. (04/06/2020).

TRAFFIC RESTRICTIONS:

Based on the current load rating analysis dated 1/13/2020, it is recommended that this bridge be posted for the SU, C and ST5 type vehicles as follows: SU = 11 tons, C = 16 tons, ST5 = 18 tons. The bridge is currently posted for SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 29 and 30.

REVIEWED BY:

Schedule Notes



BRIDGE INSPECTION REPORT

PREPARED FOR: FDOT District 6
 BRIDGE OWNER: MIAMI-DADE COUNTY
 INSPECTION TYPE: Interim
 CONTRACT No. CA611

Inspected by:
Marlin Engineering, Inc.

Bridge No. 874294

REPORT CONTAINS

Inspection Date: 04-26-21

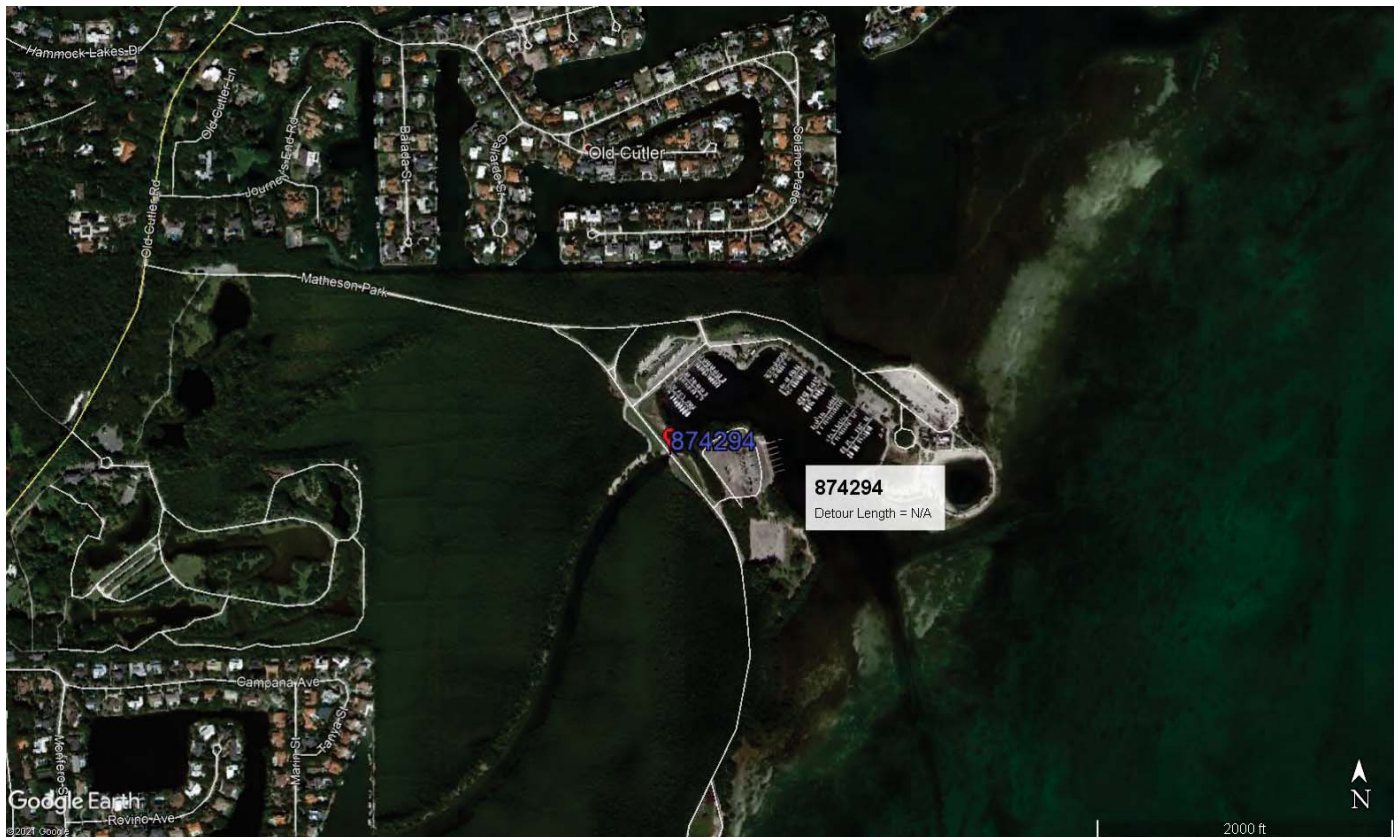
- | | | | |
|---|--|---|---|
| <input checked="" type="checkbox"/> BrM Inspection Report | <input type="checkbox"/> Bridge Profile | <input type="checkbox"/> Fracture Critical Data | <input type="checkbox"/> Addendum |
| <input checked="" type="checkbox"/> CIDR Information | <input type="checkbox"/> Underwater Inspection | <input checked="" type="checkbox"/> Load Rating Summary Sheet | <input type="checkbox"/> Mechanical and Electrical Data |



**Matheson Hmk Road over
 Matheson Hammock Canal**

Facility Carried & Location

Matheson Hammock Park



Location Map

Detour Length = N/A

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM****Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)****Structure ID: 874294****Inspection****DISTRICT: D6 - Miami****INSPECTION DATE: 4/26/2021 HIXS**

BY: Marlin Engineering, Inc.	STRUCTURE NAME: Not recorded
OWNER: 2 County Hwy Agency	YEAR BUILT: 1967
MAINTAINED BY: 2 County Hwy Agency	SECTION NO.: 87 000 757
STRUCTURE TYPE: 5 Prestressed Concrete - 01 Slab	MP: 0.080
LOCATION: Matheson Hammock Park	ROUTE: 00000
SERV. TYPE ON: 5 Highway-pedestrian	FACILITY CARRIED: Matheson Hmk Road
SERV. TYPE UNDER: 5 Waterway	FEATURE INTERSECTED: Matheson Hammock Canal

☐ FUNCTIONALLY OBSOLETE☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Interim

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 4/26/2021 UNDERWATER: 4/6/2020

SUFFICIENCY RATING:	15.5
HEALTH INDEX:	85.48

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

BY: Marlin Engineering, Inc.
 OWNER: 2 County Hwy Agency
 MAINTAINED BY: 2 County Hwy Agency
 STRUCTURE TYPE: 5 Prestressed Concrete - 01 Slab
 LOCATION: Matheson Hammock Park
 SERV. TYPE ON: 5 Highway-pedestrian
 SERV. TYPE UNDER: 5 Waterway

STRUCTURE NAME: Not recorded
 YEAR BUILT: 1967
 SECTION NO.: 87 000 757
 MP: 0.080
 ROUTE: 00000
 FACILITY CARRIED: Matheson Hmk Road
 FEATURE INTERSECTED: Matheson Hammock Canal

- ☐ THIS BRIDGE CONTAINS FRACTURE CRITICAL COMPONENTS
- ☐ THIS BRIDGE IS SCOUR CRITICAL
- ☒ THIS REPORT IDENTIFIES DEFICIENCIES WHICH REQUIRE PROMPT CORRECTIVE ACTION
- ☐ FUNCTIONALLY OBSOLETE ☒ STRUCTURALLY DEFICIENT

TYPE OF INSPECTION: Interim

DATE FIELD INSPECTION WAS PERFORMED: ABOVE WATER: 4/26/2021 UNDERWATER: 4/6/2020

OVERALL NBI RATINGS:

DECK: 3 Serious	CHANNEL: 6 Bank Slumping
SUPERSTRUCTURE: 3 Serious	CULVERT: N N/A (NBI)
SUBSTRUCTURE: 4 Poor	SUFF. RATING: 15.5
PERF. RATING: Poor	HEALTH INDEX: 85.48

FIELD PERSONNEL / TITLE / NUMBER:**INITIALS**

Guzman, Armando - Bridge Inspector (CBI#00407) (lead)

Monterail, Jonathan - Assistant Bridge Inspector

Rego, Alexis - Bridge Inspector (CBI#00409)

Campo, Luis - Bridge Inspector (CBI #00619)

Alfonso, Rene - Bridge Inspector Assistance

REVIEWING BRIDGE INSPECTION SUPERVISOR:

Rego, Alexis - Bridge Inspector (CBI#00409)

CONFIRMING REGISTERED PROFESSIONAL ENGINEER:

Vers, Julie - Structural Design Manager (P.E. # 77896) Marlin Engineering
 1700 NW 66 Avenue
 Suite 106
 Plantation Florida 33313

SIGNATURE: _____

DATE: _____

The official record of this package has been electronically signed and sealed by Julie A. Vers, P.E. on the date adjacent to the seal as required by Rule 61G15-23.004, F.A.C.. Printed copies of this document are not considered signed and sealed and the signature must be verified on any electronic copies.



This report contains information relating to the physical security of a structure and depictions of the structure. This information is confidential and exempt from public inspection pursuant to sections 119.071(3)(a) and 119.071(3)(b), Florida Statutes. Only the cover page of this report may be inspected and copied.

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

All Elements

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3099	87.64	14	0.4	423	11.96	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	14	70	6	30	0	.	20 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	35	100	0	.	35 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	292	100	0	.	292 (SF)
0	1900 / 3	Distortion	0	.	0	.	90	100	0	.	90 (SF)
0	510 / 3	Wearing Surfaces	1734	65.83	0	.	900	34.17	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	900	100	0	.	900 sq.ft

Element Inspection Notes:

8099/3 Notes: The top of the slab units is not visible due to an asphalt overlay. The width of the sonovoid slab units was field verified to be 3ft. wide.

SECONDARY:

_Centerline raised pavement markers are missing along the structure. Previously missing object markers were installed. Refer to Photo 01. NO CHANGE.

_Sidewalk concrete panels are loose and move under pedestrian load. (Total 300 SF). Refer to Photo 02. NO CHANGE.

_The underside of the slab unit joints and bent caps show evidence of water seepage. NO CHANGE. NCAR.

_There is one exposed piece of corroded scrap metal on Slab Unit 1-6 underside at 9ft. from Abutment 1. Previously documented under Defect 1090 as a spall with exposed rebar having minor section loss. Refer to Photo 03. NO CHANGE.

Refer to Defects 1080, 1100, 1110, and 1900 for additional deficiencies

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Replace missing object markers at the four corners of the bridge and provide missing RPMs throughout the bridge.

_Properly secure the sidewalk panels.

_Monitor slab unit 1-1 for possible independent movement on the slab unit.

_Clean and coat exposed prestressing and reinforce Slab Unit 2-8.

_Repair spalls, delaminations, and cracks along the underside of the slab units

_Clean and coat exposed rebar and repair spall along the underside of slab unit 1-6, 9ft. from Abutment 1.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was partially completed. Recommendation will be issued to provide missing RPMs.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

1080/3 CS-3:

_Slab Unit 1-9 exhibits a spall/delamination up to 36in. L x 24in. W x 2.5in. D over Abutment 1, with an exposed stirrup, no measurable section loss. (Total 6 SF). Refer to Photo 04. NO CHANGE.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

CS-2:

_Slab Unit 2-6, east edge exhibits a delamination 30in. L x 4in. W starting at Pier 2 cap. (Total 3 SF). NO CHANGE.

_Slab Unit 2-7, west edge exhibits a delamination up to 24in. L x 4in. W starting at Pier 2 cap. (Total 2 SF). NO CHANGE.

_Slab Unit 2-8 underside exhibits a delamination up to full width x 36in. L with associated cracks and rust staining, starting at Bent 2 cap. (Total 9 SF). Refer to Photo 05. NEW.

1100/3

CS-3:

_Slab Unit 2-8, midspan has a spall 15ft. L x 24in. W x up to 4in. D with 7 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (3 broken strands). Previously noted a spall 10ft. L x 24in. W x up to 4in. D with 5 exposed strands, 2 broken threads, and 6 exposed transverse rebars. (Total 20 SF). Refer to Photo 06. INCREASE.

_Slab Unit 2-9, midspan has a spall/delamination up to 15ft. L x 12in. W x 2in. D with 2 prestressing strands and 7 transverse rebars having up to 90% section remaining. (Total 15 SF). Refer to Photo 06. NEW.

1110/3

CS-3:

_Slab Unit 1-6 east edge has two delamination areas, one up to 5ft. L x 6in. W starting at Abutment 1 and the other starting at Pier Cap 2 up to 9ft. L x 12in. W with associated cracks up to 1/16in. W with efflorescence throughout. (Total 14 SF). NO CHANGE.

_Slab Unit 1-7 east edge has a spall/delamination 24in. L x 12in. W with associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out over Abutment 1. (Total 2 SF). NO CHANGE.

_Slab Unit 1-7, east edge has a delamination 7ft. L x 4in. W, with an associated crack of up to 1/16in. starting at Pier 2 cap. (Total 7 SF). NO CHANGE.

_Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W starting at Abutment 1 with associated cracks up to 1/4in. W with efflorescence and corrosion bleed-out and associated spalling up to 4ft. L x 6in. W x 2in. D approximately 10ft from Abutment 1. (Total 19 SF). Refer to Photo 07. NO CHANGE.

_Slab Unit 1-8 east edge has a delamination 4ft. L x 15in. W and associated cracks up to 1/32in. W with efflorescence and corrosion bleed-out, 9ft. from Pier Cap 2. (Total 5 SF). NO CHANGE.

_Slab Unit 1-8 has a delaminated area up to 8ft. L x 3ft. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out starting at Pier Cap 2. (Total 24 SF). NO CHANGE.

_Slab Unit 1-9 west edge has a delaminated area 9ft. L x 10in. W and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out, starting near the 3/4 point and extending to Pier 2 cap. (Total 9 SF). NO CHANGE.

_Slab Unit 2-7 east edge is intermittently cracked/delaminated up to span length x 16in. W (average width) with up to 1/4in. W cracks. (Total 38 SF). NO CHANGE.

_Slab Unit 2-8 west half has two delaminated areas up to 15ft. L x 18in. W (average width) at south and north ends, with associated cracks of up to 1/4in. W. (Total 60 SF). NO CHANGE.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

_Slab Unit 2-9 west edge has a delaminated area up to 5ft. L x 5in. W with associated cracking up to 1/4in. wide, starting at the Pier 2 cap. (Total 5 SF). NO CHANGE.

_Slab Unit 3-6 has a delamination up to 24in. L x 6in. W on the east edge over Pier 3, with an associated crack of up to 1/16in. W. (Total 2 SF). NO CHANGE.

_Slab Unit 3-6 east edge has a delaminated area up to 42in. L x 8in. W with associated cracks up to 1/16in. W. (Total 4 SF). NO CHANGE.

_Slabs Unit 3-7 has two delaminated areas, one starting at Pier 3 up to 8ft. L x 15in. W (average width) with associated cracks, and the second, near mid-span up to 3ft. L x 30in. W. (Total 25 SF). NO CHANGE.

_Slab Unit 3-7 has an unsound repaired area 12ft. L x up to slab width (3ft.) starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out. (Total 30 SF). Refer to Photo 08. NO CHANGE.

_Slab Unit 3-8 has a spall/delamination up to 8ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3. (Total 24 SF). Refer to Photo 09. NO CHANGE.

_Slab Unit 3-8 has an unsound repair/delamination up to 42in. L x 30in. W with associated cracks up to 1/16in. W with efflorescence starting at Abutment 4. (Total 9 SF). NO CHANGE.

_Slab Unit 3-8 has an unsound repair/delamination up to 74in. L x up to slab width (3ft.) with associated cracks up to 1/16in. W with efflorescence starting 5.5ft. from Abutment 4. (Total 15 SF). NO CHANGE.

1900/3

CS-3:

_Slab Unit 1-1 exhibits a slight outward rotation at Abutment 1 with up to 1/4in. height difference in reference to the top of the cap, potentially indicating shear key failure. (Total 90 SF). Refer to Photo 10. NO CHANGE. NCAR.

510/3

For deficiencies refer to Defect 3220.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

_Clean and seal cracks and rutting along the expansion joints.

_Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.

_Monitor cracks along slab unit joints for independent movement of the slab units.

CORRECTIVE ACTION EVALUATION:

_The corrective action noted above was completed.

_The corrective action noted above was not completed. Recommendation will be repeated.

_The corrective action noted above was not completed. Recommendation will be repeated.

3220/3

CS-3:

_The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated 1in. W rutting over the slab unit joints and upheaving up to 1in. H at the shoulders, possibly indicating independent slab unit movement. (Total 600 SF). Refer to Photo 11. NO CHANGE.

_The asphalt overlay at Spans 1 and 2 has multi-directional cracking up to 1/2in. W on Lane 2 (NB), worse condition is on Span 1 which has a hollow-sounding area 19.5ft L x 11ft. W, starting 1 ft. from the right sidewalk. (Total 300 SF). Refer to Photo 12. NO CHANGE.

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

Inspection/CIDR Report with PDF attachment(s) (INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	205 / 3	Re Conc Column	0	.	0	.	4	100	0	.	4 each
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 each
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	3	100	0	.	3 each

Element Inspection Notes:

205/3 Note: At high tide, the seawater reaches the lower section of the columns.

Refer to Defects 1090 and 1130 for deficiencies.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

- _Remove any loose concrete and repair delaminations and spalls along the Column 2-2.
- _Repair delaminations and seal cracks along Bents 2 and 3 columns.
- _Install cathodic protection to Bents 2 and 3 columns.

CORRECTIVE ACTION EVALUATION:

- _The corrective action noted above was not completed. Recommendation will be repeated.
- _The corrective action noted above was not completed. Recommendation will be repeated.
- _The corrective action noted above was not completed. Recommendation will be repeated.

1090/3

CS-3:

_Column 2-2, south face has a spall/delamination up to 55in. H x 32in. W x 4in. D with two exposed longitudinal rebars and five stirrups, having areas of up to 80% section remaining. Additionally, there are areas of delamination around the column circumference covering the entire column height with associated cracks up to 1/4in. W as a consequence of corrosion of the steel reinforcement. Previously noted as a spall/delamination 7ft. H x 3ft. W x 3in. D with one exposed rebar and one stirrup. (Total 1 ea.) Refer to Photos 13, 14, and 15. INCREASE.

1130/3

CS-3:

_Columns 2-1, 3-1, and 3-2 have delaminated areas along their entire length with associated cracks up to full height x 1/16in. W, as a result of corrosion of the steel reinforcement. (Total 3 ea.) NO CHANGE.

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	234 / 3	Re Conc Pier Cap	48	70.59	12	17.65	8	11.76	0	.	68 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	12	60	8	40	0	.	20 ft

Element Inspection Notes:

234/3 Refer to Defect 1080 for additional deficiencies.

PREVIOUS RECOMMENDED CORRECTIVE ACTION:

- _Remove vegetation growing on west end of Bents 2 and 3 caps.
- _Repair spalls and delaminations along Bents 2 and 3 caps.

CORRECTIVE ACTION EVALUATION:

- _The corrective action noted above was completed.
- _The corrective action noted above was not completed. Recommendation will be repeated.

1080/3

CS-3:

_Bent 2 cap, south face has a spall/delamination up to 48in. L x 17in. H x 3/4 in. D over Column 2-2, and on the same location, north face a delamination 20in. L x 12in. H. Previously noted in the south face as a spall/delamination up to 3ft. L x 16in. H x 1 in.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM****Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)****Structure ID: 874294****Inspection****DISTRICT: D6 - Miami****INSPECTION DATE: 4/26/2021 HIXS**

D. (Total 4 LF) Refer to Photos 16 and 17. INCREASE.

_Bent 3 cap, bottom and north faces has two unsound repaired areas up to 30in. L x 24in. W with multidirectional cracks up to 1/64in. W between Columns 3-1 and 3-2. (Total 4 LF) Refer to Photo 18. NO CHANGE.

CS-2:

_Pier 3 cap has intermittent delaminated areas up to 3ft. L x 16in. H between Columns 3-1 and 3-2, along the top and bottom north edges. (Total 12 LF) Refer to Photo 18. NO CHANGE.

Total Number of Elements*: 3

*excluding defects/protective systems

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

Inspector Recommendations

UNIT: 0	DECKS		
ELEMENT/ENV:	8099 / 3 PS Conc Slab (Sonovoid)	ELEM CATEGORY:	Decks/Slabs
CONDITION STATE			PRIORITY
1 , 2 , 3	MMS Quantity: 300 sf Element Estimated Quantity: 300 (SF)		3
WORK ORDER RECOMMENDATION:			
Properly secure the sidewalk concrete panels. Photo 02			
1 , 2 , 3	MMS Quantity: 10 sf Element Estimated Quantity: 10 (SF)		3
WORK ORDER RECOMMENDATION:			
Replace missing raised pavement markers along the centerline of the structure. Photo 01			
ELEMENT/ENV:	8099:510:3220 / 3 Crack (Wearing Surface)	ELEM CATEGORY:	Decks/Slabs
CONDITION STATE			PRIORITY
3	MMS Quantity: 600 sf Element Estimated Quantity: 600 sq.ft		3
WORK ORDER RECOMMENDATION:			
Monitor the slab units for independent movement. Photo 11			
3	MMS Quantity: 900 sf Element Estimated Quantity: 900 sq.ft		3
WORK ORDER RECOMMENDATION:			
Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2. Photos 11 and 12			
ELEMENT/ENV:	8099:1080 / 3 Delamination/Spall/Patched Area	ELEM CATEGORY:	Decks/Slabs
CONDITION STATE			PRIORITY
2 , 3	MMS Quantity: 298 sf Element Estimated Quantity: 298 (SF)		3
WORK ORDER RECOMMENDATION:			
Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs. Photos 03 to 05 and 07 to 09			
ELEMENT/ENV:	8099:1100 / 3 Exposed Prestressing	ELEM CATEGORY:	Decks/Slabs
CONDITION STATE			PRIORITY
3	MMS Quantity: 35 sf Element Estimated Quantity: 35 (SF)		2
WORK ORDER RECOMMENDATION:			
Clean and coat exposed prestressing strands and rebars, repair spalls and reinforce the Slab units 2-8 and 2-9. Photo 06			

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

Inspector Recommendations

UNIT: 0 SUBSTRUCTURE
ELEMENT/ENV: 205:1090 / 3 Exposed Rebar ELEM CATEGORY: Substructure

CONDITION STATE			PRIORITY
3	MMS Quantity: 40 mh	Element Estimated Quantity: 1 each	2
WORK ORDER RECOMMENDATION: Clean and coat exposed rebars, repair spalls/delaminations and reinforce Column 2-2. Photos 13 to 15			

ELEMENT/ENV: 205:1130 / 3 Cracking (RC and Other) ELEM CATEGORY: Substructure

CONDITION STATE			PRIORITY
3	MMS Quantity: 40 mh	Element Estimated Quantity: 4 each	3
WORK ORDER RECOMMENDATION: Repair delaminations and seal cracks along Bents 2 and 3 columns. Photos 13 to 15			
3	MMS Quantity: 80 mh	Element Estimated Quantity: 4 each	3
WORK ORDER RECOMMENDATION: Install jackets with cathodic protection to Bents 2 and 3 columns. Photos 13 to 15			

ELEMENT/ENV: 234:1080 / 3 Delamination/Spall/Patched Area ELEM CATEGORY: Substructure

CONDITION STATE			PRIORITY
2 , 3	MMS Quantity: 40 mh	Element Estimated Quantity: 20 ft	2
WORK ORDER RECOMMENDATION: Repair spalls and delaminations along Bents 2 and 3 caps. Photos 16 to 18			

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north. (Entrance on North end, boat ramp on South end).

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

TRAFFIC RESTRICTIONS:

Based on the current load rating analysis dated 1/13/2020, the bridge is posted for the SU, C and ST5 type vehicles as follows:
 SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 19 and 20.

REVIEWED BY:

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

**Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS

INSPECTION NOTES: **HIXS** **4/26/2021**

Sufficiency Rating Calculation Accepted by knmeira at 5/5/2021 3:15 PM.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure. (04/26/2021).

This Interim inspection (04/26/2021) was conducted to evaluate Element 8099 PS Conc Slab (Sonovoid), Element 234 Re Conc Pier Cap and Element 205 Re Conc Column, for the status of the entire structure refer to the last Regular NBI Inspection (04/06/2020).

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/26/2021).

The Substructure NBI Rating is coded 4 (Poor) due to extensive spalls with exposed rebars along Column 2-2, and delaminations and cracks along the columns and pier caps throughout the structure. (04/26/2021).

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 04/26/2021 per Julie A. Vers, P.E.

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED

RT: Right

LT: Left

L: Long

W: Wide

H: High

D: Deep

in.: Inches

ft.: Feet

LF: Linear Feet

SF: Square Feet

NE: Northeast

NW: Northwest

SE: Southeast

SW: Southwest

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 01 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Centerline raised pavement markers are missing along the structure. Previously missing object markers were installed.

WORK ORDER RECOMMENDATION:

Replace missing raised pavement markers along the centerline of the structure.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 02 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Sidewalk concrete panels are loose and move under pedestrian load.

WORK ORDER RECOMMENDATION:

Properly secure the sidewalk concrete panels.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 03 Element/Env 8099/3: PS Conc Slab (Sonovoid)

There is one exposed piece of corroded scrap metal on Slab Unit 1-6 underside at 9ft. from Abutment 1.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 04 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-9 exhibits a spall/delamination up to 36in. L x 24in. W x 2.5in. D over Abutment 1, with an exposed stirrup, no measurable section loss.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 05 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 2-8 underside exhibits a delamination up to full width x 36in. L with associated cracks and rust staining, starting at Bent 2 cap.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 06 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 2-8, midspan has a spall 15ft. L x 24in. W x up to 4in. D with 7 exposed and corroded transverse rebars with up to 60% section remaining and 5 exposed and corroded prestressing strands with up to 0% section remaining (3 broken strands).

Slab Unit 2-9, midspan has a spall/delamination up to 15ft. L x 12in. W x 2in. D with 2 prestressing strands and 7 transverse rebars having up to 90% section remaining.

WORK ORDER RECOMMENDATION:

Clean and coat exposed prestressing strands and rebars, repair spalls and reinforce the Slab units 2-8 and 2-9.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 07 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-8 west edge is intermittently delaminated up to 15ft. L x 15in. W starting at Abutment 1 with associated cracks up to 1/4in. W with efflorescence and corrosion bleed-out and associated spalling up to 4ft. L x 6in. W x 2in. D approximately 10ft from Abutment 1.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 08 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 3-7 has an unsound repaired area 12ft. L x up to slab width (3ft.) starting from Abutment 4 with hollow sounding throughout and associated cracks up to 1/16in. W with efflorescence and corrosion bleed-out.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 09 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 3-8 has a spall/delamination up to 8ft. L x 3ft. W x 1in. D and associated cracks with corrosion bleed-out starting at Pier 3.

WORK ORDER RECOMMENDATION:

Clean and coat exposed steel and repair spalls and delaminations along the underside of sonovoid slabs.

FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 10 Element/Env 8099/3: PS Conc Slab (Sonovoid)

Slab Unit 1-1 exhibits a slight outward rotation at Abutment 1 with up to 1/4in. height difference in reference to the top of the cap, potentially indicating shear key failure. No anti-rotation block is in place.

WORK ORDER RECOMMENDATION:
None.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 11 Element/Env 8099/ 510/3: PS Conc Slab (Sonovoid)/ Wearing Surfaces

The asphalt overlay has longitudinal cracks up to span length x 1/4in. W with associated 1in. W rutting over the slab unit joints and upheaving up to 1in. H at the shoulders, possibly indicating independent slab unit movement.

WORK ORDER RECOMMENDATION:

- _ Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.
- _ Monitor the slab units for independent movement.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 12 Element/Env 8099/ 510/3: PS Conc Slab (Sonovoid)/ Wearing Surfaces

The asphalt overlay at Spans 1 and 2 has multi-directional cracking up to 1/2in. W on Lane 2 (NB), worse condition is on Span 1 which has a hollow-sounding area 19.5ft L x 11ft. W, starting 1 ft. from the right sidewalk.

WORK ORDER RECOMMENDATION:

Seal cracks on the asphalt along the slab unit joints and multi-directional cracks on Lane 2 (NB) in Spans 1 and 2.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 13 Element/Env 205/3: Re Conc Column

Column 2-2, south face has a spall/delamination up to 55in. H x 32in. W x 4-3/4in. D with two exposed longitudinal rebars and five stirrups, having areas of up to 80% section remaining.

WORK ORDER RECOMMENDATION:

- _ Clean and coat exposed rebars, repair spalls/delaminations and reinforce Column 2-2.
- _ Repair delaminations and seal cracks along Bents 2 and 3 columns.
- _ Install jackets with cathodic protection to Bents 2 and 3 columns.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 14 Element/Env 205/3: Re Conc Column

Spall/delamination with exposed reinforcement having up to 80% remaining in south face of Column 2-2. (close up view)

WORK ORDER RECOMMENDATION:

- _Clean and coat exposed rebars, repair spalls/delaminations and reinforce Column 2-2.
- _Repair delaminations and seal cracks along Bents 2 and 3 columns.
- _Install jackets with cathodic protection to Bents 2 and 3 columns.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 15 Element/Env 205/3: Re Conc Column

Areas of delamination around the column circumference covering the entire column height with associated cracks up to 1/4in. W as a consequence of corrosion of the steel reinforcement.

WORK ORDER RECOMMENDATION:

- _ Clean and coat exposed rebars, repair spalls/delaminations and reinforce Column 2-2.
- _ Repair delaminations and seal cracks along Bents 2 and 3 columns.
- _ Install jackets with cathodic protection to Bents 2 and 3 columns.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 16 Element/Env 234/3: Re. Concrete Pier Cap

Bent 2 cap, south face has a spall/delamination up to 48in. L x 17in. H x 3/4 in. D over Column 2-2, and on the same location, north face a delamination 20in. L x 12in. H. (south view)

WORK ORDER RECOMMENDATION:

Repair spalls and delaminations along Bents 2 and 3 caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 17 Element/Env 234/3: Re. Concrete Pier Cap

Bent 2 cap, south face has a spall/delamination up to 48in. L x 17in. H x 3/4 in. D over Column 2-2, and on the same location, north face a delamination 20in. L x 12in. H. (bottom view)

WORK ORDER RECOMMENDATION:

Repair spalls and delaminations along Bents 2 and 3 caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 18 Element/Env 234/3: Re. Concrete Pier Cap

Areas of unsound repairs on the bottom face of Pier 3 cap, intermittent delaminated areas up to 3ft. L x 16in. H between Columns 3-1 and 3-2, along the top and bottom north edges.

WORK ORDER RECOMMENDATION:

Repair spalls and delaminations along Bents 2 and 3 caps.

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 19: STRUCTURE NOTES

North Approach Posting Sign

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM
Inspection/CIDR Report with PDF attachment(s)
(INTERIM INSPECTION REPORT)**

Structure ID: 874294

Inspection

DISTRICT: D6 - Miami

INSPECTION DATE: 4/26/2021 HIXS



Photo 20: STRUCTURE NOTES

South Approach Posting Sign

Bridge No.	874294	Analysis Method:	LRFR-LRFD	FDOT Bridge Load Rating Summary Form (Page 1 of 1)
Location	Matheson hammock Road over matheson Hammock Canal			
Description	3 Spans, 2-30'&1-40', Prestressed voided slab beams 36"x17"			

Rating Type	Rating Type	Gross Axle Weight (tons)	Moment/Shear/Service		Dead Load Factor	Live Load Factor	Live Load Distrib. Factor (axles)	Rating Factor	Span No. - Girder No., Interior/Exterior, %Span Length	RF-Weight (tons)
Level	Vehicle	Weight	Member Type	Limit	DC	LL	LLDF	RF	Governing Location	RATING
Inventory	HL93	36	Prestressed	Service	1.00	0.80	0.600	0.210	Central span, midspan	7.6
Operating	HL93	36	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.330	Central span, midspan	11.9
Permit	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Permit Max Span	FL120	60	Prestressed	Strength, Shear	1.25/0.90	1.35	0.500	0.270	Central span, 1/4 point	16.2
Legal	SU2	17	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.690	Central span, midspan	11.7
	SU3	33	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.370	Central span, midspan	12.2
	SU4	35	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.340	Central span, midspan	11.9
	C3	28	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.650	Central span, midspan	18.2
	C4	36.7	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	16.9
	C5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.440	Central span, midspan	17.6
	ST5	40	Prestressed	Strength, Moment	1.25/0.90	1.35	0.600	0.460	Central span, midspan	18.4
Emergency Vehicle (EV)	EV2	28.75	Prestressed	NA	NA	NA	0.600			-1
	EV3	43	Prestressed	NA	NA	NA	0.600			-1

Original Design Load	HS20 or HS20-S16-44	Performed by:	Mengyuan Chen	Date:	01/13/20
Rating Type, Analysis	LRFR-LRFD	Checked by:	Juan A. Sobrino	Date:	01/13/20
Distribution Method	Others	Sealed By:	Juan A. Sobrino	Date:	01/13/20
Impact Factor	33.0% (axle loading)	FL P.E. No.:	73121		
FL120 Gov. Span Length	38.3 (feet)	Cert. Auth. No.:	27244		
Minimum Span Length	28.3 (feet)	Phone & email:	(+1) 305 648 00 10, miami@pedelta.om		
Recommended Posting	> 39.9% below (0.000-0.600) (Required)	Company:	Pedelta Inc.		
Recommended SU Posting*	11 (tons)	Address:	2000 Ponce de Leon Blvd., Suite 624, Coral Gables, Florida 33134, USA		
Recommended C Posting	16 (tons)	<p>Juan Sobrino</p> <p>Digitally signed by Juan Sobrino Date: 2020.01.13 15:58:25 -05'00'</p> <p>Juan A. Sobrino, State of Florida, Professional Engineer, License No 73121. This document has been electronically signed and sealed by Juan A. Sobrino on January 13th, 2020 using a SHA authentication code. Printed copies of this document are not considered signed and sealed and the SHA authentication code must be verified on any electronic copies.</p>			
Recommended ST5 Posting	18 (tons)				
Owner	02 County Highway Agency				
Location	Neither Interstate traffic nor within 1 mile reasonable access to an Interstate				
EV Posting	No. EV posting is not recommended. The FAST Act does not apply				
Floor Beam Present?	No				
Segmental Bridge?	No				
Project No. & Reason	432907-1-72-02 Deterioration				
Plans Status	Built				

This 10-11-2019 summary follows the FDOT Bridge Load Rating Manual (BLRM), and the FDOT BMS Coding Guide.

*Recommended SU Posting levels for Florida SU trucks adequately restricts AASHTO SU trucks; see BLRM Chapter 7.

fdot.gov/maintenance/LoadRating.shtm

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 6/25/2021

Description

Structure Unit Identification

Bridge/Unit Key: 874294 0
 Structure Name:
 Description: SPANS 1 THRU 3
 Type: M - Main

Roadway Identification

NBI Structure No (8): 874294
 Position/Prefix (5): 1 - Route On Structure
 Kind Hwy (Rte Prefix): 4 County Hwy
 Design Level of Service: 8 Service Road
 Route Number/Suffix: 00000 / 0 N/A (NBI)
 Feature Intersect (6): Matheson Hammock Canal
 Critical Facility: Not Defense-crit
 Facility Carried (7): Matheson Hmk Road
 Mile Point (11): 0.08
 Latitude (16): 025d40'44.2" Long (17): 080d15'43.8"

Roadway Traffic and Accidents

Lanes (28): 2 Medians: 0 Speed: 15 mph
 ADT Class: 2 ADT Class 2
 Recent ADT (29): 736 Year (30): 2020
 Future ADT (114): 1168 Year (115): 2042
 Truck % ADT (109): 1
 Detour Length (19): 99 mi
 Detour Speed:
 Accident Count: -1 Rate:

Roadway Classification

Nat. Hwy Sys (104): 0 Not on NHS
 National base Net (12): 0 - Not on Base Network
 LRS Inventory Rte (13a): 87 000 757 Sub Rte (13b): 00
 Functional Class (26): 09 Rural Local
 Federal Aid System: OFF
 Defense Hwy (100): 0 Not a STRAHNET hwy
 Direction of Traffic (102): 2 2-way traffic
 Emergency: ☒

Roadway Clearances

Vertical (10): 99.99 ft Appr. Road (32): 26.25 ft
 Horiz. (47): 26.25 ft Roadway (51): 26.25 ft
 Truck Network (110): 0 Not part of natl netwo
 Toll Facility (20): 3 On free road
 Fed. Lands Hwy (105): 0 N/A (NBI)
 School Bus Route: ☐
 Transit Route: ☐

NBI Project Data

Proposed Work (075A): Not Applicable (P)
 Work To Be Done By (075B): Not Applicable (P)
 Improvement Length (076): 0 ft

Improvement Cost (094): \$ 0.00
 Roadway Improvement Cost (095): \$ 0.00
 Total Cost (096): \$ 0.00
 Year of Estimate (097):

NBI Rating

Channel (61): 6 Bank Slumping
 Deck (58): 3 Serious
 Superstructure (59): 3 Serious
 Substructure (60): 4 Poor

Culvert (62): N N/A (NBI)
 Waterway (71): 8 Equal Desirable
 Unrepaired Spalls: -1 sq.ft.
 Review Required: ☒

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 6/25/2021

Structure Identification

Admin Area: Miami-Dade
 District (2): D6 - Miami
 County (3): (87)Miami-Dade
 Place Code (4): South Miami Heights
 Location (9): Matheson Hammock Park
 Border Br St/Reg (98): Not Applicable (P) Share: 0 %
 Border Struct No (99):
 FIPS State/Region (1): 12 Florida Region 4-Atlanta
 NBIS Bridge Len (112): Y - Meets NBI Length
 Parallel Structure (101): No || bridge exists
 Temp. Structure (103): Not Applicable (P)
 Maint. Resp. (21): 2 County Hwy Agency
 Owner (22): 2 County Hwy Agency
 Historic Signif. (37): 5 Not eligible for NRHP

Structure Type and Material

Curb/Sidewalk (50): Left: 1.5 ft Right: 5.5 ft
 Bridge Median (33): 0 No median
 Main Span Material (43A): 5 Prestressed Concrete
 Appr Span Material (44A): Not Applicable (P)
 Main Span Design (43B): 01 Slab
 Appr Span Design (44B): 00 Other (NBI)

Appraisal**Structure Appraisal**

Open/Posted/Closed (41): P Posted for load
 Deck Geometry (68): 5 Above Tolerable
 Underclearances (69): N Not applicable (NBI)
 Approach Alignment (72): 8-No Speed Red thru Curv
 Bridge Railings (36a): 0 Substandard
 Transitions (36b): 0 Substandard
 Approach Guardrail (36c): 0 Substandard
 Approach Guardrail Ends (36d): 0 Substandard
 Scour Critical (113): U Unknown Foundation

Minimum Vertical Clearance

Over Structure (53): 99.99 ft
 Under (reference) (54a): N Feature not hwy or RR
 Under (54b): 0 ft

Schedule**Current Inspection**

Inspection Date: 04/26/2021
 Inspector: KNMEIAG - Armando Guzman
 Bridge Group: CA611
 Alt. Bridge Group:
 Primary Type: Interim
 Review Required: ☒

Geometrics

Spans in Main Unit (45): 3
 Approach Spans (46): 0
 Length of Max Span (48): 38.3 ft
 Structure Length (49): 100.33 ft
 Total Length: 140.33 ft
 Deck Area: 3536 sqft
 Structure Flared (35): 0 No flare

Age and Service

Year Built (27): 1967
 Year Reconstructed (106): 0
 Type of Service On (42a): 5 Highway-pedestrian
 Under (42b): 5 Waterway
 Fracture Critical Details: Not Applicable

Deck Type and Material

Deck Width (52): 35.25 ft
 Skew (34): 0 deg
 Deck Type (107): 2 Concrete Precast Panel
 Surface (108): 6 Bituminous
 Membrane: 0 None
 Deck Protection: None

Navigation Data

Navigation Control (38): Permit Not Required
 Nav Vertical Clr (39): 0 ft
 Nav Horizontal Clr (40): 0 ft
 Min Vert Lift Clr (116): 0 ft
 Pier Protection (111): 1 Not Required

NBI Condition Rating

Sufficiency Rating: 15.5
 Health Index: 85.48
 Structural Eval (67): 3 Intolerable - Correct
 Deficiency: Structurally Deficient

Minimum Lateral Underclearance

Reference (55a): N Feature not hwy or RR
 Right Side (55b): 0 ft
 Left Side (56): 0 ft

Next Inspection Date Scheduled

NBI: 04/26/2022
 Element: 10/26/2021
 Fracture Critical:
 Underwater: 04/26/2022
 Other/Special: 10/26/2021
 Inventory Photo Update Due: 04/26/2024

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 6/25/2021

Schedule Cont.

Inspection Types Performed

NBI ☐Element ☒Fracture Critical ☐Underwater ☐Other Special ☒

Inspection Intervals Required (92) Frequency (92) Last Date (93) Inspection Resources

Fracture Critical	<input type="checkbox"/>	mos		Crew Hours: 2
Underwater	<input checked="" type="checkbox"/>	24 mos	04/06/2020	Flagger Hours: 0
Other Special	<input checked="" type="checkbox"/>	6 mos	04/26/2021	Helper Hours: 0
NBI		24 mos (91)	04/06/2020 (90)	Snooper Hours: 0
				Special Crew Hours: 3
				Special Equip Hours: 0

Bridge Related

General Bridge Information

Parallel Bridge Seq:	Bridge Rail 1: Conc parapet-alum-rail
Channel Depth: 10.6 ft	Bridge Rail 2: Not applicable-No rail
Radio Frequency: -1	Electrical Devices: No electric service
Phone Number:	Culvert Type: Not applicable
Exception Date:	Maintenance Yard: Not FDOT Maintained
Exception Type: Unknown	FIHS ON / OFF: No Routes on FIHS
Accepted By Maint: 01/01/1967	Previous Structure:
Warranty Expiration: 00/00/0000	2nd Previous Structure:
Performance Rating: Poor	Replacement Structure:
Permitted Utilities: Power <input type="checkbox"/> Water <input checked="" type="checkbox"/> Gas <input type="checkbox"/> Fiber Optic <input type="checkbox"/> Sewage <input checked="" type="checkbox"/> Other <input type="checkbox"/>	

Bridge Load Rating Information

Inventory Type (065): 3 LRFR Load & Res. Fact	Inventory Rating (066): 7.6 tons
Operating Type (063): 3 LRFR Load & Res. Fact	Operating Rating (064): 11.9 tons
Original Design Load (031): HL 93	FL120 Permit Rating: 16.2 tons
Date: 01/13/2020	HS20/FL120 Max Span Rating: 16.2 tons
Initials: JS	Dynamic Impact in Percent: 33 %
Load Rating Rev. Recom.: No	Governing Span Length: 38.3 ft
Load Rating Plans Status: Field Measurements	Minimum Span Length: 28.3 ft
	Distribution Method: Others

Load Rating Notes:

LEGAL LOADS

SU2: 11.7 tons
 SU3: 12.2 tons
 SU4: 11.9 tons
 C3: 18.2 tons
 C4: 16.9 tons
 C5: 17.6 tons
 ST5: 18.4 tons
 Posting (070): 2 20.0-29.9%below
 Open/Posted/Closed (041): P Posted for load

FLOOR BEAM (FB)

FB Present: No

FB Span Length, Gov: 0.0 ft
 FB Spacing, Gov: 0.0 ft
 FB OPR Rating: 0.0 tons
 FB SU4 OPR Rating: 0.0 tons
 FB FL120 Rating: 0.0 tons

Bridge Scour and Storm Information

Pile Driving Record: No pile driving records
 Foundation Type: Unknown
 Mode of Flow: Tidal
 Rating Scour Eval: Minimal Risk
 Highest Scour Eval: Unknown
 Scour Evaluation Method:

POSTING

Recom. SU Posting: 11 tons
 Recom. C Posting: 16 tons
 Recom. ST5 Posting: 18 tons
 Actual SU Posting: 11 tons
 Actual C Posting: 16 tons
 Actual ST5 Posting: 18 tons
 Actual Blanket Posting: 99 tons
 Emergency Vehicle: 1 EV inapplicable

SEGMENTAL (SEG)

SEG Wing-Span: -1.0 ft
 SEG Web-to-Web Span: -1.0 ft
 SEG Transverse HL93 Operating: -1.00 RF

Scour Recommended I: Unknown
 Scour Recommended II: Unknown
 Scour Recommended III: Unknown
 Scour Elevation: -1 ft
 Action Elevation: -1 ft
 Storm Frequency: -1

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 6/25/2021

Elements

Inspection Date: 04/26/2021 HIXS

DECKS : Decks/Slabs

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8099 / 3	PS Conc Slab (Sonovoid)	3099	87.64	14	0.4	423	11.96	0	.	3536 (SF)
0	1080 / 3	Delamination/Spall/Patched Area	0	.	14	70	6	30	0	.	20 (SF)
0	1100 / 3	Exposed Prestressing	0	.	0	.	35	100	0	.	35 (SF)
0	1110 / 3	Cracking (PSC)	0	.	0	.	292	100	0	.	292 (SF)
0	1900 / 3	Distortion	0	.	0	.	90	100	0	.	90 (SF)
0	510 / 3	Wearing Surfaces	1734	65.83	0	.	900	34.17	0	.	2634 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	900	100	0	.	900 sq.ft

DECKS : Joints

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	301 / 3	Pourable Joint Seal	0	.	0	.	104	74.29	36	25.71	140 ft
0	2310 / 3	Leakage	0	.	0	.	104	100	0	.	104 ft
0	2330 / 3	Seal Damage	0	.	0	.	0	.	36	100	36 ft

MISCELLANEOUS : Channel

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8290 / 3	Channel	0	.	0	.	1	100	0	.	1 (EA)
0	9150 / 3	Bank Erosion	0	.	0	.	1	100	0	.	1 (EA)

MISCELLANEOUS : Other Elements

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	321 / 3	Re Conc Approach Slab	1410	100	0	.	0	.	0	.	1410 sq.ft
0	510 / 3	Wearing Surfaces	957	91.14	0	.	93	8.86	0	.	1050 sq.ft
0	3220 / 3	Crack (Wearing Surface)	0	.	0	.	93	100	0	.	93 sq.ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	205 / 3	Re Conc Column	0	.	0	.	4	100	0	.	4 each
0	1090 / 3	Exposed Rebar	0	.	0	.	1	100	0	.	1 each
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	3	100	0	.	3 each

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	215 / 3	Re Conc Abutment	65	92.86	0	.	5	7.14	0	.	70 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	0	.	5	100	0	.	5 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	234 / 3	Re Conc Pier Cap	48	70.59	12	17.65	8	11.76	0	.	68 ft
0	1080 / 3	Delamination/Spall/Patched Area	0	.	12	60	8	40	0	.	20 ft

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8393 / 3	Bulkhead Seawall Any Material	0	.	0	.	354	100	0	.	354 ft
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	314	100	0	.	314 ft

FLORIDA DEPARTMENT OF TRANSPORTATION BRIDGE MANAGEMENT SYSTEM

REPORT ID: INSP005

Inspection/CIDR Report with PDF attachment(s)

Structure ID: 874294

CIDR

DATE PRINTED: 6/25/2021

0	6000 / 3	Scour	0	.	0	.	40	100	0	.	40 ft
---	----------	-------	---	---	---	---	----	-----	---	---	-------

SUBSTRUCTURE : Substructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	8394 / 3	R/Conc Abut Slope Protection	3968	73.81	0	.	1408	26.19	0	.	5376 (SF)
0	1130 / 3	Cracking (RC and Other)	0	.	0	.	320	100	0	.	320 (SF)
0	4000 / 3	Settlement	0	.	0	.	1088	100	0	.	1088 (SF)

SUPERSTRUCTURE : Superstructure

Str Unit	Elem/Env	Description	Qty1	%1	Qty2	%2	Qty3	%3	Qty4	%4	T Qty
0	333 / 3	Other Bridge Railing	167	83.5	33	16.5	0	.	0	.	200 ft
0	1000 / 3	Corrosion	0	.	30	100	0	.	0	.	30 ft
0	1020 / 3	Connection	0	.	3	100	0	.	0	.	3 ft

Total Number of Elements*: 10

*excluding defects/protective systems

Inspection Information**Inspection Date:** 04/26/2021**Type:** Interim**Inspector:** KNMEIAG - Armando Guzman**Inspection Notes:** Sufficiency Rating Calculation Accepted by knmeira at 5/5/2021 3:15 PM.

The structure is on a 6 months inspection frequency due to NBI Rating 3 for SIA Items 58 Deck and 59 Superstructure. (04/26/2021).

This Interim inspection (04/26/2021) was conducted to evaluate Element 8099 PS Conc Slab (Sonovoid), Element 234 Re Conc Pier Cap and Element 205 Re Conc Column, for the status of the entire structure refer to the last Regular NBI Inspection (04/06/2020).

The Deck and Superstructure are coded 3 (Serious) due to spalls and delaminations along more than 25% of any of the slab units. Slabs Units 1-6, 2-7, and 2-8 meet this criteria. (04/26/2021).

The Substructure NBI Rating is coded 4 (Poor) due to extensive spalls with exposed rebars along Column 2-2, and delaminations and cracks along the columns and pier caps throughout the structure. (04/26/2021).

LOAD CAPACITY EVALUATION:

Since the current load rating dated 1/13/2020, there is no indication that deterioration, geometric changes or additional dead load have occurred that would warrant a new load rating analysis. This only applies to this inspection dated 04/26/2021 per Julie A. Vers, P.E.

LEGEND:

NCAR: NO CORRECTIVE ACTION RECOMMENDED

RT: Right

LT: Left

L: Long

W: Wide

H: High

D: Deep

in.: Inches

ft.: Feet

LF: Linear Feet

SF: Square Feet

NE: Northeast

NW: Northwest

SE: Southeast

SW: Southwest

**FLORIDA DEPARTMENT OF TRANSPORTATION
BRIDGE MANAGEMENT SYSTEM**

REPORT ID: INSP005

Structure ID: 874294

**Inspection/CIDR Report with PDF attachment(s)
CIDR**DATE PRINTED: 6/25/2021

Structure Notes

BRIDGE OWNER: MIAMI-DADE COUNTY

Bridge inventoried from south to north. (Entrance on North end, boat ramp on South end).

P/S Slab Units on R/Conc Caps and Abutments over P/Conc Columns. (3 spans)

TRAFFIC RESTRICTIONS:

Based on the current load rating analysis dated 1/13/2020, the bridge is posted for the SU, C and ST5 type vehicles as follows: SU = 11 tons, C = 16 tons, ST5 = 18 tons. Refer to posting signs Photos 19 and 20.

REVIEWED BY:

Schedule Notes

**APPENDIX C – HANNA et. al, “TRANSVERSE POST-TENSIONING DESIGN AND DETAILING OF
PRECAST, PRESTRESSED CONCRETE ADJACENT-BOX-GIRDER BRIDGES”**

Transverse post-tensioning design and detailing of precast, prestressed concrete adjacent-box-girder bridges

**Kromel E. Hanna,
George Morcous,
and Maher K. Tadros**

Precast concrete adjacent-box-girder bridges are the most prevalent box-girder system for short- and medium-span bridges (which typically span from 20 ft to 127 ft [6.1 m to 38.7 m]), especially on secondary roadways. These bridges consist of multiple precast concrete box girders that are butted against each other to form the bridge deck and superstructure.

There is new interest in using these bridges for rapid construction under the Federal Highway Administration (FHWA) Highways for Life program. Adjacent box girders are generally connected using partial- or full-depth grouted shear keys along the sides of each box. Transverse ties are usually used in addition to the grouted shear keys, and they may vary from a limited number of threaded rods to several post-tensioned tendons. In some cases, no topping is applied to the structure, while in other cases a non-composite topping or a composite structural slab is added.

Bridges built with adjacent precast, prestressed concrete box girders have several advantages:

Editor's quick points

- This paper presents a review of various transverse design and detailing practices for adjacent-box-girder bridges.
- Design charts were developed for various combinations of span length, bridge width, skew angle, and girder depth using the latest loading from *AASHTO LRFD Bridge Design Specifications* to update the information in section 8.9 of the *PCI Precast Prestressed Concrete Bridge Design Manual*, which was based on an earlier version of the AASHTO standard specifications.
- This research was funded by PCI through the Daniel P. Jenny Fellowship.

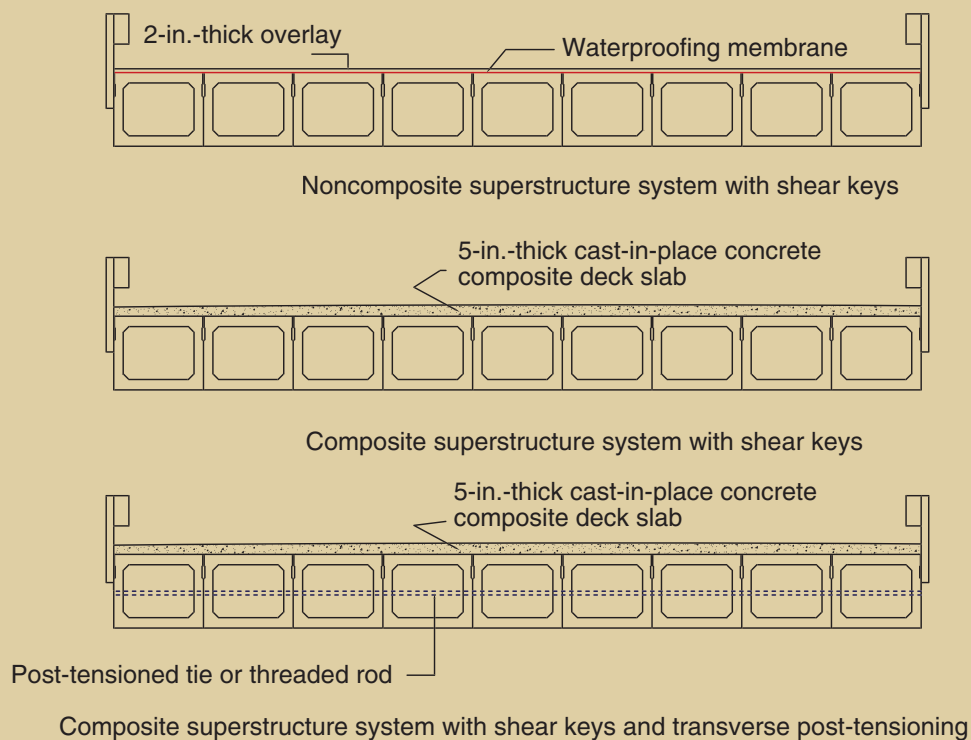


Figure 1. Adjacent-box-girder bridges incorporate various practices in the design and detailing of transverse connecting systems. Note: 1 in. = 25.4 mm.

- ease and speed of construction because of eliminating concrete forming and placing operations (for example, the Arbor Rail Line Bridge in Nebraska City, Neb., was erected and opened to traffic within 72 hr)¹
- a shallow superstructure depth, which is often necessary to maintain the required vertical clearance (for example, an interstate bridge in Colorado has a span-to-depth ratio of 39)
- low construction cost compared with I-girder bridges and other competing systems
- hollow portions inside the box girders that reduce the self-weight of the girders and provide space for gas lines, water pipes, telephone ducts, storm drains, and other utilities
- improved bridge aesthetics because of the flat soffit and slender superstructure
- high torsional stiffness, which is ideal for curved-bridge construction

Bridges constructed using box girders have been in service for many years and have generally performed well. However, a recurring problem is cracking in the grouted joints

between adjacent units, resulting in reflective cracks in the wearing surface.

The development of these longitudinal cracks over the shear keys jeopardizes the durability and structural behavior of adjacent-box-girder bridges.^{2,3} In most cases, the cracking leads to leakage, which allows chloride-laden water to penetrate the sides and bottoms of the girders, causing corrosion of the steel reinforcement. In addition, the load distribution among the girders is adversely affected because the loaded girders are required to carry more load than the design load.³

These deficiencies have led to severe deterioration and premature replacement of several bridges. On December 27, 2005, the east-side fascia girder of the Lakeview Drive Bridge over Interstate 70 in Washington, Pa., failed near midspan and fell to the highway below. Inspection of the bridge revealed heavy spalling and corrosion of the strands on the bottom flange of the failed noncomposite prestressed concrete box girder. Additional corrosion was revealed on other box girders, and the bridge was subsequently removed from service.⁴

A similar failure occurred in a railroad bridge in Nebraska in 2007. Unfortunately, public attention focuses on the few failed cases and not on the many successful examples.

Current practice

Adjacent-box-girder bridges incorporate various practices in the design and detailing of transverse connecting systems. **Figure 1** shows three configurations. The first is a noncomposite system with a nonstructural overlay as the riding surface applied directly to the top flange of the adjacent box girders. This system depends only on the grouted shear key to provide the shear-transfer mechanism between adjacent box girders.

The second is a thick, reinforced cast-in-place concrete slab anchored to the supporting box girders using shear connectors to act as a composite superstructure system.

The third system is a typical transverse connection made between the adjacent box girders using a post-tensioning tie or a threaded rod. This transverse connection system can be used in conjunction with the composite or noncomposite systems to prevent differential deflection.

According to the Ministry of Transportation of Ontario's (MTO's) *Ontario Highway Bridge Design Code*,⁵ the general design philosophy of adjacent-member systems assumes that the entire load between adjacent members is transferred by transverse shear, and the transverse flexural rigidity is completely ignored.

Also, grouted shear keys are considered inadequate to transfer the shear force, and therefore a structural concrete slab of a minimum thickness of 5.9 in. (150 mm) is required. The transverse shear force is determined as a function of the bridge width-to-span ratio, longitudinal flexural rigidity, and longitudinal torsional rigidity.

Some states' departments of transportation (DOTs) combine the use of a structural concrete slab and transverse post-tensioning. This is based on the assumption that both shear and flexure forces must be transversely transferred at the joints between adjacent members to control both translational and rotational deformations.⁶

In Japan, adjacent box girders are designed using sections and design criteria similar to those used in the United States. However, longitudinal joints are detailed differently and transverse post-tensioning is significantly higher. Cast-in-place concrete is placed in full-depth joints that are 6.7 in. (170 mm) wide and 22 in. (560 mm) deep. After grouting, post-tensioning is applied through several ducts located at different elevations. All box girders are covered with a 2-in.-thick to 3-in.-thick (50 mm to 75 mm) asphalt-concrete wearing surface. Using the Japanese practice, longitudinal cracking and concrete deterioration has rarely been reported. El-Remaily et al.⁶ give details of the post-tensioning arrangement and joint dimensions used.

In Korea, transverse connection is achieved by using mid-depth shear keys fully filled with cast-in-place concrete in addition to heavy transverse post-tensioning similar to the Japanese practice. The choice of a mid-depth shear key is based on a detailed analysis and full-scale testing.⁷

The state of Oregon has developed empirical transverse design and detailing procedures for adjacent box girders that have demonstrated satisfactory performance over several years. The developed system is based on using transverse threaded ties at several locations according to the span length; grouted, partial-depth shear keys; and recesses as 1/4 in. (6 mm) chamfer at the bottom edges of the girder to prevent spalling due to stress concentration.

The results of research conducted by the West Virginia DOT on several bridges that had joint fracture and topping cracks revealed that vertical shear failure in the key was due to poor grouting and inadequate transverse tie force.⁸ As a result of this study, the West Virginia DOT follows certain guidelines:

- Post-tensioned high-strength ties are used.
- A pourable epoxy is used instead of a nonshrink grout in the shear key.
- The surfaces to be grouted are sandblasted.

Before 1992 in New York state, depths of shear keys were about 12 in. (300 mm) from the tops of the precast concrete girders.⁹ Transverse tendons applying a compressive force of 30 kip (133 kN) were used across the width of a bridge. Spans up to 50 ft (15 m) long had no transverse tendons, but those from 50 ft to 75 ft (23 m) long had one transverse tendon at the center. For those longer than 75 ft, tendons were used only at the outer quarter points.

The bridge continuity in transverse direction was ensured by using a 6-in.-thick (150 mm), cast-in-place concrete deck slab reinforced with welded-wire reinforcement. A survey in 1990⁸ indicated that 54% of such bridges built from 1985 to 1990 had developed longitudinal cracks over the shear keys. In 1992, two major changes were adopted in New York state's design standards:

- Shear keys were placed at almost the full depth of the precast concrete box girders.
- The number of transverse tendons was increased to three for spans less than 50 ft (15 m) and five for longer spans.

Since the changes were adopted, more than 100 bridges have been built statewide. In 1996, a survey was conducted to evaluate the effectiveness of implemented design changes. The survey indicated that only 23% of the bridges

built from 1993 to 1996 experienced longitudinal cracks. This indicated the effectiveness of applying transverse post-tensioning to reduce cracking of the deck slab.⁹

The Ohio DOT constructed a high-performance concrete (HPC) adjacent-box-girder bridge.¹⁰ This bridge was constructed as a replacement for a three-span bridge. The bridge used an experimental shear key at mid-depth of the cross section. The girders were tightened together using nonprestressed threaded rods located transversely through diaphragms at the ends and quarter points of the bridge.

The shear keys were grouted after tightening the transverse bars. The area above the shear key was filled with sand and a sealant to further guard against leakage. After constructing the entire bridge width, the bridge was subjected to an eccentric load of 120 kip (534 kN) using four Ohio DOT trucks filled with gravel. The researchers reported that the deflection profiles in the transverse direction showed that all of the girders were working together. In addition, while subjecting the bridge to eccentric load, the deflection on the loaded side was greater than that on the opposite side of the bridge width.

Miller et al.¹¹ and Hlavacs et al.¹² studied the performance of nonshrink grout and epoxy in shear keys. Nonshrink grout in shear keys close to the top edge of the girder experienced cracks before any load was applied. The researchers reported that these cracks developed because of temperature stresses. The use of epoxy grout made it possible to prevent cracking under either temperature or load effects, but the coefficient of its thermal expansion was two to three times greater than that of concrete.

Gulyas et al.¹³ compared the behavior of nonshrink grout with the behavior of magnesium ammonium phosphate mortars in the shear keys. The researchers tested the component material in assemblies using different types of tests, such as vertical shear, direct tension, and longitudinal shear tests. The vertical shear test was intended to simulate the action of a vehicle wheel load on one member and no wheel load on the adjacent member. The direct tension test attempted to simulate the transverse shortening of the precast concrete member due to shrinkage and also to simulate the drying shrinkage that can occur in the keyway grout.

The longitudinal shear tests were performed in the direction parallel to the keyway to simulate the action of the prestressed concrete member shortening because of creep and shrinkage while the grout would not shorten to the same degree. In all tests, the magnesium ammonium phosphate-grouted assemblies displayed an exceptionally higher failure load than the nonshrink grout composite assemblies.

In an attempt to overcome the problems associated with the failure of the shear keys, El-Esnawi¹⁴ suggested a new shear-key design. The new design proposed moving the

shear key from its position in the upper third of the gap closer to the midheight of the box-girder section. His experimental program included testing the current shear-key design against the proposed one while incorporating different grout materials such as nonshrink grout, magnesium ammonium phosphate mortar, and epoxy resin mortar in both of the designs. The test specimens were loaded gradually until failure.

El-Esnawi observed that the static-load capacity was almost tripled from the current shear-key design with the same grouting material. He reported that magnesium ammonium phosphate was sensitive to carbonated concrete surfaces, and it was difficult to provide a carbonate-free contact surface to prevent the chemical reaction with magnesium ammonium phosphate. The research also revealed that epoxy grout was a strong grouting material that had excellent adhesion with concrete. However, its preparation had many difficulties and its long-term behavior under different temperature changes was questionable.

Annamalai et al.¹⁵ conducted an experimental program to investigate the effect of transverse post-tensioning on the behavior of small assemblies. The parameters studied were the number and thickness of shear keys and the level and distribution of the prestressing. They concluded that post-tensioning significantly improved the shear strength of grouted shear-key connections, and post-tensioned grouted shear-key connections exhibited a high degree of monolithic action.

Assemblies with three keys showed higher rigidity than specimens with two keys. Assemblies with a 1-in.-thick (25 mm) joint were found to have significantly higher shear strengths than specimens with 2-in.-thick (50 mm) joints for the same prestress level. The connections without shear keys and with a prestress of 800 psi (5520 kPa) had nearly the same shear strength as connections with shear keys and no prestress. Prestress in combination with shear keys provided superior performance. The shear strength was not significantly influenced by the distribution of prestress along the height of the specimen.

Stanton and Mattock¹⁶ tested the strength of welded connectors acting alone and with grout keys. The experimental program involved six specimens. Each specimen consisted of two 6-in.-thick (150 mm) reinforced concrete slabs joined together at their edges using a 5-ft-long (1.5 m) shear key.

Stanton and Mattock concluded that the forces from the wheel loads were transferred through the shear key. The steel connectors carried shear forces induced before grouting because of differential camber, and tension forces because of shrinkage. They concluded that the strength of the shear key was affected by inclined cracking in the parts of the member flanges above and below the shear key rather

than by failure of the grout itself. They recommended the use of transverse post-tensioning to improve the behavior of transverse connections.

Huckelbridge et al.³ conducted a total of six field tests on three bridges with noncomposite topping and two field tests with composite cast-in-place concrete decks. One of the bridges was tested before and after repairing a severely deteriorated joint.

They reported that a relative displacement between the girders of more than 0.001 in. (0.025 mm) indicated failure in the shear key. The magnitude of relative displacement experienced by each bridge depended on the actual length of the fracture, stiffness of the girders, and magnitude and proximity of the wheel load to the failed joint. Relative displacements between 0.003 in. and 0.02 in. (0.075 mm and 0.50 mm) were observed at joints that indicated at least partially fractured shear keys. The results also revealed that tie bars had little to no impact on shear-key performance.

Issa et al.¹⁷ tested a total of 36 full-scale specimens for vertical shear, direct tension, and flexural capacity. Four different grout materials were used to construct the shear keys in the specimens. The grout materials were set grout, set 45 for normal temperatures, set 45 for hot weather, and polymer concrete.

Polymer concrete was found to be the best material for transverse joints in terms of strength, bond, and mode of failure. However, they recommended the use of set grout in transverse deck joints due to its ease of use and satisfactory performance and polymer concrete in the joints subjected to excessive stresses or when quick repair is required.

Martin and Osburn¹⁸ tested two precast, prestressed concrete-slab bridge models. Each model consisted of three adjacent precast, prestressed concrete slabs that were connected by two different types of transverse connections. The precast, prestressed concrete slabs had a cross section of 8 in. \times 36 in. (200 mm \times 910 mm), a length of 18 ft (5.5 m), and a span of 16 ft (4.9 m).

Each bridge model was tested by loading the two outer slabs cyclically at midspan by equal concentrated loads of 16 kip (71 kN), which was intended to simulate American Association of State Highway and Transportation Officials (AASHTO) HS-20 wheel loads.

In the first bridge model, the slabs were joined together by tie rods at the third point of the span, and the tie rods were tensioned to 12 kip (53 kN). The joints were grouted using high-strength, nonshrink grout.

In the second bridge model, the slabs were joined together with three welded connectors located at both supports and

midspan. The joints were grouted using relatively low-strength, high-shrinkage grout.

In both bridge models, it was found that the moment resisted by each outer slab was about 33% greater than the moment resisted by the middle slab. Martin and Osburn concluded that a properly grouted shear key and either transverse tie rods or welded connectors are an effective way to transfer shear between adjacent members.

El-Shahawy¹⁹ investigated the behavior of the transverse connections in the double-tee bridges. He tested a half-scale bridge model consisting of three 30-ft-long (8.2 m) double-tees. The transverse connections consisted of V-shaped joints between the girders filled with nonshrink portland cement grout and transverse post-tensioning strands. The developed stresses due to transverse post-tensioning strands were equal to 150 psi (1030 kPa) at the middle portion and 300 psi (2070 kPa) at the ends.

The behavior of the transverse connection was investigated by conducting several punching-shear tests on the deck slab followed by a load-distribution test across the entire bridge width. The results from all tests indicated that the selected level of transverse prestressing satisfied the design requirements. It was also concluded that transverse post-tensioning helped the slab achieve monolithic behavior.

According to the *AASHTO LRFD Bridge Design Specifications*,²⁰ the use of transverse mild-steel rods secured by nuts is not sufficient to achieve full transverse flexural continuity. Section 5.14.4.3.3d recommends a minimum effective post-tensioning pressure of 250 psi (1720 kPa) through the shear key. There is neither a rational justification for this value nor an adequate explanation regarding the area over which this pressure is applied when different shear keys are used.

The PCI subcommittee on adjacent-member bridges conducted a survey on the current practices in the design and construction of adjacent-box-girder bridges in United States and Canada.⁹ This survey indicated that 29 states and 3 provinces are currently using adjacent-box-girder bridges.

Most of these transportation agencies have experienced premature reflective cracks in the wearing surface on the bridges built in the late 1980s and early 1990s. These agencies have emphasized the importance of eliminating these cracks that allow the penetration of water and deicing chemicals and lead to the corrosion of reinforcing steel in the sides and bottoms of concrete box girders. The states and provinces have recommended preventive actions based on the lessons learned in the past two decades:

- Cast-in-place concrete deck on top of the adjacent box girders can prevent water leakage and uniformly distribute the loads on adjacent box girders.

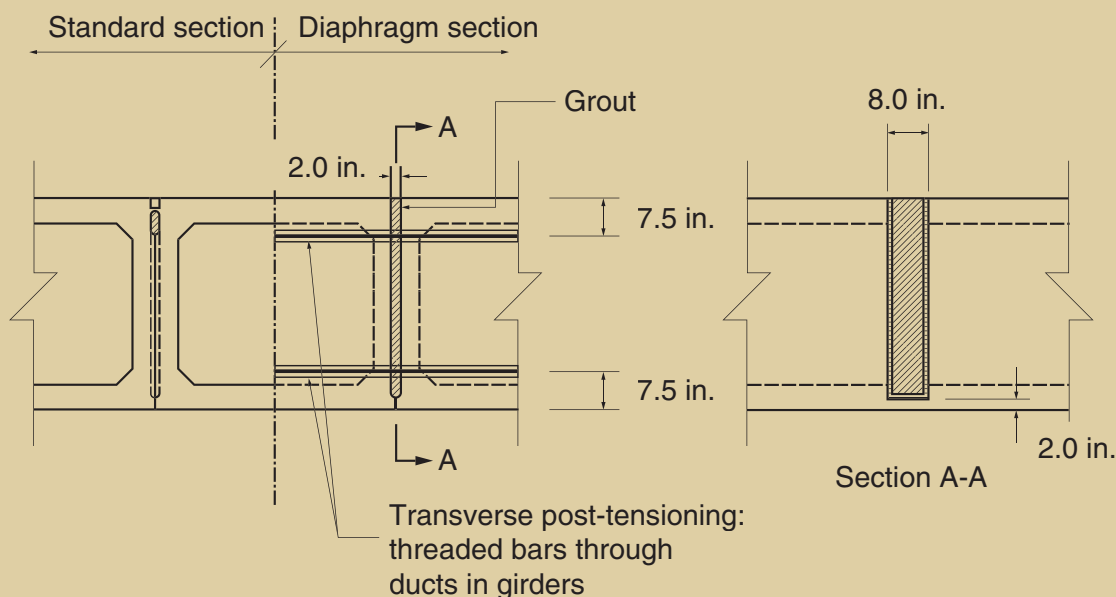


Figure 2. The transverse diaphragms are made continuous across the entire width of the bridge using grouted full-depth shear keys and post-tensioning tendons. Source: Figure 8.9.3-1. PCI Bridge Design Manual Steering Committee, *Precast Prestressed Concrete Bridge Design Manual* (Chicago, IL: PCI, 2003). Note: 1 in. = 25.4 mm.

- Nonshrink grout or the appropriate sealant instead of the conventional sand-cement mortar in the shear keys should be used in addition to blast cleaning of key surfaces prior to grouting. Also, a few states have recommended the use of full-depth shear keys due to their superior performance over the traditional top-flange keys.
- Transverse post-tensioning is recommended to improve load distribution and minimize differential deflections among adjacent box girders. Adequate post-tensioning should be applied after grouting the shear keys to minimize the tensile stresses that cause longitudinal cracking at these joints.
- End diaphragms should be used to ensure proper seating of adjacent box girders, and intermediate diaphragms should be used to provide the necessary stiffness in the transverse direction.
- Wide bearing pads under the middle of the box and sloped bearing seats that match the surface cross slope are recommended to eliminate the rocking of the box while grouting the shear keys.
- Adequate concrete cover and corrosion-inhibiting admixtures should be used in the concrete to resist the chloride-induced corrosion of reinforcing steel.
- It is recommended to eliminate the use of welded connections between adjacent box girders and to avoid

dimensional tolerances that result in inadequate sealing of the shear keys.

PCI method

PCI's *Precast Prestressed Concrete Bridge Design Manual*²¹ method was developed by El-Remaily et al.⁶ and is reported in section 8.9 of the manual. In this method, the post-tensioning force required to achieve adequate stiffness in the transverse direction to keep differential deflection within the acceptable limit (0.02 in. [0.50 mm]) is calculated.

This method assumes that post-tensioned transverse diaphragms are the primary mechanism for the distribution of wheel loads across the bridge. Five diaphragms are provided in each span: one at each end, one at midspan, and one at each quarter point. Without diaphragms, each box girder must be designed to carry a full set of wheel loads without contribution from adjacent box girders. As a result, a large differential deflection between adjacent girders will take place and reflective cracking is generally expected. However, if the box girders are transversely connected using diaphragms, the loads are distributed over the entire bridge width, and the deflected shape becomes a smooth curve. The transverse diaphragms are made continuous across the entire width of the bridge using grouted, full-depth shear keys and post-tensioning tendons (**Fig. 2**).

To determine the required amount of post-tensioning, the bridge is analyzed using a grid model. A series of longitu-

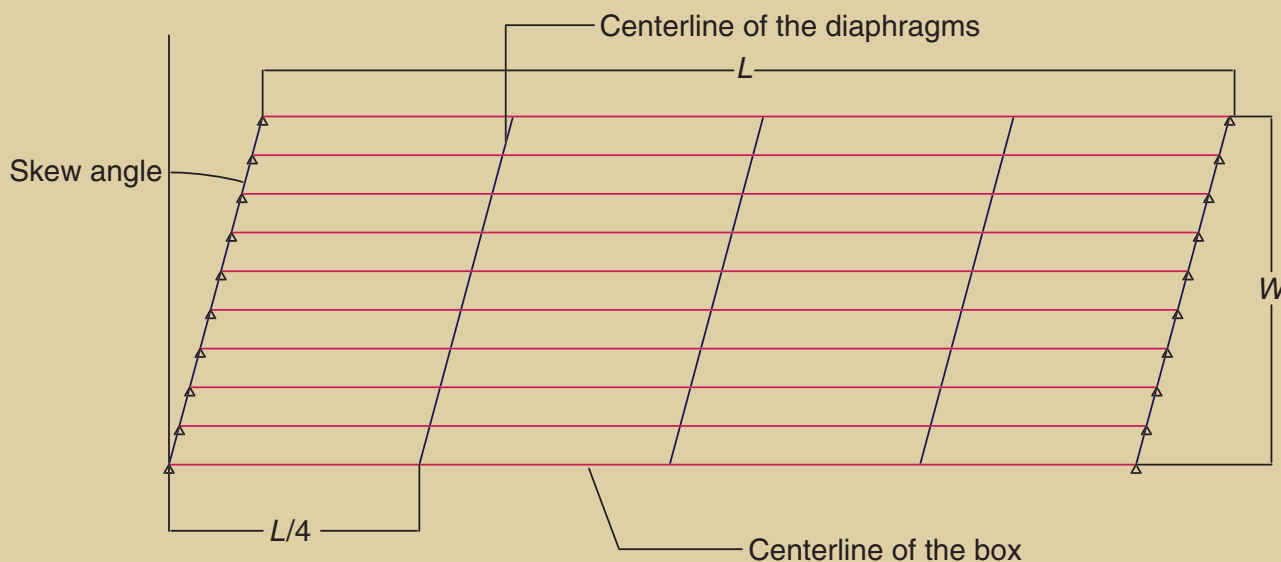


Figure 3. This drawing shows the grid analysis model. Note: L = span length; W = bridge width.

dinal girder elements located at the centerline of each box girder is used to represent the box girders, and a series of transverse girder elements located at the ends and quarter points is used to represent the diaphragms (**Fig. 3**). The joints between elements allow the transmission of shear, bending, and torsion. The weight of barrier rails and live loads are the main source of transverse bending moments generated in the diaphragms. This is because self-weight, deck weight, and wearing-surface weight are considered uniform on all of the elements and therefore do not generate any differential movements.

Transverse post-tensioning force is calculated so that diaphragm concrete stresses due to both loads and post-tensioning are within the allowable limits (compression = $0.6 f'_c$ where f'_c is specified compressive strength of concrete and tension is 0). Tensile stresses are not permitted in the diaphragm in order to prevent possible cracking at the interface between precast concrete components and the grout at shear-key locations. Also, post-tensioning force is applied concentrically in the transverse direction because diaphragms experience significant alternating positive and negative bending moments under different loading conditions.

The design chart currently available in the PCI bridge design manual was developed for the AASHTO standard box girders in **Fig. 4** and **Table 1**, assuming mild skew angles (that is, less than 15 deg), average span lengths, and AASHTO HS-25 truck loading with impact.⁶ New charts need to be developed to accommodate the cases of highly skewed bridges with different span lengths and using the AASHTO LRFD specifications truck and lane loads in addition to dynamic load allowance.²⁰

Updated design charts and design equation

The updated design charts were developed using the same PCI method for the four standard AASHTO box girders in **Fig. 4** and **Table 1**. For each girder, several combinations of bridge width, span length, and skew angle were considered. The AASHTO LRFD specifications for truck and lane live loads (HL-93) and dynamic load allowance (33% for truck load only) were applied in addition to 0.48 kip/ft (7.0 kN/m) for the self-weight of a solid concrete barrier.²⁰

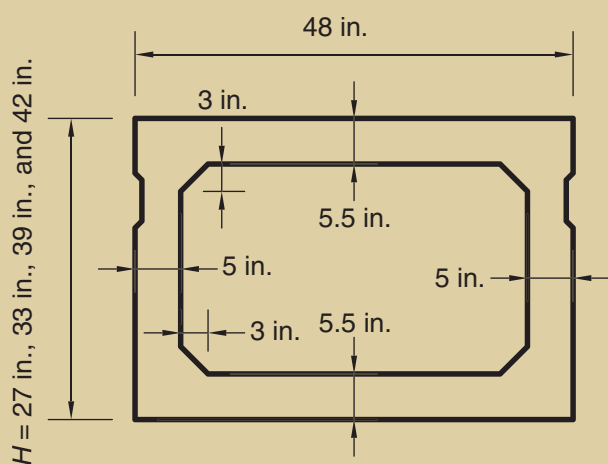


Figure 4. This drawing shows the American Association of State Highway and Transportation Officials' standard box girder used for developing the design charts currently available in the PCI *Precast Prestressed Concrete Bridge Design Manual*. Note: H = height of box girder. 1 in. = 25.4 mm.

Table 1. Box beam properties

Type	Height H , in.	Area A , in. ²	Y_{bottom}	Moment of inertia I , in. ⁴
BI-48	27	692.5	13.37	65,941
BII-48	33	752.5	16.33	110,499
BIII-48	39	812.5	19.29	168,367
BIV-48	72	842.5	20.78	203,088

Note: Y_{bottom} = distance from bottom of girder to center of gravity. 1 in. = 25.4 mm.

Figure 5 shows the effective post-tensioning force versus bridge width for the four standard box girders, assuming a 0 deg skew angle and a span-to-depth ratio of 30. This graph indicates that for any girder depth, the wider the bridge, the higher the required post-tensioning force. It also indicates that the required force is higher in shallower girders than in deeper girders for the same bridge width. This is mainly to compensate for the reduction in the transverse stiffness due to the use of shallower diaphragms. Each line in Fig. 5 has two different curvatures. The first curvature represents the relationship when the negative moment controls the design, which occurs in the relatively narrow bridge widths (up to 52.0 ft [15.9 m]). The second curvature represents the relationship when the positive moment controls the design, which occurs in wider bridges.

Figure 6 shows the PCI bridge design manual design chart superimposed over the updated design chart. This graph indicates a significant increase in the required post-tensioning force (up to 40% in some cases) in the updated

charts. This is mainly due to the use of the AASHTO LRFD specifications on live-load and dynamic-load allowance. This increase varies depending on the box-girder depth and the bridge width, and it is more noticeable in narrow bridges than in wide bridges. It should be noted that the PCI bridge design manual values correspond to a skew angle of 15 deg and average span length, while the proposed values correspond to a skew angle of 0 deg and a span-to-depth ratio of 30.

Figure 7 shows the required post-tensioning force versus bridge width for a 0 deg skew angle and span-to-depth ratios of 30 and 40. Although the effect of the span-to-depth ratio was evaluated for the four standard box girders, only the lines for the 27-in.-deep and 42-in.-deep (690 mm and 1070 mm) box girders were plotted for clarity. This plot indicates that the span-to-depth ratio has an insignificant and variable effect on the required post-tensioning force per unit length. As the span-to-depth ratio increased, the required prestressing force increased when the design

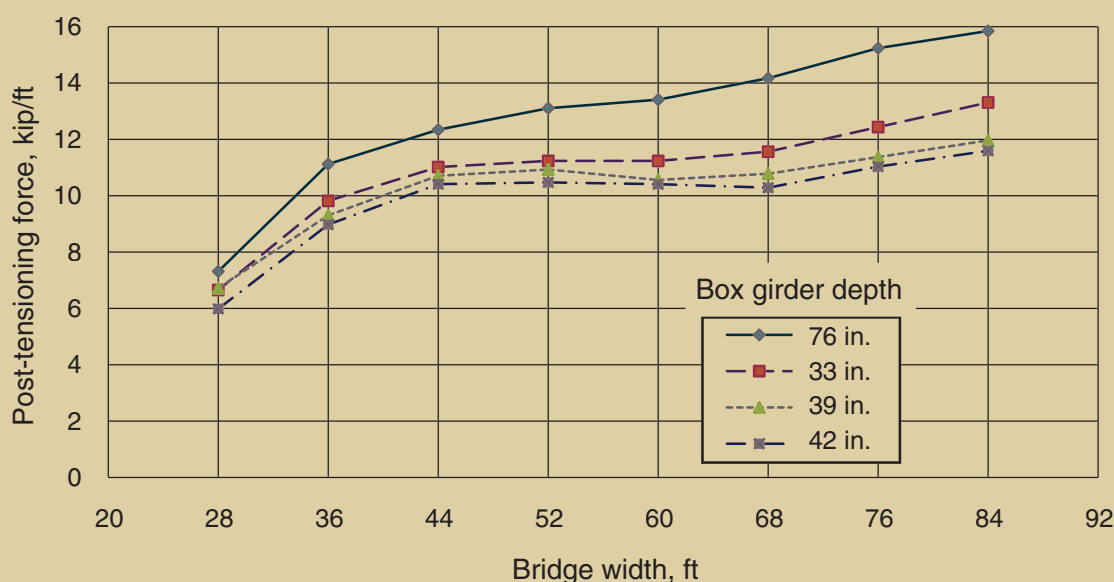


Figure 5. This graph shows the effect of bridge width on post-tensioning force at the midspan diaphragm for the four standard box girders assuming a 0 deg skew angle and a span-to-depth ratio of 30. Note: 1 in. = 25.4 mm; 1 ft = 0.305 m; 1 kip = 4.448 kN.

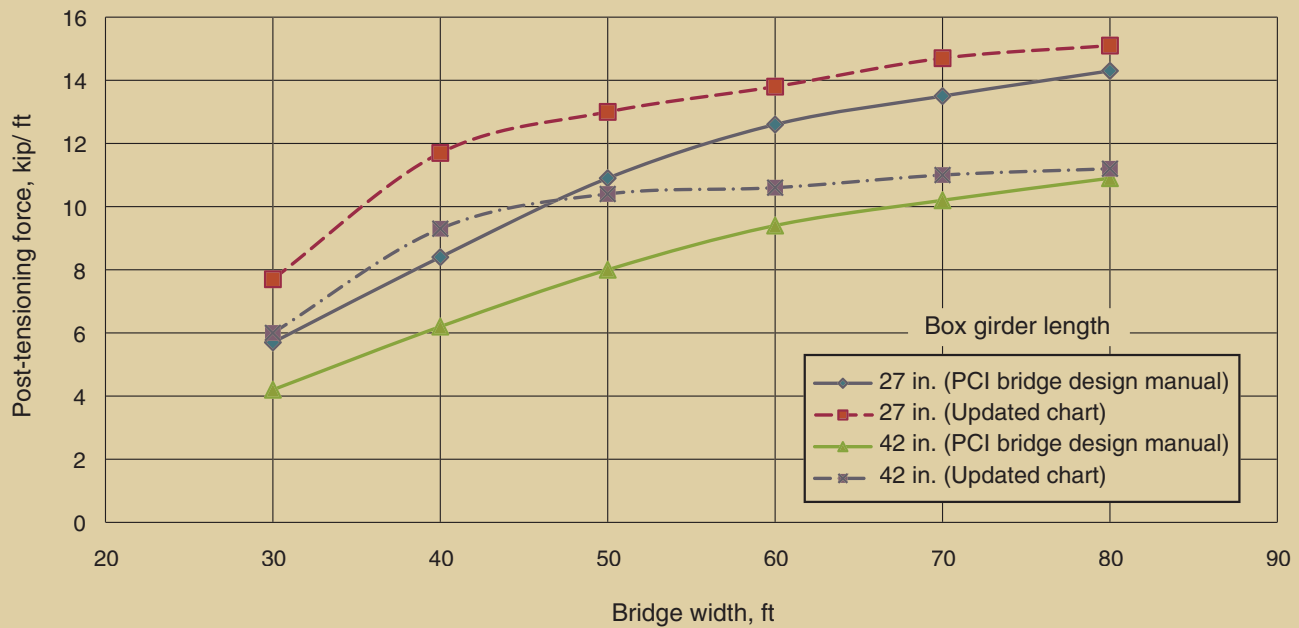


Figure 6. This graph compares the *Precast Prestressed Concrete Bridge Design Manual* design chart with updated charts showing the effect of bridge depth on post-tensioning force. Note: 1 in. = 25.4 mm; 1 ft = 0.305 m; 1 kip = 4.448 kN.

was positive-moment controlled, and decreased when the design was negative-moment controlled. This effect was more noticeable in the shallow girders.

Figure 8 shows the effect of skew angle on the required post-tensioning force at the midspan diaphragm for a bridge width of 52 ft (16 m) and a span-to-depth ratio of 30. Figure 8 indicates that the impact of the skew angle on

the required post-tensioning force is minimal, especially on deep girders that usually correspond to longer spans. For shallow girders used in short-span bridges, as the skew angle increased the required post-tensioning force also increased.

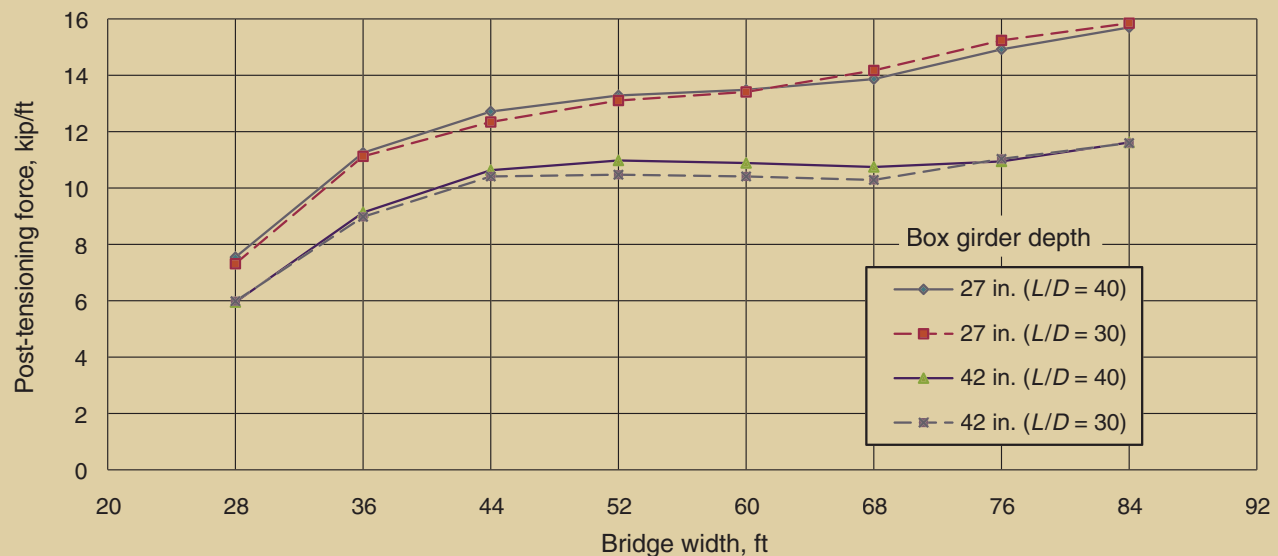


Figure 7. This graph shows the effect of the span-to-depth ratio on post-tensioning force at the midspan diaphragm for a 0 deg skew angle and span-to-depth ratios equal to 30 and 40. Note: D = depth; L = span. 1 in. = 25.4 mm; 1 ft = 0.305 m; 1 kip = 4.448 kN.

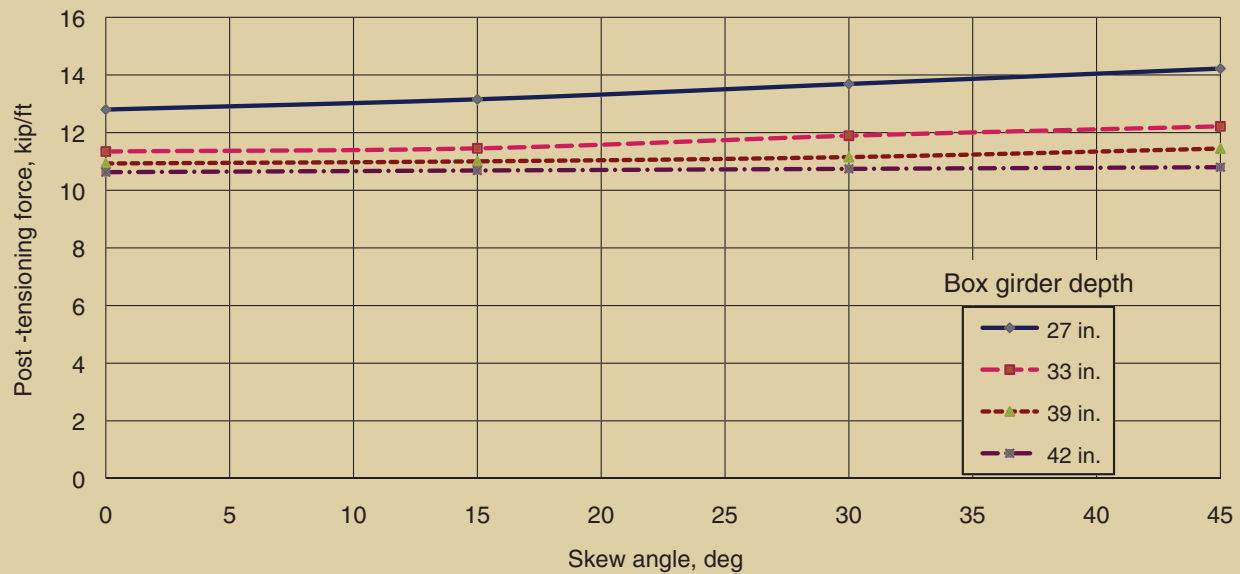


Figure 8. This graph shows the effect of the bridge skew angle on post-tensioning force for the midspan diaphragm for a bridge width of 52 ft and a span-to-depth ratio of 30. Note: 1 in. = 25.4 mm; 1 ft = 0.305 m; 1 kip = 4.448 kN.

Figures 5, 7, and 8 indicate that the bridge width and box-girder depth are the most important parameters in determining the required post-tensioning force per unit length of the bridge. Therefore, the designer should first estimate the force based on the bridge width and girder depth using the proposed design chart (Fig. 5). These values correspond to

a span-to-depth ratio of 30 and a skew angle of 0 deg and should be corrected using Fig. 7 and 8, respectively, when different span-to-depth ratios or skew angles are used.

Data from the grid analysis were used to develop a simplified design equation for calculating the required post-

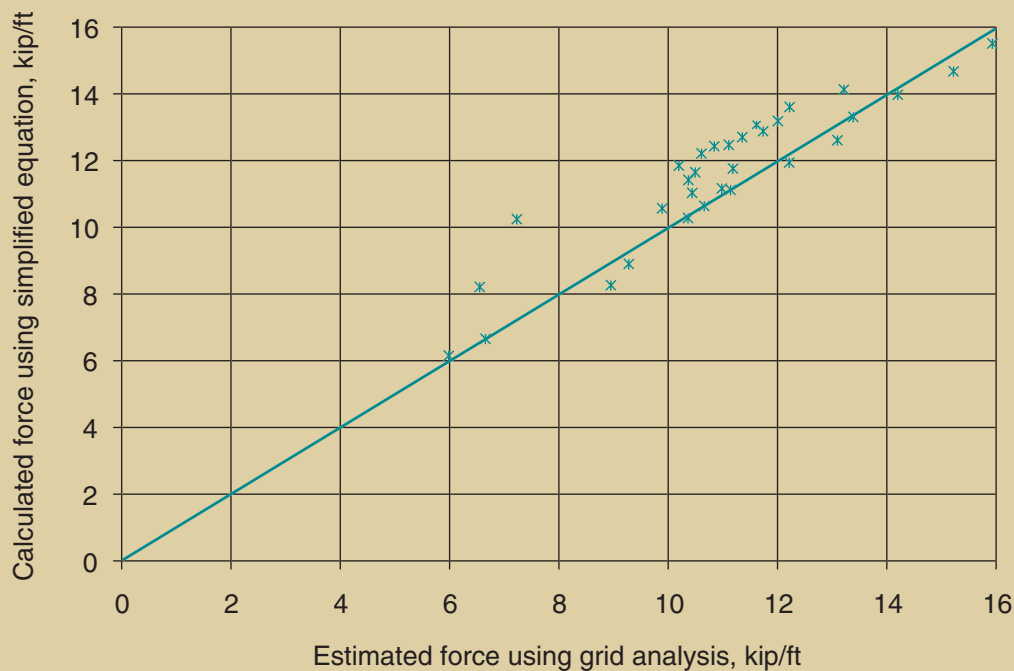


Figure 9. This graph compares the post-tensioning force estimated using grid analysis with the proposed equation. Note: 1 in. = 25.4 mm; 1 ft = 0.305 m; 1 kip = 4.448 kN.

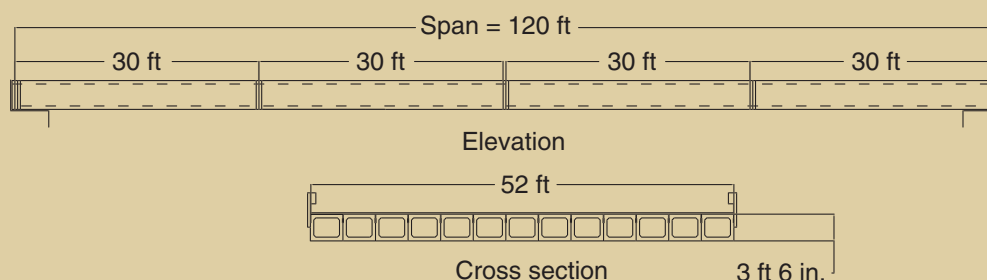


Figure 10. This drawing illustrates the bridge geometry for the design example. Note: 1 in. = 25.4 mm; 1 ft = 0.305 m.

tensioning force P (kip/ft) for the intermediate diaphragm per unit length of the bridge. The following equation was developed by fitting the data points obtained from the grid analysis of all cases. The first part of the equation represents the relationship when the negative moment controls the design, which occurs in smaller bridge widths (up to 52.0 ft [15.9 m]). The second part of the equation represents the relationship when the positive moment controls the design, which occurs in wider bridges. These relationships were assumed to be linear to eliminate sophisticated formulations.

$$P = \left(\frac{0.9W}{D} - 1.0 \right) K_L K_S \leq \left(\frac{0.2W}{D} + 8.0 \right) K_L K_S$$

where

D = box depth

W = bridge width

K_L = correction factor for span-to-depth ratio

$$= 1.0 + 0.003 \left(\frac{L}{D} - 30 \right)$$

K_S = correction factor for skew angle more than 0 deg

$$= 1.0 + 0.002\theta$$

L = bridge span

θ = skew angle

To evaluate the accuracy of the simplified equation in fitting the analysis data, the post-tensioning force values obtained using the equation were compared with those obtained using the grid analysis for several combinations of bridge width and depth. Span-to-depth ratio and skew angle were kept constant to evaluate the accuracy of the basic equation without any correction factors. **Figure 9** shows that the simplified equation provides a conservative

estimate of the required transverse post-tensioning force in most of the cases, with an average deviation of 7.7%.

Design example

The provided design example illustrates the design steps of the single-span bridge (**Fig. 10**).

Bridge data

Figure 10 shows the cross section and the elevation of the bridge.

Span = 120 ft (37 m)

Width = 52 ft (16 m)

Depth = 42 in. (1070 mm) (AASHTO LRFD specifications standard box girder)

Skew = 15 deg

Concrete strength

Precast concrete $f'_c = 6000$ psi (41 MPa)

Grout $f'_c = 6000$ psi (41 MPa)

Box girder section properties

Area $A = 842.5$ in.² (543,600 mm²)

Moment of inertia $I = 203,088$ in.⁴ (8.453×10^{10} mm⁴)

Diaphragm section properties

The cross section of the diaphragms is rectangular. The depth of the diaphragm is equal to the depth of the box girder (42 in. [1070 mm]), and the width is 8 in. (200 mm)

$A = 336$ in.² (216,800 mm²)

$I = 49,392$ in.⁴ (1.68×10^{10} mm⁴)

Loading

Dead load: curb and railing $w = 0.48$ kip/ft (7.0 kN/m)

Live load: HL-93 truck and lane load

Impact factor for truck load = 33%

Calculation of the required transverse post-tensioning force using working stresses analysis

The grid analysis was used to get the member forces. Moments of the midspan diaphragm were used for design calculations. The live-load positions were chosen to give the maximum positive and maximum negative moments. Allowable compressive strength due to effective prestress plus maximum load was calculated using the following equation.

$$0.6 f'_c = 0.6(6000) = 3600 \text{ psi (24,800 kPa)}$$

Tension is not permitted. These stresses must be checked for both the maximum positive and maximum negative load cases:

- Positive-moment load case: the unfactored maximum positive moment is 147 kip-ft (199 kN-m).

$$f_{bot} = -\left(\frac{147(12)(1000)(21)}{49,392}\right) + \frac{P(1000)}{336} \geq 0$$

where

$$P_{diaphragm} \geq 252 \text{ kip (1121 kN)}$$

f_{bot} = stress in bottom of diaphragm

$$f_{top} = -\left(\frac{147(12)(1000)(21)}{49,392}\right) + \frac{P(1000)}{336} \leq 3600$$

$$P_{diaphragm} \leq 958 \text{ kip (4381 kN)}$$

f_{top} = stress in top of diaphragm

- Negative-moment load case: the unfactored maximum negative moment is 187 kip-ft (254 kN-m).

$$f_{top} = -\left(\frac{187(12)(1000)(21)}{49,392}\right) + \frac{P(1000)}{336} \geq 0$$

$$P_{diaphragm} \geq 324 \text{ kip (1441 kN)}$$

$$f_{bot} = -\left(\frac{187(12)(1000)(21)}{49,392}\right) + \frac{P(1000)}{336} \leq 3600$$

$$P_{diaphragm} \leq 890 \text{ kip (3959 kN)}$$

Based on the previous calculations, the total required transverse post-tensioning force per diaphragm is 324 kip (1440 kN). The total required transverse post-tensioning force per foot of the bridge is 324/30, which equals 10.8 kip/ft (158 kN/m).

According to section 5.14.4.3.3d of the AASHTO LRFD specifications and using the area of the full-depth vertical shear key as the contact area, the minimum required transverse post-tensioning force per diaphragm is equal to $0.25(8)(42 - 2)$, or 80 kip (360 kN). This is low because it represents only 25% of the force calculated using the updated PCI method. If the entire side of the box is used as the contact area, the minimum required transverse post-tensioning force per diaphragm is $0.25(30)(12)(42)$, or 3780 kip (16,800 kN). This is extremely high because it is 10 times the force calculated using the updated PCI method.

Calculation of the required transverse post-tensioning force using the developed equation

From the proposed equation, the required transverse post-tensioning force is calculated as follows.

$$\begin{aligned} K_L &= 1.0 + 0.003\left(\frac{L}{D} - 30\right) \\ &= 1.0 + 0.003\left(\frac{120(12)}{42} - 30\right) = 1.013 \end{aligned}$$

$$K_s = 1.0 + 0.002\theta = 1.0 + 0.002(15) = 1.03$$

The required post-tensioning force:

$$\begin{aligned} P &= \left(\frac{0.9W}{D} - 1.0\right) K_L K_s \leq \left(\frac{0.2W}{D} + 8.0\right) K_L K_s \\ &= \left(\frac{0.9(52)(12)}{42} - 1.0\right) (1.013)(1.03) \\ &\leq \left(\frac{0.2(52)(12)}{42} + 8.0\right) (1.013)(1.03) \\ &= 12.9 \leq 11.5 \therefore P = 11.5 \text{ kip/ft (168 kN/m)} \end{aligned}$$

$$P_{diaphragm} = 11.5(30) = 345 \text{ kip (1535 kN)}$$

Required prestressing strands

Two tendons will be used in each diaphragm. The required area of post-tensioning force A_{ps} is calculated by dividing the required force $P_{diaphragm}$ by the effective prestress f'_s , which is assumed to be 55% of the ultimate strength of the strands f_{pu} .

$$A_{ps} = 345 / (0.55 \times 270) = 2.32 \text{ in.}^2 (15.0 \text{ mm}^2)$$

Try six 0.6-in.-diameter strands at each tendon. The total area is 2.604 in.² (16.80 mm²), which is acceptable.

Conclusion

Based on the results of the parametric study and the comparison of the updated design chart with the existing PCI bridge design manual design chart, several conclusions are made:

- The latest AASHTO LRFD specifications for live-load and dynamic-load allowance cause a significant increase (up to 40% in some cases) in the required transverse post-tensioning force for adjacent-box-girder bridges.
- The bridge width and girder depth have the most significant effect on the required transverse post-tensioning force. For any girder depth, an increase in the bridge width is accompanied by a higher post-tensioning force. Also, the required force is higher in shallower girders than in deeper girders for the same bridge width.
- Span-to-depth ratio has a variable effect on the required transverse prestressing force per unit length. As the span-to-depth ratio increases, the required prestressing force also increases when positive moment controls the design, and less prestressing force is required when negative moment controls. This effect is more noticeable in the shallow girders.
- Skew angle has a minimal effect on the required transverse post-tensioning force, especially on deep girders that usually correspond to longer spans. For shallow girders used in short-span bridges, greater skew angles require more transverse post-tensioning force.
- The simplified design equation provides the required transverse post-tensioning force per unit length of the bridge as a function of its width and box-girder depth and accounts for the span-to-depth ratio and skew angle using correction factors. The average deviation of the values calculated using the simplified equation and the grid analysis results is 7.7%.

Acknowledgments

The authors acknowledge the invaluable support of the PCI subcommittee on Adjacent Member Bridges led by Kevin Eisenbeis and the financial and technical support of PCI through the Daniel P. Jenny Fellowship.

References

1. Hennessey, S. A., and K. A. Bexten. 2002. Value Engineering Results in Successful Precast Railroad Bridge Solution. *PCI Journal*, V. 47, No. 4 (July–August): pp. 72–77.
2. Kahl, S. 2005. Box-Beam Concerns Found under the Bridge. *C&T Research Record*, No. 102 (September): pp. 1–4.
3. Huckelbridge, A. A., H. El-Esnawi, and F. Moses. 1995. Shear Key Performance in Multi-Beam Box Girder Bridges. *Journal of Performance of Constructed Facilities*, V. 9, No. 4 (November): pp. 271–285.
4. Naito, C., R. Sause, I. Hodgson, S. Pessiki, and C. Desai. 2006. Forensic Evaluation of Prestressed Box Beams from the Lake View Drive Bridge over I-70. Advanced Technology for Large Structural Systems (ATLSS) report no. 06-13.
5. Ministry of Transportation of Ontario (MTO). 1995. *Ontario Highway Bridge Design Code*. 1995. MTO.
6. El-Remaily, A., M. K. Tadros, T. Yamane, and G. Krause. 1996. Transverse Design of Adjacent Precast Prestressed Concrete Box Girder Bridges. *PCI Journal*, V. 41, No. 4 (July–August): pp. 96–113.
7. Nam, J. W., H. J. Kim, J. H. Kim, S. H. Nam, S. B. Kim, and K. J. Byun. 2008. International Perspective: Overview and Application of Precast Prestressed Box-Beam Bridges in Korea. *PCI Journal*, V. 53, No. 4 (July–August): pp. 83–107.
8. PCI Bridges Committee. 2008. Reflective Cracking in Adjacent Box Girder Bridge Superstructures. *Subcommittee on Adjacent Box Beam Bridges*, October.
9. Lall, J., S. Alampalli, and E. F. Dicocco. 1998. Performance of Full-Depth Shear Keys in Adjacent Prestressed Box Beam Bridges. *PCI Journal*, V. 43, No. 2 (March–April): pp. 72–79.
10. Greuel, A., T. M. Baseheart, B. T. Rogers, R. A. Miller, and B. M. Shahrooz. 2000. Evaluation of a High Performance Concrete Box Girder Bridge. *PCI Journal*, V. 45, No. 6 (November–December): pp. 60–71.

11. Miller, R. A., G. M. Hlavacs, T. Long, and A. Greuel. 1999. Full-Scale Testing of Shear Keys for Adjacent Box Girder Bridges. *PCI Journal*, V. 44, No. 6 (November–December): pp. 80–90.
12. Hlavacs, G. M., T. Long, R. A. Miller, and T. M. Baseheart. 1997. Nondestructive Determination of Response of Shear Keys to Environmental and Structural Cyclic Loading. *Transportation Research Record*, No. 1574 (November): pp. 18–24.
13. Gulyas, R. J., G. J. Wirthlin, and J. T. Champa. 1995. Evaluation of Keyway Grout Test Methods for Precast Concrete Bridges. *PCI Journal*, V. 40, No. 1 (January–February): pp. 44–57.
14. El-Esnawi, H. H. 1996. Evaluation of Improved Shear Key Designs for Multi-Beam Prestressed Concrete Box Girder Bridges. PhD thesis. Case Western Reserve University, Cleveland, Ohio.
15. Annamali, G., and R. C. Brown. 1990. Shear Transfer Behavior of Post-tensioned Grouted Shear Key Connections in Precast Concrete-Framed Structures. *ACI Structural Journal*, V. 87, No. 1 (January-February): pp. 53–60.
16. Stanton, J. F., and A. H. Mattock. 1986. *Load Distribution and Connection Design for Precast Stemmed Multi-Beam Bridge Superstructures*. TRB report no. 287. Washington, DC: Transportation Research Board.
17. Issa, M. A., C. L. R. Valle, S. Islam, and H. A. Abdalla. 2003. Performance of Transverse Joint Grout Materials in Full-Depth Precast Concrete Bridge Deck Systems. *PCI Journal*, V. 48, No. 4 (July–August): pp. 92–103.
18. Martin, L. D., and A. E. N. Osborn. 1983. Connections for Modular Concrete Bridge Decks. Federal Highway Administration 82/106, National Technical Information Service document PB84-118058, Consulting Engineering Group Inc., Glenview, IL.
19. El-Shahawy, M. 1990. Feasibility Study of Transversely Prestressed Double Tee Bridges. *PCI Journal*, V. 35, No. 5 (September–October): pp. 56–69.
20. American Association of State Highway and Transportation Officials (AASHTO). 2004. *AASHTO LRFD Bridge Design Specifications*. 3rd ed. Washington, DC: AASHTO.
21. PCI Bridge Design Manual Steering Committee. 2003. *Precast Prestressed Concrete Bridge Design Manual*. MNL-133. 2nd ed. Chicago, IL: PCI.

Notation

A = area

A_{ps} = required area of post-tensioning force

D = depth

f_{bot} = stress in bottom of diaphragm

f'_c = specified compressive strength of concrete

f_{pu} = ultimate strength of the strand

f'_s = effective prestress

f_{top} = stress in top of diaphragm

H = height

I = moment of inertia

K_L = correction factor for span-to-depth ratio

K_S = correction factor for skew angle more than 0 deg

L = bridge span

P = post-tensioning force per unit length of the bridge

$P_{diaphragm}$ = post-tensioning force on the diaphragm

w = dead load of curb and railing

W = bridge width

Y_{bottom} = distance from bottom of girder to center of gravity

θ = skew angle

About the authors



Kromel E. Hanna, PhD, is a Post-Doctoral Fellow for the Civil Engineering Department at the University of Nebraska–Lincoln in Omaha, Neb.



George Morcous, PhD, P.E., is an assistant professor for the Construction Systems Department at the University of Nebraska–Lincoln.



Maher K. Tadros, PhD, P.E., is a Leslie D. Martin Professor of Civil Engineering at the University of Nebraska–Lincoln.

Synopsis

Precast, prestressed concrete adjacent box girders are widely used in short- and medium-span bridges. Rapid construction and low construction cost are the main attractions of this system. Also, the continuous flat soffit and relatively high span-to-depth ratio make this system aesthetically pleasing.

However, reflective cracking and leakage have been reported along the longitudinal joints between adjacent box girders in a number of bridges. The cracking and leakage are mainly due to inadequate design and detailing of the transverse connection between adjacent box girders, which eventually leads to excessive

differential displacement and rotation of adjacent box girders. The reflective cracking and leakage allow chloride-induced corrosion of reinforcing steel and prestressing strand and premature deterioration of the bridge superstructure.

This paper presents a review of the various practices in the transverse design and detailing of adjacent-box-girder bridges. The basis for calculating the transverse post-tensioning force according to PCI's *Precast Prestressed Concrete Bridge Design Manual* is discussed. Design charts and equations were developed for various combinations of span length, bridge width, skew angle, and girder depth using the latest loading from *AASHTO LRFD Bridge Design Specifications*. These aids may be viewed as an update to the information in section 8.9 of the PCI bridge design manual, which was based on an earlier version of the AASHTO standard specifications.


Keywords

Adjacent box girder, bridge deterioration, grid analysis, longitudinal joint, rapid construction, shear key, transverse design.

Review policy

This paper was reviewed in accordance with the Precast/Prestressed Concrete Institute's peer-review process.

Reader comments

Please address any reader comments to *PCI Journal* editor-in-chief Emily Lorenz at elorenz@pci.org or Precast/Prestressed Concrete Institute, c/o *PCI Journal*, 209 W. Jackson Blvd., Suite 500, Chicago, IL 60606. 

**APPENDIX D – STRUCTURAL TECHNOLOGIES, LLC, “V-WRAP C200HM HIGH MODULUS
CARBON FIBER FABRIC”**

Typical Data for V-Wrap C200HM

Storage Conditions:	Store dry at 40°F – 90°F (4°C – 32°C)
Color:	Black
Primary Fiber Direction:	0° (unidirectional)
Weight:	17.7 oz/yd ² (600 g/m ²)
Shelf life:	10 years

Fiber Properties (Dry)

Tensile Strength:	790,000 psi (5,440 MPa)
Tensile Modulus:	42 x 10 ⁶ psi (289,550 MPa)
Elongation:	1.9 %

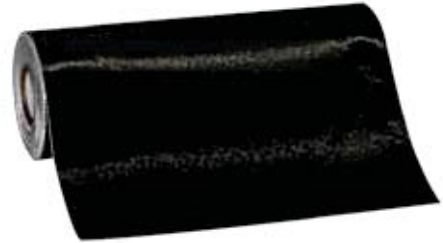
Cured Laminate Properties

Tensile Strength:	180,000 psi (1,241 MPa)
Modulus of Elasticity:	14.24 x 10 ⁶ psi (98,181 MPa)
Elongation at Break:	1.27%
Thickness:	0.04 in. (1.02 mm)
Strength per Unit Width:	7,200 lbs/in. (1.26 kN/mm)

Average Values

Design Values*

155,000 psi (1,068 MPa)
14.0 x 10 ⁶ psi (96,527 MPa)
1.1%
0.04 in. (1.02 mm)
6,200 lbs/in. (1.09 kN/mm)



*Design properties are based on ACI 440.2R using average minus three standard deviations.

Description:

V-Wrap C200HM is a unidirectional carbon fiber fabric with fiber oriented in the 0° direction. V-Wrap C200HM system is field laminated using environmentally friendly, two-part 100% solids and high strength structural adhesives to form a carbon fiber reinforced polymer (CFRP) system used to reinforce structural elements.

Product Uses:

V-Wrap strengthening systems can be used to resolve strength deficiencies and increase the load carrying capacity of building, bridges, silos, chimneys, and other structures.

Loading Increases:

- Increasing the live loads capacity of floor systems
- Increasing shear and flexural strengths of reinforced and prestressed beams
- Increasing the axial capacity of columns
- Increasing the live load capacity of parking garages

Seismic Strengthening:

- Column confinement for ductility improvement
- Masonry and concrete shear walls strengthening

Damage to Structural Parts:

- Correct strength deficiency due to deterioration and corrosion
- Restore strength of structural elements damaged by fire

Change in Structural System:

- Load redistribution due to removal of walls, beams or columns
- Removal of slab sections for new openings

Design or Construction Defects:

- Insufficient amount of shear or flexural reinforcement
- Insufficient size and/or layout of reinforcement
- Insufficient reinforcing bar or lap splice length
- Low compressive strength in beams, slabs, and columns

Advantages:

- ICC-ES ESR-3606 listed product
- 0% VOC
- 100% Solvent free
- Non-corrosive reinforcement system
- Lightweight flexible fabric can be wrapped around complex shapes
- Used for shear, confinement or flexural strengthening
- High strength and high modulus
- Light weight
- Reduces crack width
- Alkali resistant
- Low aesthetic impact

Packaging:

Fabric: 24 in. width x 150 ft rolls
0.61 m width x 45.7 m rolls

How To Use:

Design:

Design should comply with ACI 440.2R or recognized design/specification entity and is typically based on CFRP contribution determined by detailed analysis. Design values will vary based on project requirements and applicable environmental and strength reduction factors. Contact STRUCTURAL TECHNOLOGIES to determine applicable design factors.

Surface Preparation:

Surfaces to receive V-Wrap C200HM must be clean and sound. It must be dry and free of frost. All dust, laitance, grease, curing compounds, waxes, deteriorated materials, and other bond inhibiting materials must be removed from the surface prior to application. Existing uneven surfaces must be filled with appropriate epoxy putty or repair mortar. Use abrasive blasting, pressure wash, shotblast, grind or other approved mechanical means to achieve an open-pore texture with a concrete surface profile of CSP-3 or better (ICRI). In certain applications and at the engineer's discretion, the bond between the substrate and the fabric may be determined to be non-critical (such as in column confinement applications). All corners must be rounded to 1/2" radius minimum. A minimum overlap [or lap splice] of 6" is required to achieve continuity. The adhesive strength of the concrete may be verified after surface preparation by random pull-off testing (ASTM D7522) at the discretion of the engineer. Minimum tensile strength of 200 psi must be achieved.

Cutting V-Wrap C200HM:

Fabric can be cut to appropriate length by using a commercial quality heavy-duty scissors.

Application:

Installation of the V-Wrap C200HM strengthening system should be performed only by a specially trained, approved contractor. The V-Wrap C200HM strengthening system shall consist of V-Wrap C200HM carbon fabric and V-Wrap epoxy resins such as: V-Wrap 600, V-Wrap 700S, and V-Wrap 770.

Note the specified number of plies, ply widths, and fiber orientation. Mix resin components using recommended procedures on product datasheet. Apply one coat of V-Wrap epoxy as a primer to the surface using a nap roller. Fill minor

concrete defects such as bug holes and other imperfections using V-Wrap 770 epoxy mixed with fumed silica (thickened epoxy) or V-Wrap PF putty. Apply thickened epoxy or putty using a roller or trowel to prime surface. Adjust the gap between saturator rollers to approximately 42 mils. Using a saturator machine, pre-saturate the appropriate length of V-Wrap C200HM with V-Wrap epoxy adhesive as a saturant. Install the saturated FRP sheet. Use a rib roller to remove all air pockets and ensure intimate contact with the surface. If a splice is needed, a minimum 6" overlap is required. On multiple plies with splices, stagger the splice locations. If required, apply topcoat material.

Limitations:

- Design calculations must be approved by a licensed professional engineer.
- System is a vapor barrier.
- Concrete deterioration and steel corrosion must be resolved prior to application.
- Minimum application temperature is 40°F.

Storage:

Store material in a cool, dark space. Low humidity is recommended.

Handling:

Approved personal protection equipment should be worn at all times. Particle mask is recommended for possible airborne particles. Gloves are recommended when handling fabrics and resins to avoid skin irritation. Safety glasses are recommended to prevent eye irritation. Wear chemical resistant clothing/gloves/goggles. Ventilate area. In absence of adequate ventilation, use properly fitted NIOSH respirator.

Cleanup:

Dispose of material in accordance with local disposal regulations. Uncured material can be removed with approved solvents. Cured materials can only be removed mechanically.

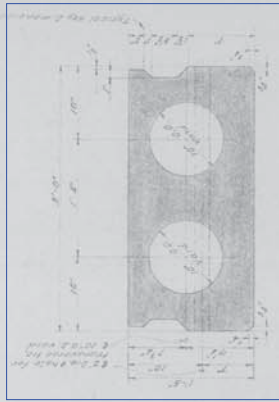
First Aid:

In case of skin contact, wash thoroughly with soap and water. For eye contact, flush immediately with plenty of water; contact physician immediately. For respiratory problems, remove to fresh air. Wash clothing before reuse.

STRUCTURAL TECHNOLOGIES, LLC warrants its products to be free from manufacturing defects and to meet STRUCTURAL TECHNOLOGIES' current published properties when applied in accordance with STRUCTURAL TECHNOLOGIES' directions and tested in accordance with ASTM and STRUCTURAL TECHNOLOGIES Standards. User determines suitability of product for use and assumes all risks. Buyer's sole remedy shall be limited to the purchase price or replacement of product and excludes labor or the cost of labor. Any claim for breach of this warranty must be brought within one year of the date of purchase.

No other warranties expressed or implied including any warranty of merchantability or fitness for a particular purpose shall apply. STRUCTURAL TECHNOLOGIES shall not be liable for any consequential or special damages of any kind, resulting from any claim or breach of warranty, breach of contract, negligence or any legal theory. STRUCTURAL TECHNOLOGIES assumes no liability for use of this product in a manner to infringe on another's patent.

**APPENDIX E – STRUCTURAL TECHNOLOGIES, LLC., PRELIMINARY BRIDGE REPAIR
RECOMMENDATIONS**



PARTIALLY FILL CORES WITH CONCRETE TO CONNECT THE NEW CIP CONCRETE

PARTIALLY FILL WITH FOAM TO CREATE A BACKING FOR THE REPAIR CONCRETE

LONGITUDINAL FRP 2 PILES 36" WIDE VWRAP C200HM FULL LENGTH OF PLANK - 40 FT

INSTALL #4 CONCRETE 18" DIA. CORES WITH RE-500 V2 EPOXY 6" INTO THE EXISTING CONCRETE

31#2 (PER PLANK) 24" WITH GOOD PT STRANDS

PLANK UNIT 2-8 (VERIFY)

PLANK UNIT 2-9 (VERIFY)

2021-10-01 MATHESON HAMMOCK ROAD OVER MH CANAL

PROPOSED REPAIR/STRENGTHENING

1. (2) PLANKS - UNIT 2-8 AND UNIT 2-9 AT SECOND SPAN.
2. REMOVE ALL DELAMINATED/SPALLED CONCRETE DOWN TO SOUND CONCRETE. THE EXTENT/LENGTH OF REPAIR WILL BE DEPENDENT ON THE DAMAGE/CORROSION IN THE STRANDS (REFER TO ITEM 4).
3. CUT AND REMOVE SIGNIFICANTLY CORRODED STEEL. EXPOSE AT A MIN. 3 FT OF SOUND PRESTRESSING STRANDS ON BOTH ENDS OF THE REPAIR AREA. NOTE THERE ARE UP TO (7) PT STRANDS AFFECTED BY DAMAGED/REPAIR WHICH NEEDS TO BE EXPOSED.
4. APPLY CORROSION INHIBITORS TO ALL EXPOSED STEEL TO PREVENT FUTURE CORROSION.
5. INSTALL NEW LONGITUDINAL STEEL AND L-DOWELS, AS SHOWN. SPLICE LONGITUDINAL STEEL WITH THE PT STRANDS 30".
6. PARTIALLY FILL THE CORES WITH FOAM MATERIAL AS SHOWN TO CREATE A BACKING FOR THE REPAIR CONCRETE.
7. FORM AND PUMP HIGH EARLY STRENGTH CONCRETE REPAIR MATERIAL WITH MIN. F'C-6000 PSI.
8. INSTALL V-WRAP FRP REINFORCEMENT AS SHOWN.
9. APPLY 2 COATS OF TSTRATA TC TO BOTTOM OF THE TWO UNITS (CONCRETE AND FRP).

BRIDGE SLAB SCHEDULE

UNIT	NO.	THICKNESS	SPACING
1	1	24" - 3"	24" - 3"
2	2	24" - 3"	24" - 3"
3	3	24" - 3"	24" - 3"
4	4	24" - 3"	24" - 3"
5	5	24" - 3"	24" - 3"
6	6	24" - 3"	24" - 3"
7	7	24" - 3"	24" - 3"
8	8	24" - 3"	24" - 3"
9	9	24" - 3"	24" - 3"
10	10	24" - 3"	24" - 3"
11	11	24" - 3"	24" - 3"
12	12	24" - 3"	24" - 3"
13	13	24" - 3"	24" - 3"
14	14	24" - 3"	24" - 3"
15	15	24" - 3"	24" - 3"
16	16	24" - 3"	24" - 3"
17	17	24" - 3"	24" - 3"
18	18	24" - 3"	24" - 3"
19	19	24" - 3"	24" - 3"
20	20	24" - 3"	24" - 3"
21	21	24" - 3"	24" - 3"
22	22	24" - 3"	24" - 3"
23	23	24" - 3"	24" - 3"
24	24	24" - 3"	24" - 3"
25	25	24" - 3"	24" - 3"
26	26	24" - 3"	24" - 3"
27	27	24" - 3"	24" - 3"
28	28	24" - 3"	24" - 3"
29	29	24" - 3"	24" - 3"
30	30	24" - 3"	24" - 3"
31	31	24" - 3"	24" - 3"
32	32	24" - 3"	24" - 3"
33	33	24" - 3"	24" - 3"
34	34	24" - 3"	24" - 3"
35	35	24" - 3"	24" - 3"
36	36	24" - 3"	24" - 3"
37	37	24" - 3"	24" - 3"
38	38	24" - 3"	24" - 3"
39	39	24" - 3"	24" - 3"
40	40	24" - 3"	24" - 3"
41	41	24" - 3"	24" - 3"
42	42	24" - 3"	24" - 3"
43	43	24" - 3"	24" - 3"
44	44	24" - 3"	24" - 3"
45	45	24" - 3"	24" - 3"
46	46	24" - 3"	24" - 3"
47	47	24" - 3"	24" - 3"
48	48	24" - 3"	24" - 3"
49	49	24" - 3"	24" - 3"
50	50	24" - 3"	24" - 3"
51	51	24" - 3"	24" - 3"
52	52	24" - 3"	24" - 3"
53	53	24" - 3"	24" - 3"
54	54	24" - 3"	24" - 3"
55	55	24" - 3"	24" - 3"
56	56	24" - 3"	24" - 3"
57	57	24" - 3"	24" - 3"
58	58	24" - 3"	24" - 3"
59	59	24" - 3"	24" - 3"
60	60	24" - 3"	24" - 3"
61	61	24" - 3"	24" - 3"
62	62	24" - 3"	24" - 3"
63	63	24" - 3"	24" - 3"
64	64	24" - 3"	24" - 3"
65	65	24" - 3"	24" - 3"
66	66	24" - 3"	24" - 3"
67	67	24" - 3"	24" - 3"
68	68	24" - 3"	24" - 3"
69	69	24" - 3"	24" - 3"
70	70	24" - 3"	24" - 3"
71	71	24" - 3"	24" - 3"
72	72	24" - 3"	24" - 3"
73	73	24" - 3"	24" - 3"
74	74	24" - 3"	24" - 3"
75	75	24" - 3"	24" - 3"
76	76	24" - 3"	24" - 3"
77	77	24" - 3"	24" - 3"
78	78	24" - 3"	24" - 3"
79	79	24" - 3"	24" - 3"
80	80	24" - 3"	24" - 3"
81	81	24" - 3"	24" - 3"
82	82	24" - 3"	24" - 3"
83	83	24" - 3"	24" - 3"
84	84	24" - 3"	24" - 3"
85	85	24" - 3"	24" - 3"
86	86	24" - 3"	24" - 3"
87	87	24" - 3"	24" - 3"
88	88	24" - 3"	24" - 3"
89	89	24" - 3"	24" - 3"
90	90	24" - 3"	24" - 3"
91	91	24" - 3"	24" - 3"
92	92	24" - 3"	24" - 3"
93	93	24" - 3"	24" - 3"
94	94	24" - 3"	24" - 3"
95	95	24" - 3"	24" - 3"
96	96	24" - 3"	24" - 3"
97	97	24" - 3"	24" - 3"
98	98	24" - 3"	24" - 3"
99	99	24" - 3"	24" - 3"
100	100	24" - 3"	24" - 3"

BRIDGE FRAMING PLAN

PLAN - PRESTRESSED UNITS

ELEVATION - PRESTRESSED UNITS

HART-REYNOLDS & ASSOCIATES, INC.		CORAL GABLES, FLORIDA	
MATHESON HAMMOCK PARK		DADE COUNTY, FLORIDA	
BRIDGE AND APPROACH ROAD		CORAL GABLES, FLORIDA	
Drawn By: J.C.	Checked By: J.C.	Project No.:	Sheet No.:
Date: JUNE 1961	Date: JUNE 1961	Project No.:	Sheet No.:
Author: J.C.	Reviewer: J.C.	Project No.:	Sheet No.:
PRESTRESSED SLAB UNITS		No. 8	
at 12. Month			